

Advances in sheet metal forming research

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हिन्दी संस्करण (Hindi Version)

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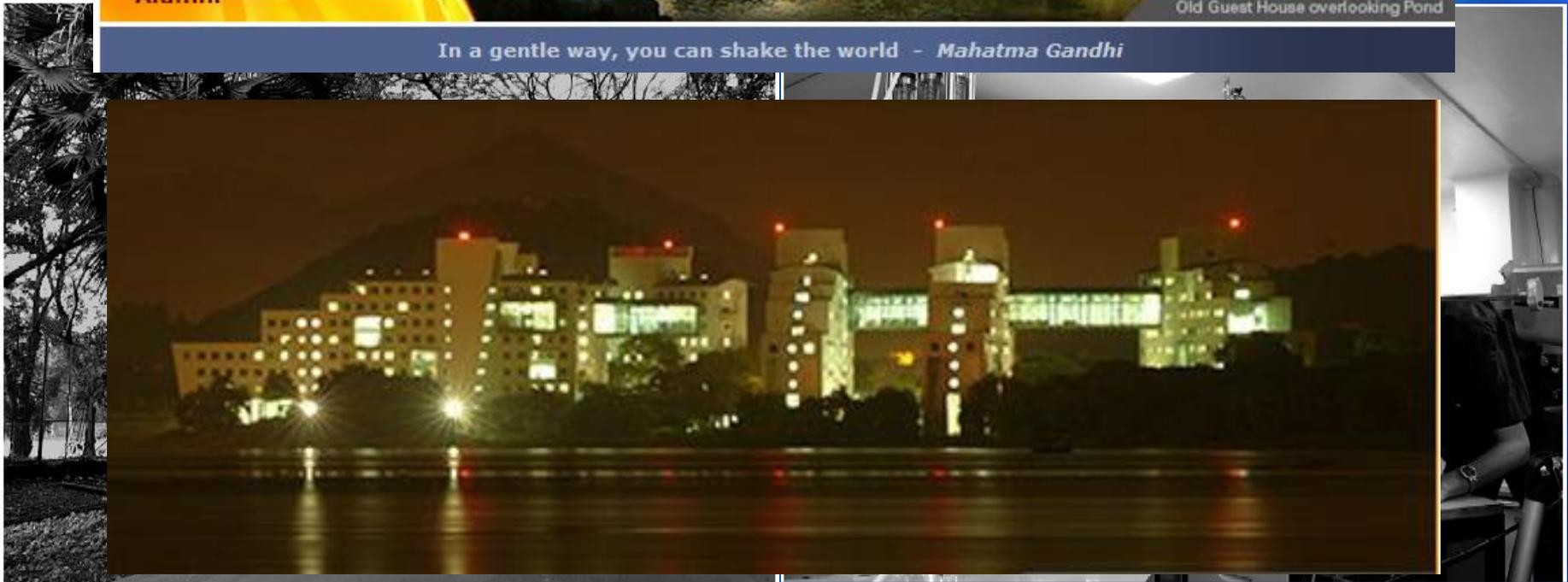
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Old Guest House overlooking Pond

In a gentle way, you can shake the world - *Mahatma Gandhi*



Engages in research, education, training, technology development and related activities in most areas of technology, science & management

- 530 acres (5.3 sq. km) of campus area
- 15 Departments, 1 School, 4 IDPs & 9 Centers
- ~600 fulltime faculty & 90 adjunct faculty
- ~1300 support staff
- ~9600 students (P.G ~ 6000; PhD~2000)
- ~750 project research staff



Patents (India and Foreign) 2012-2013	>100
Number of industries which come to us for projects	>2000
Research funding in INR (Governmental & Industrial, 2012-13)	~300 Cr
Number of technology spinoffs from IITB technologies	>50

Overview of NCAIR

Vision

- ❖ Create a World Class Aerospace Ecosystem in India

Mission

- ❖ To be a catalyst for collaboration between industry, Academia, R&D Organizations and Government
- ❖ To provide economically viable and sustainable solutions
- ❖ To promote Innovation, Knowledge Creation and Entrepreneurship
- ❖ To disseminate knowhow and develop human resources

Inception

19th November 2010

Key Strategic Technologies

Machining

Forming

Casting

Scope of Materials

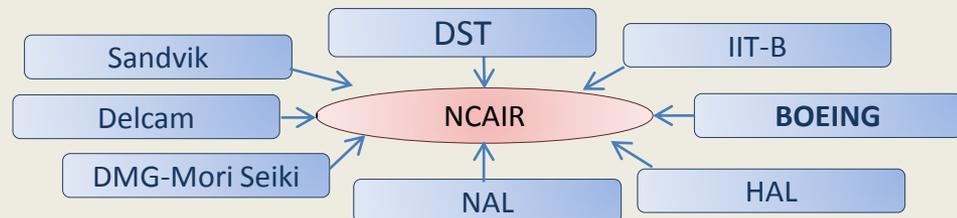
Titanium

Super Alloys

Composites

Aluminum, Magnesium, AHSS

Stake-holders



Services of NCAIR

Core Services

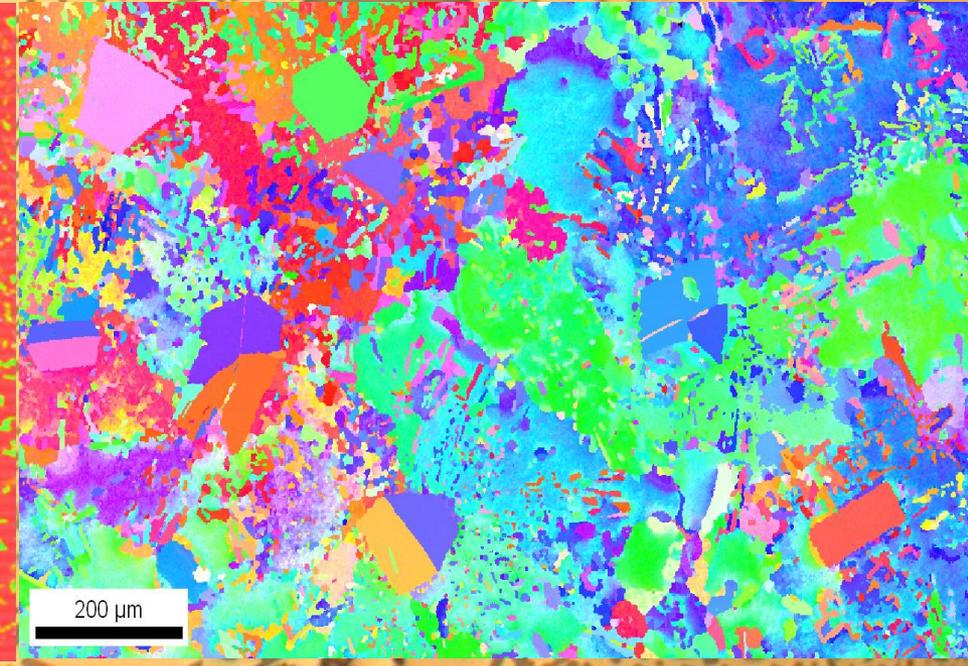
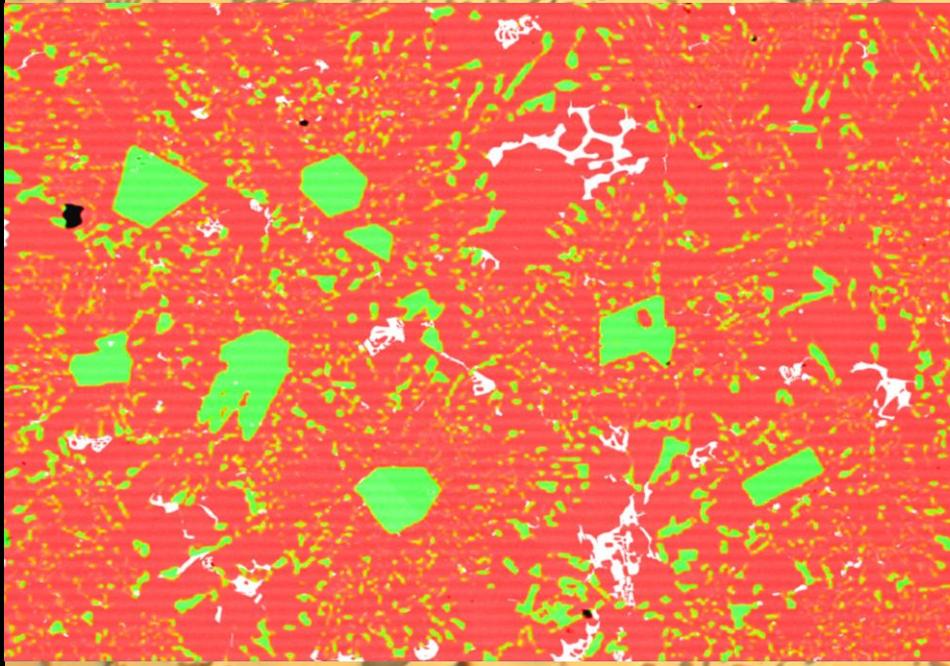
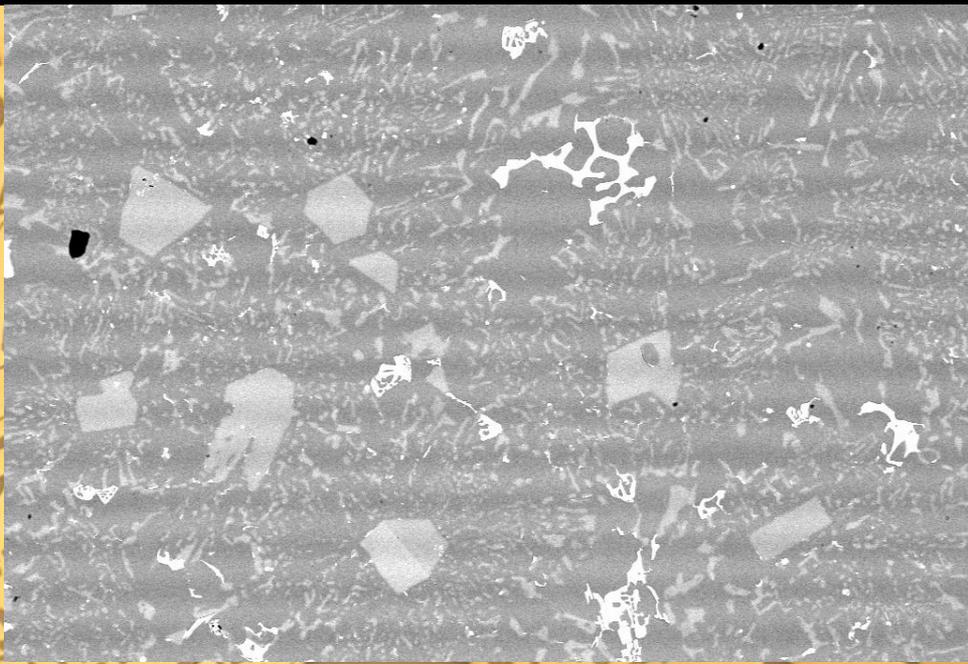
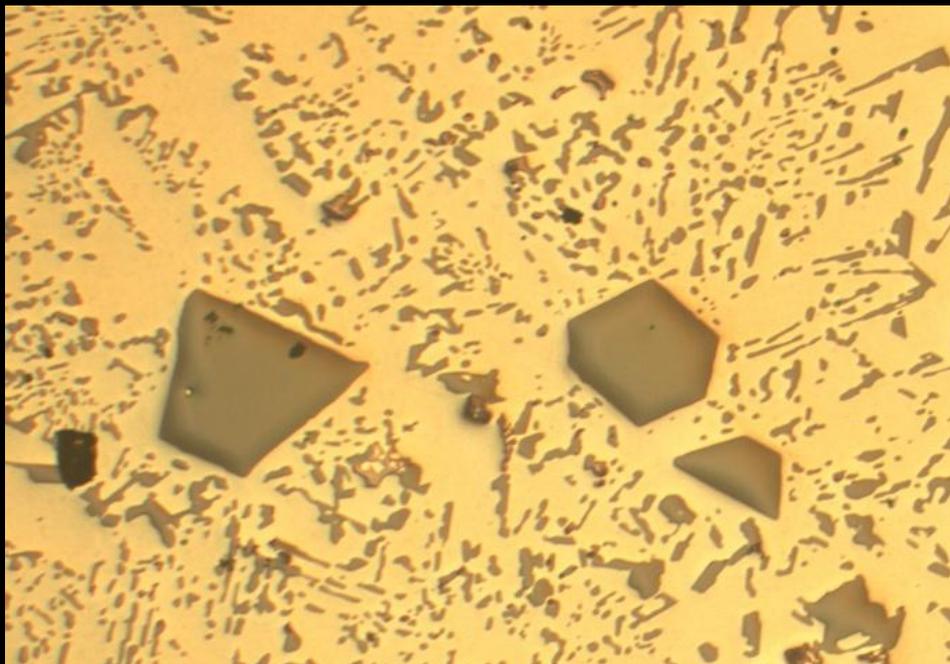
- ✓ R&D Projects
- ✓ Technology Transfer

Enabling Services

- ✓ Specialized Training Programs
- ✓ Adv Aero Mfg and testing facilities for R&T Activities
- ✓ Mentoring and business Services

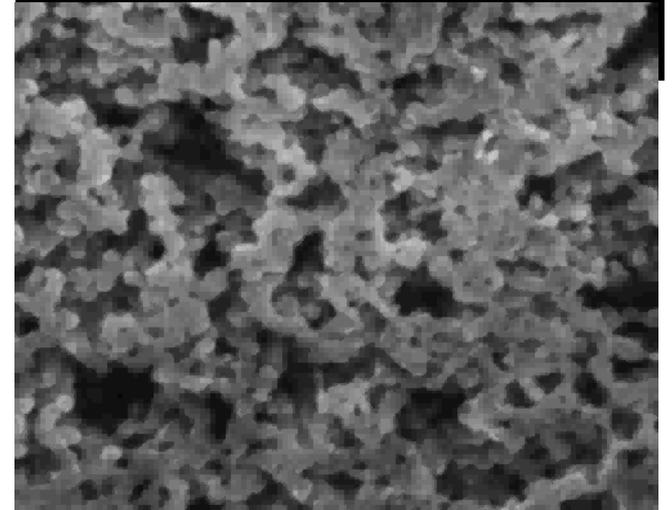
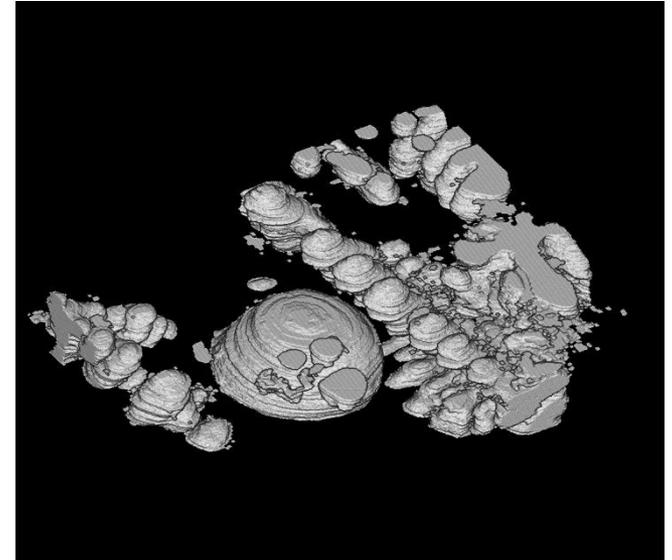
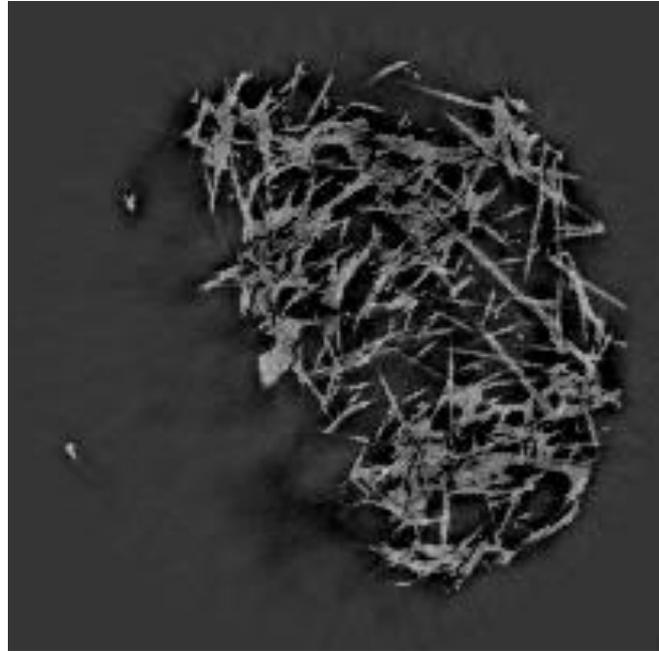
Content

- Macro modeling
 - Constitutive property (anisotropy and evolution) based
- Micro Modeling
 - Second-phase particle based large scale modeling
- Nano Modeling
 - Nano structure modification using pre-form annealing

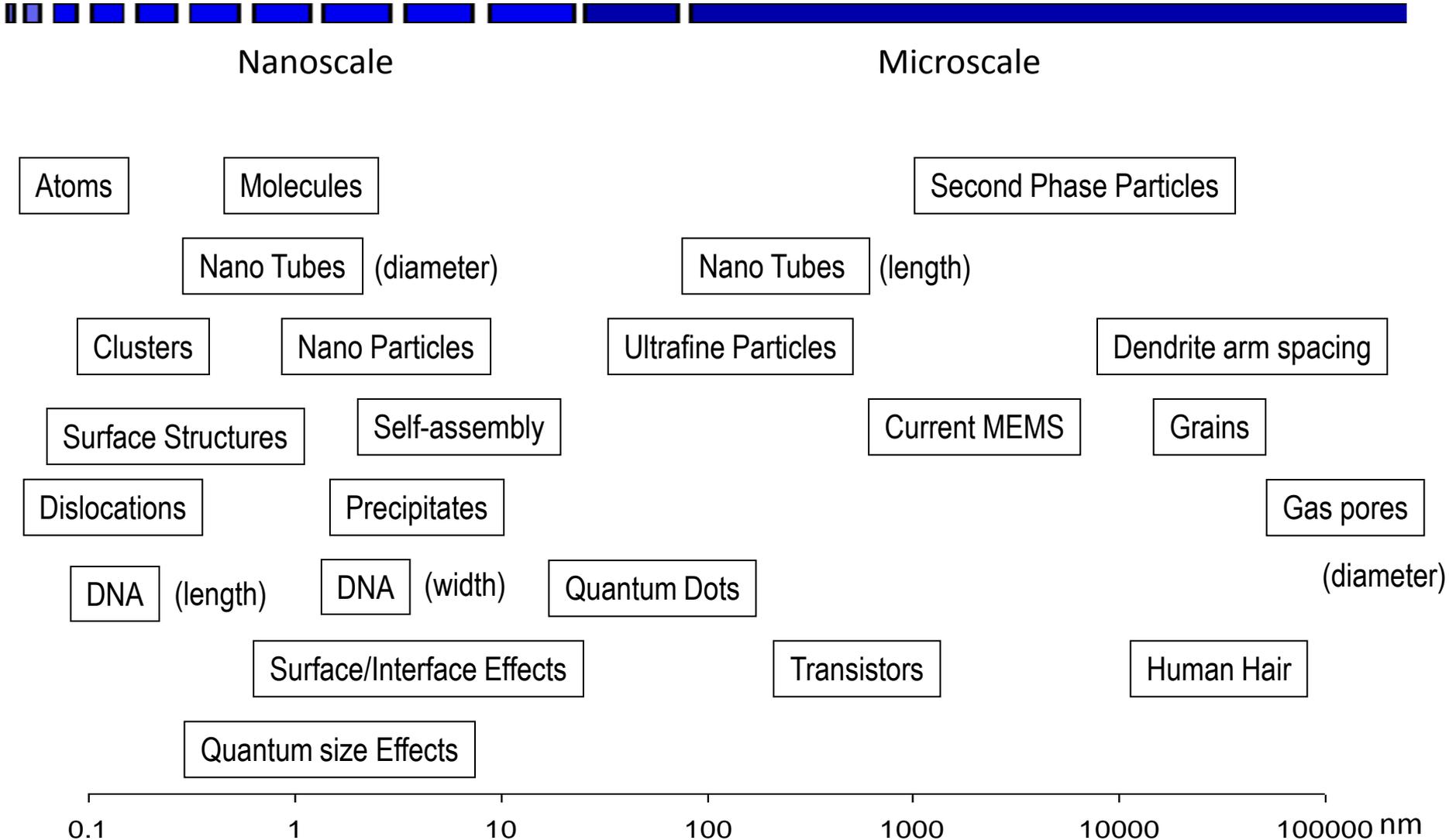


Modalities of acquisition

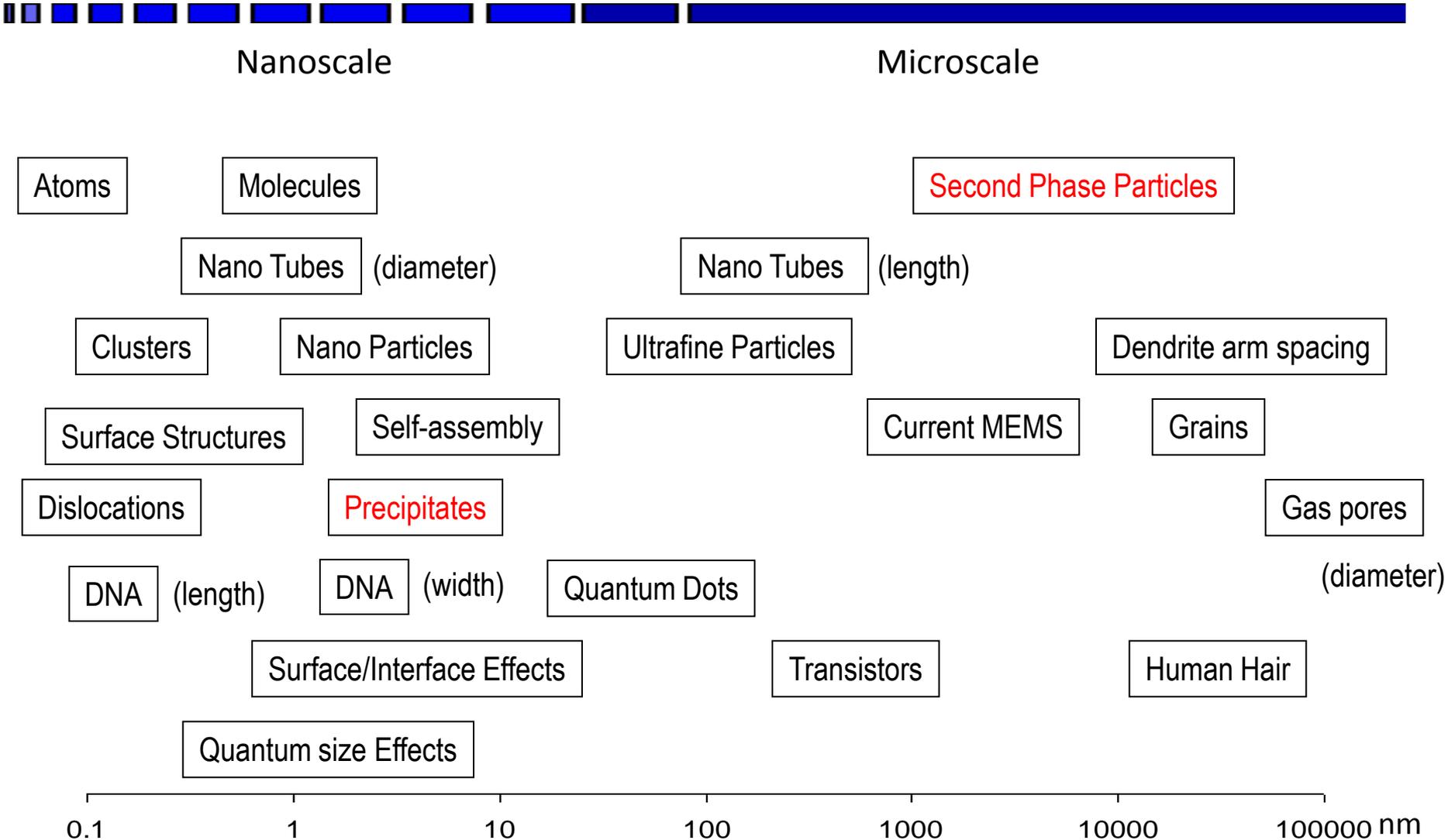
- Optical
- SEM
- EBSD
- FIB
- TEM
- AFM
- SPM
- X-ray CT
- PET, MRI, SIMS, etc.



Larger to smaller



Larger to smaller



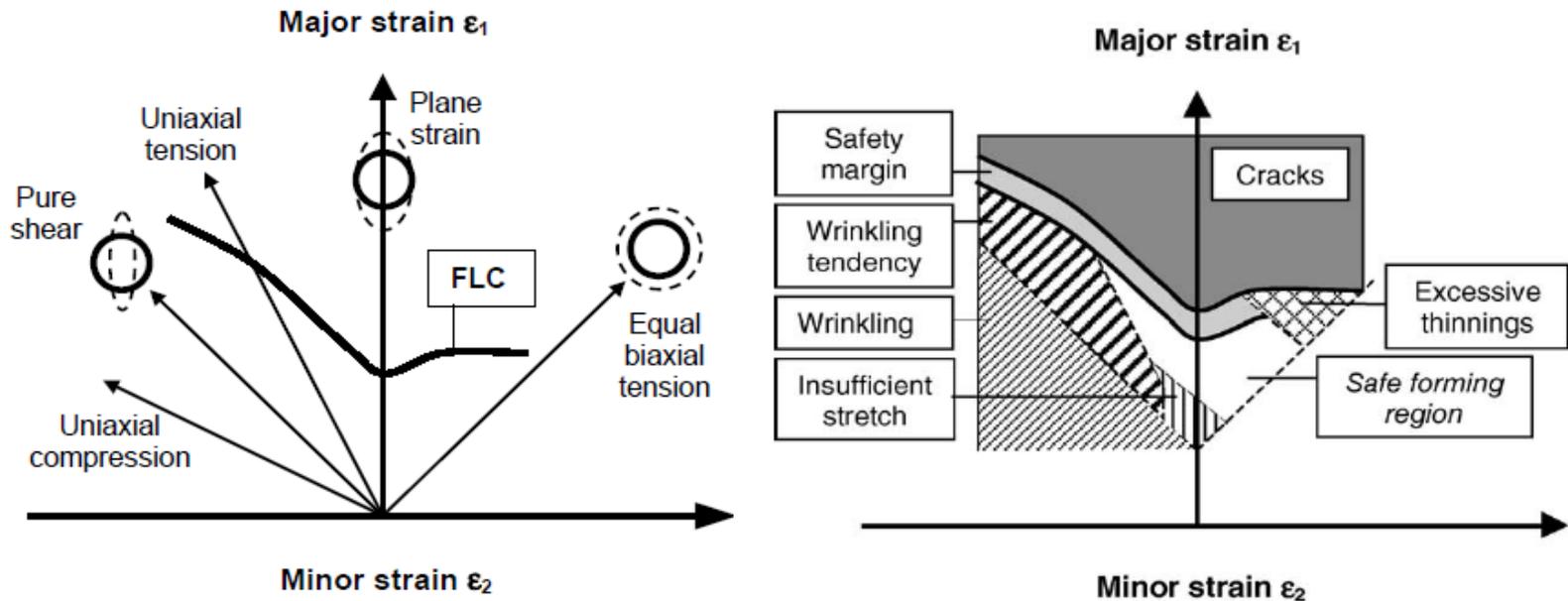
Case Study 1

Macro modeling of Ti64 sheet deformation

Technological challenges

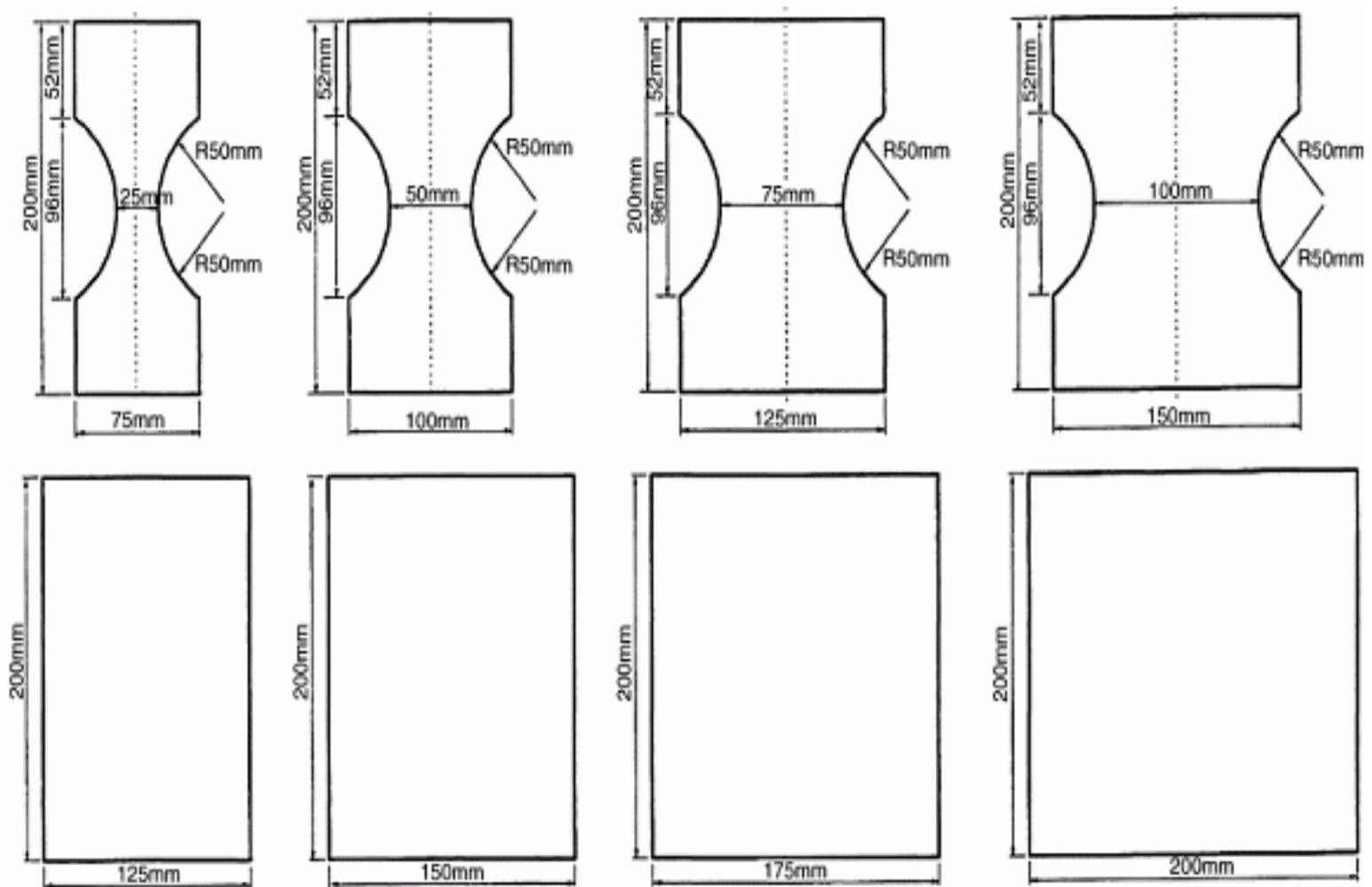
- Formability
- A-class surface finish
- Dent resistant after paint-bake
- Cost

Forming Limit Diagram(FLD)



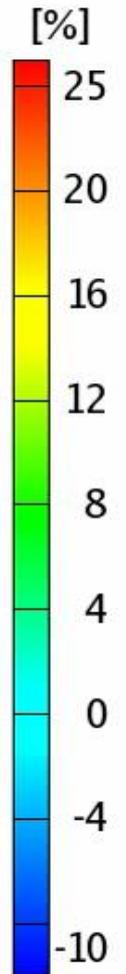
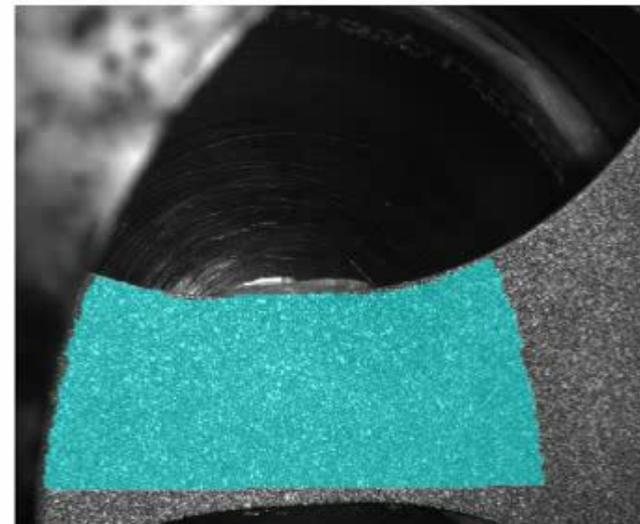
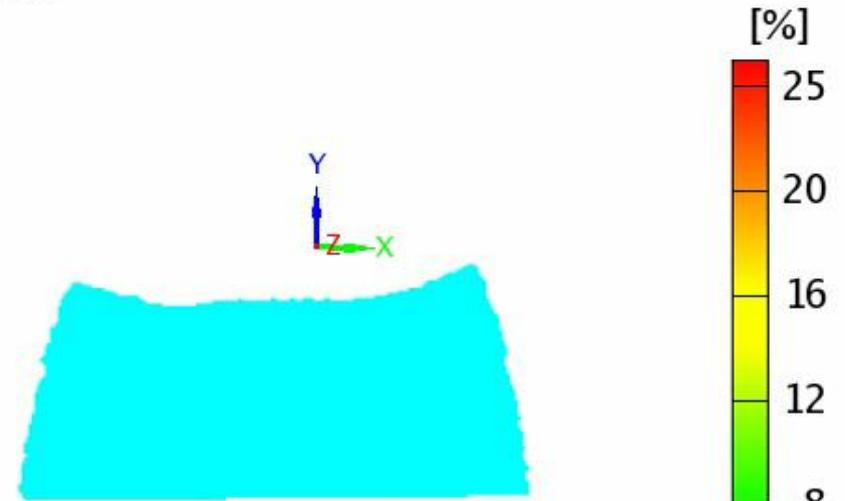
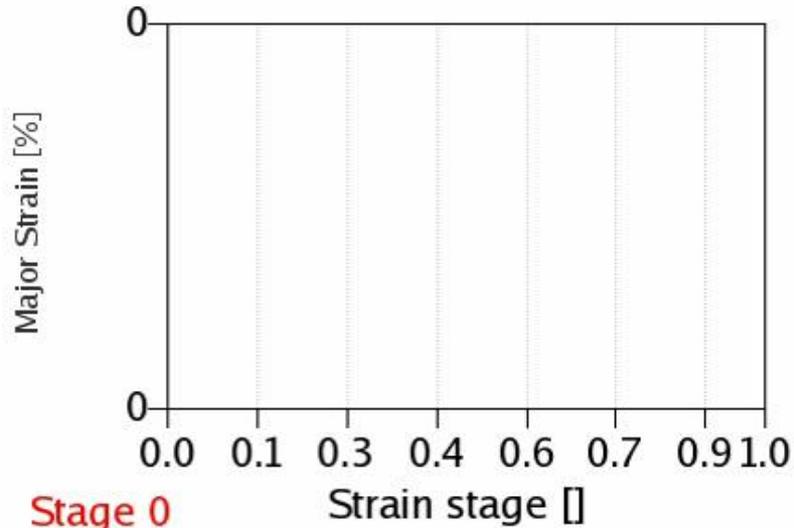
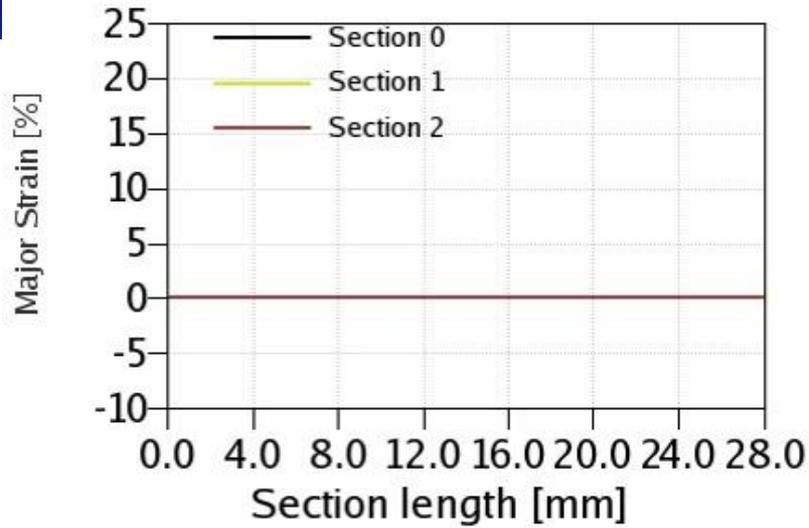
- FLD indicates different modes of deformation
- FLD indicates different forming regions

Specimens geometry for Forming Limit Diagram

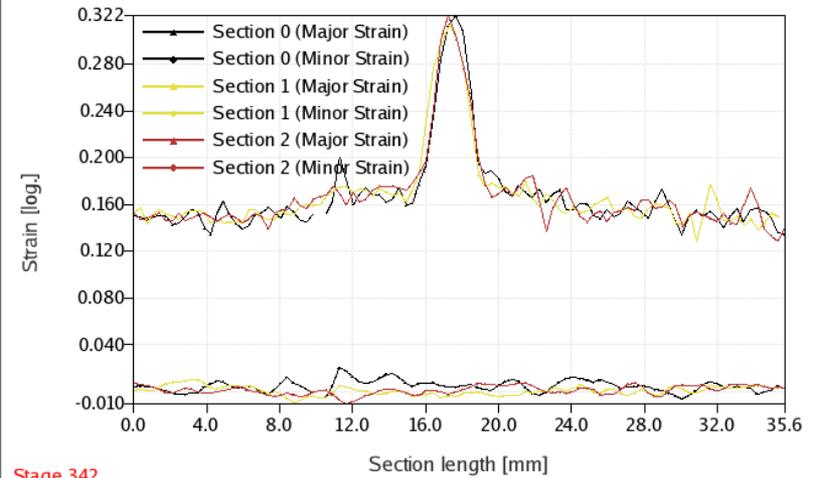
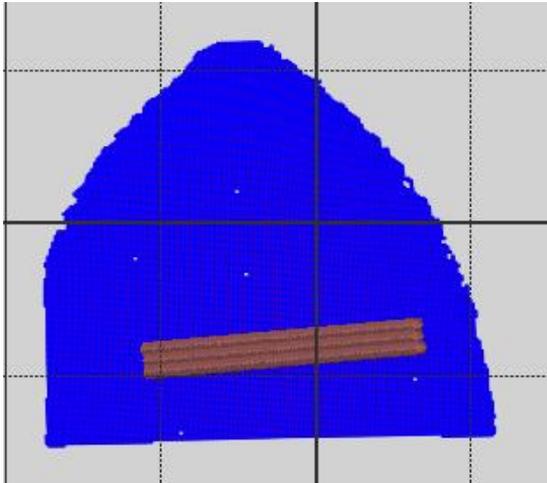


Major Strain

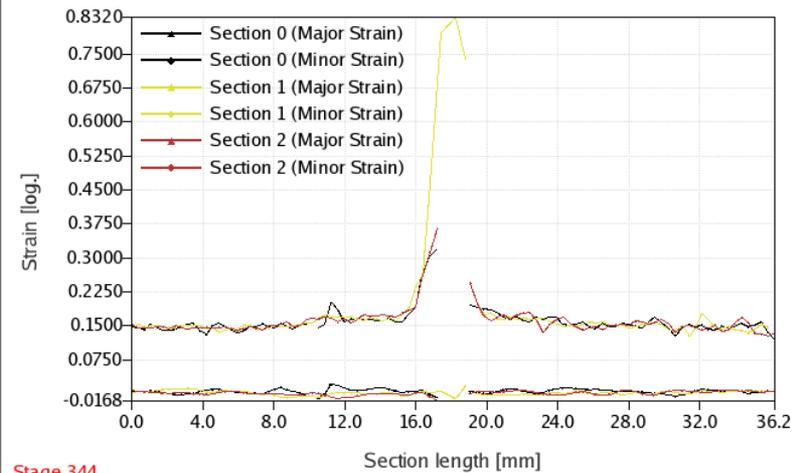
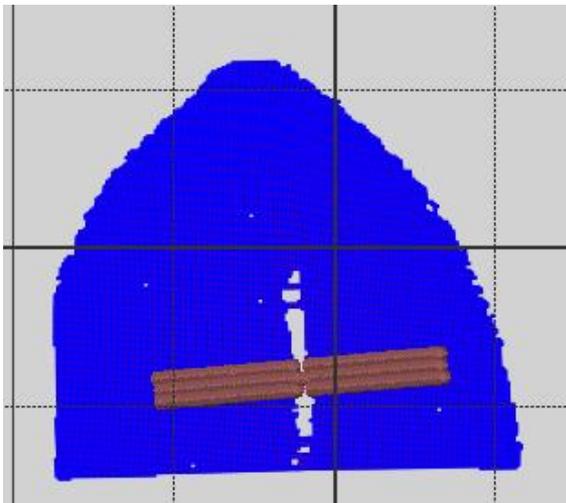
Stage 0
Time 0.00 s



Strain diagram

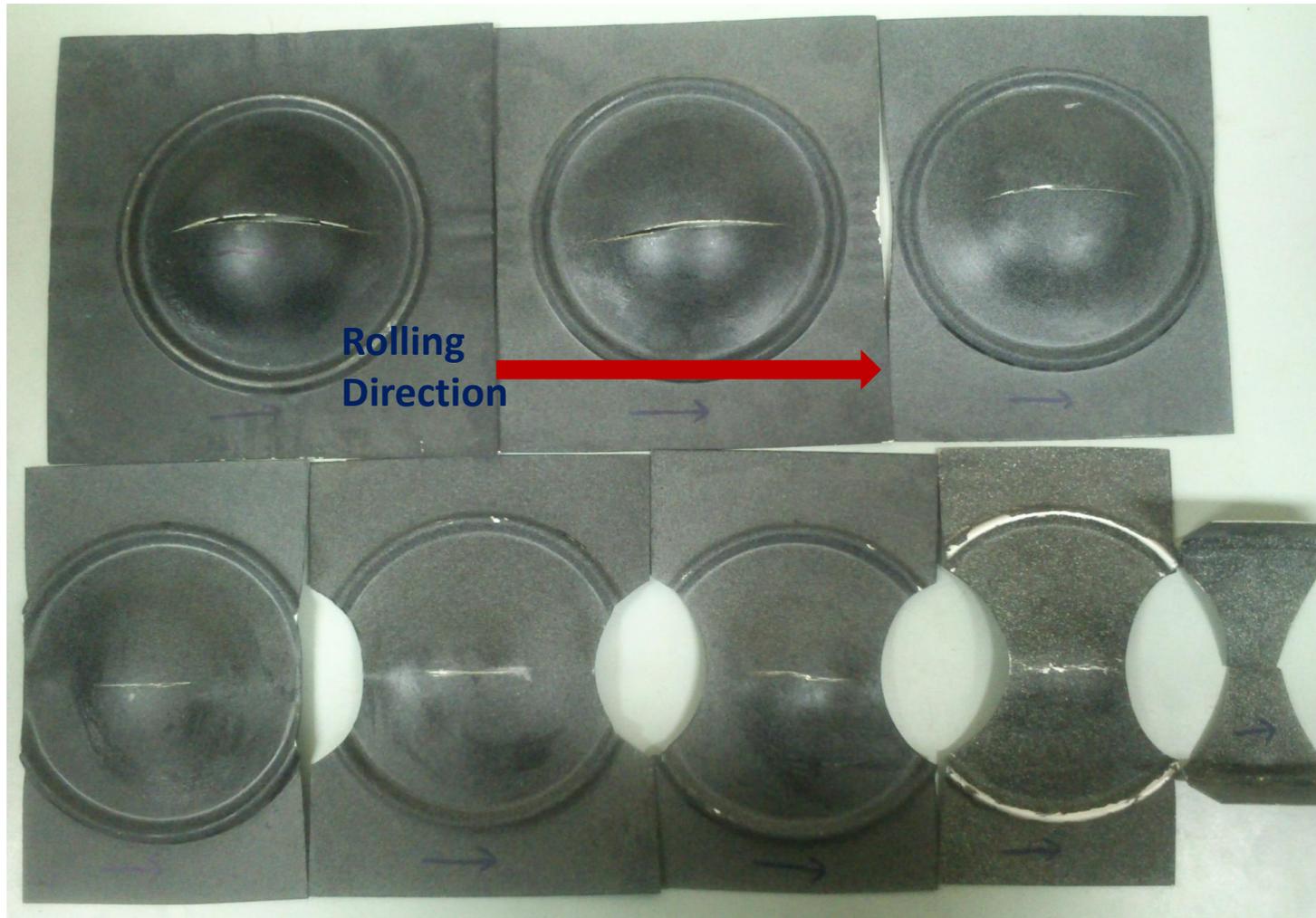


Stage 342

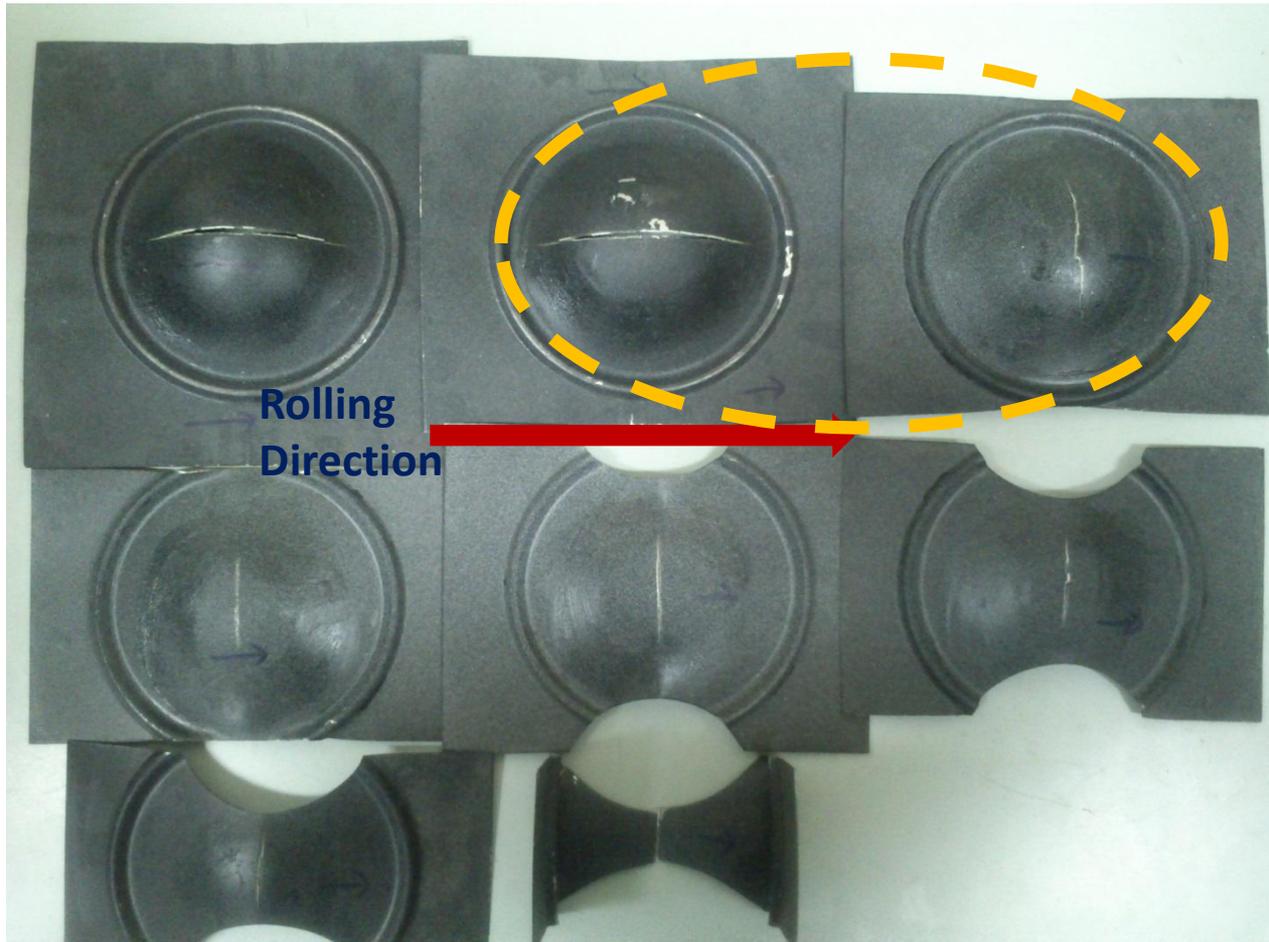


Stage 344

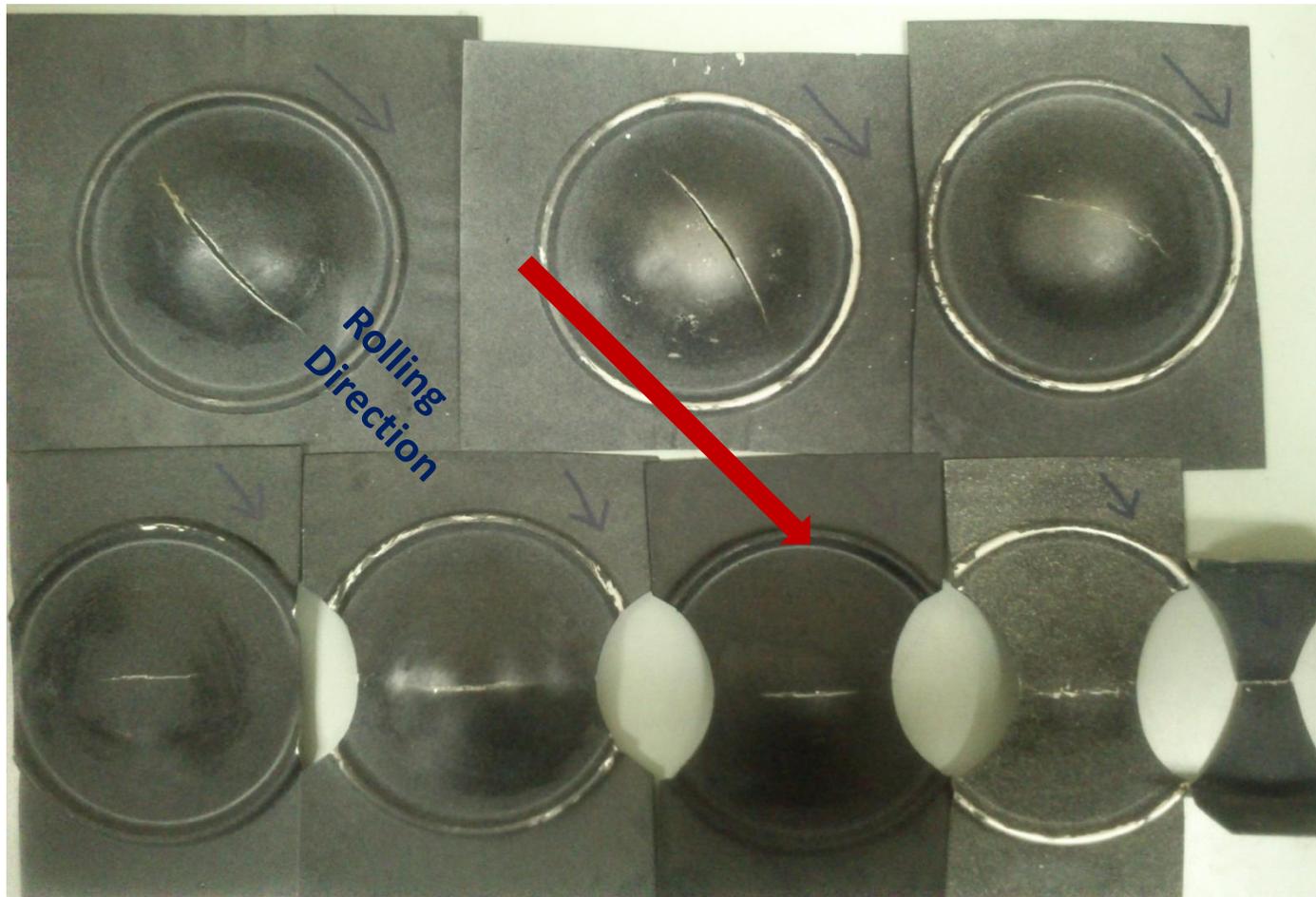
FLD with major stress along TD



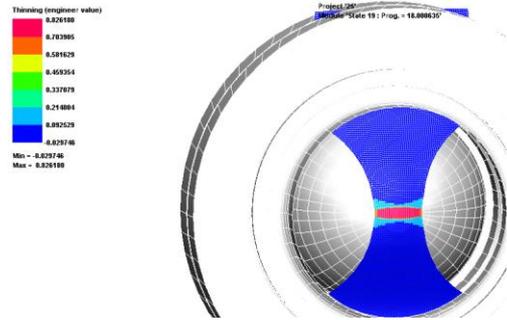
FLD with major stress along RD



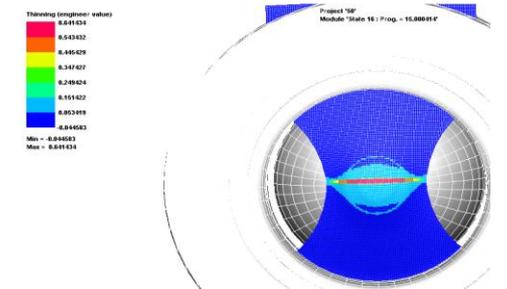
FLD with major stress along ID



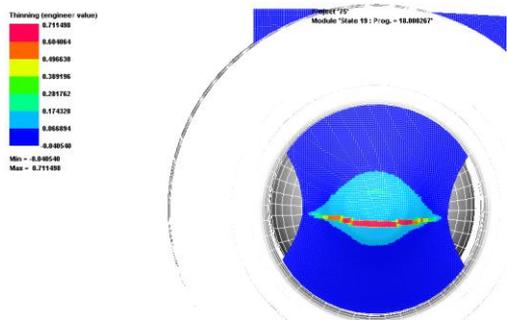
Transverse direction



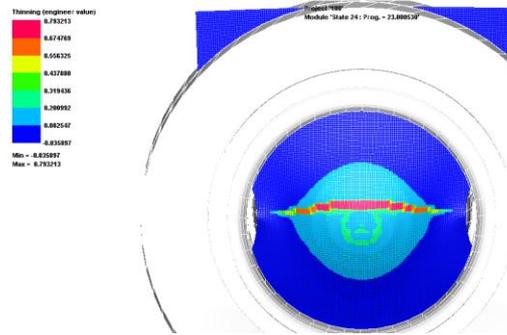
25X200



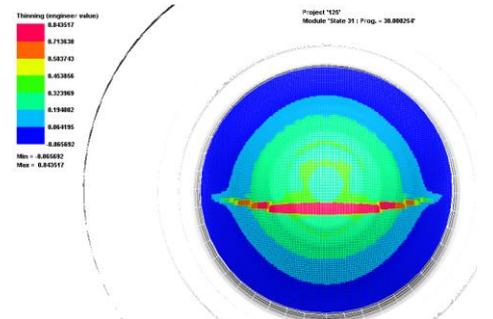
50X200



75X200



100X200



125X200

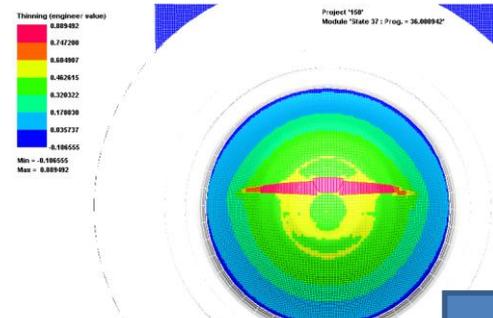
$R0 = 0.558$

$R45 = 0.704$

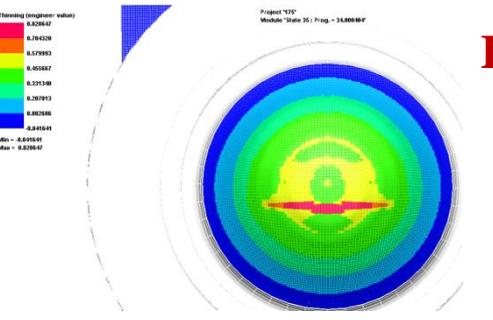
$R90 = 0.833$

$N = 0.09, k = 400 \text{ Mpa}$

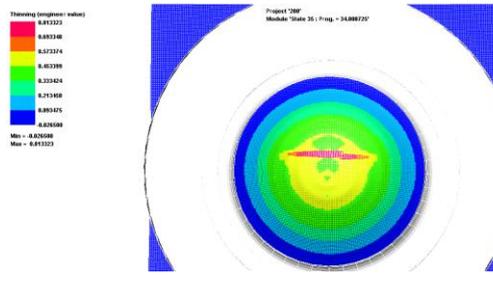
$\nu = 0.01$



150X200



175X200

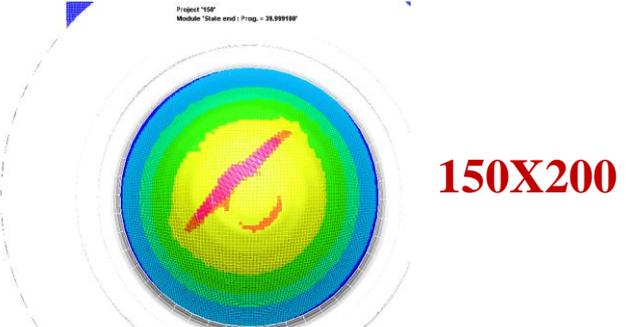
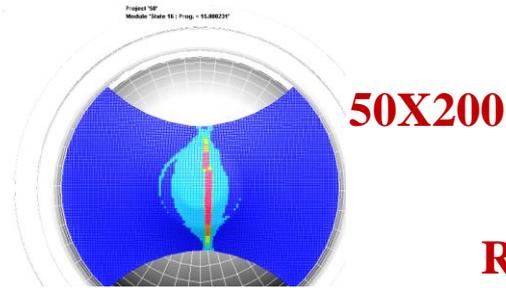
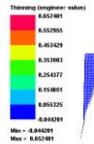
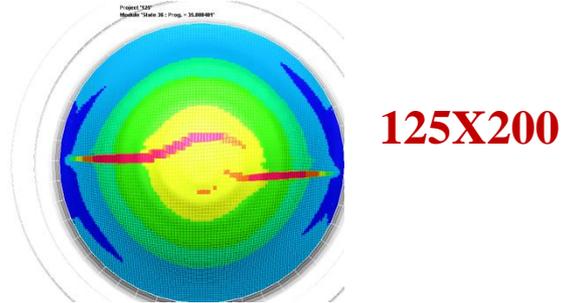
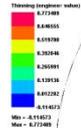
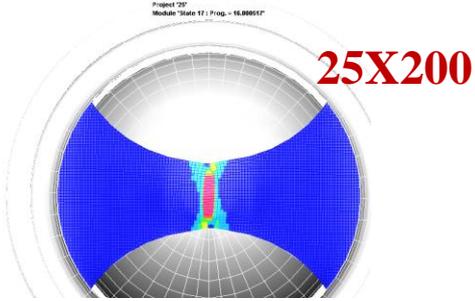
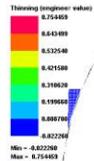


200X200

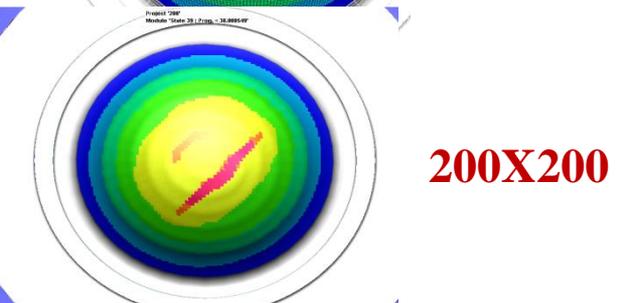
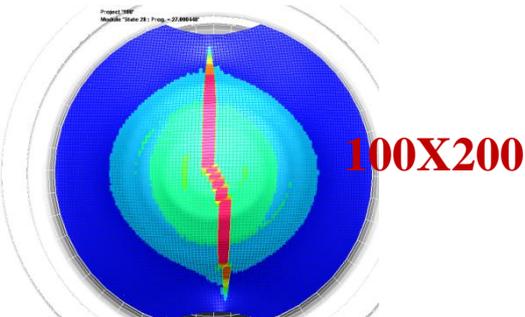
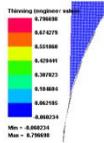
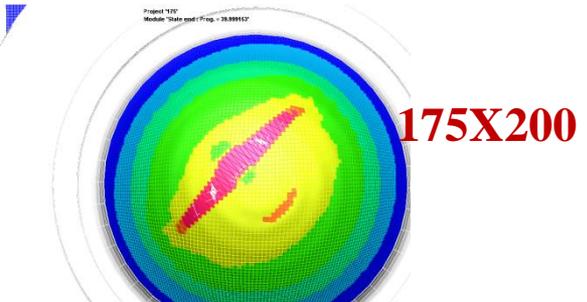
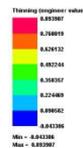
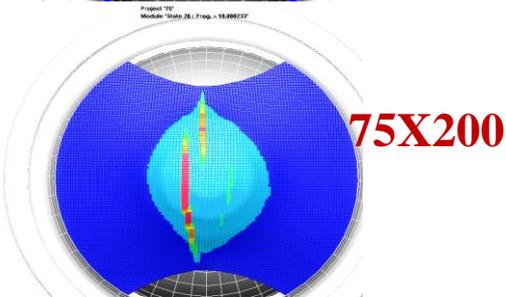
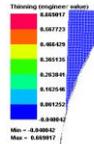


Rolling direction

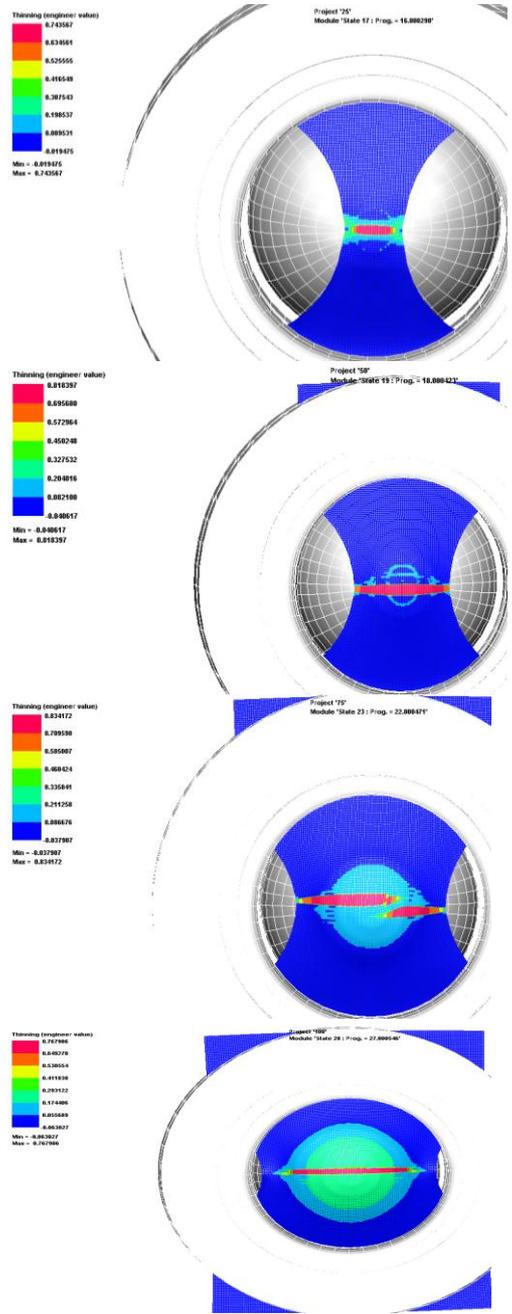
Inclined direction



Rolling direction



Rolling direction



25X200

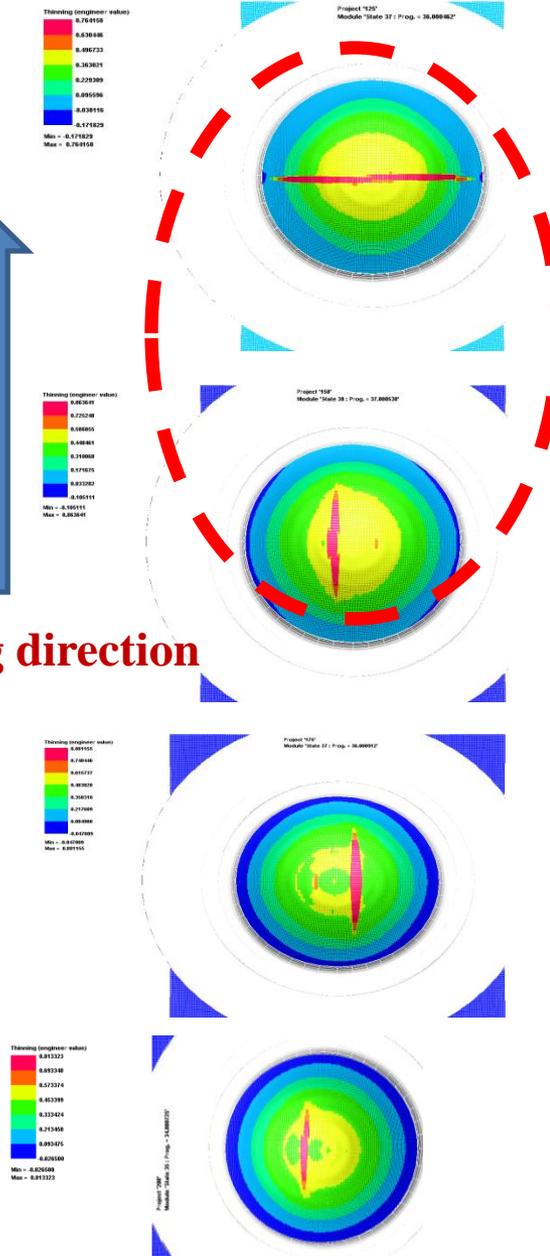
50X200

75X200

100X200



Rolling direction



125X200

150X200

175X200

200X200

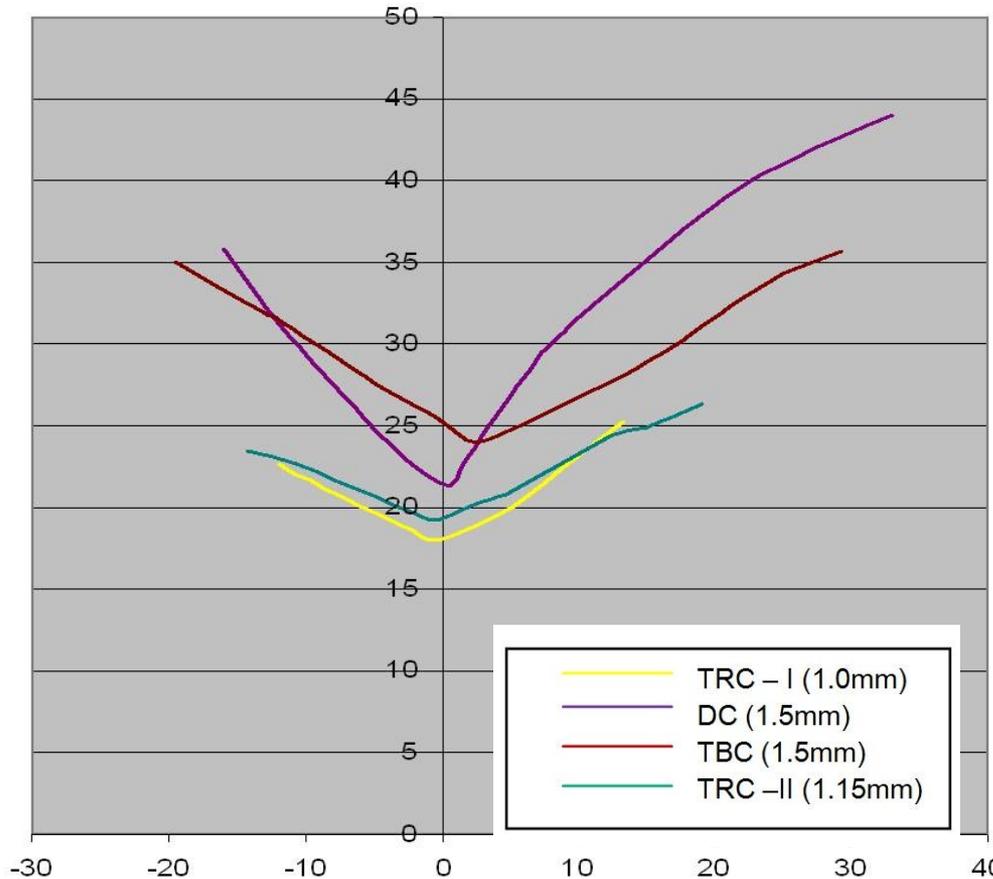
Summary

- The final fracture is a sum total effect of sample geometry (w.r.t. loading) and material anisotropy.
- The changeover from fracture along rolling direction to major stress direction can be captured by macro anisotropic analysis.

Case Study 2

Al sheet formability (DC vs CC)

Motivation



Large formability variation of same 5754 Al alloy processed through different processes

Automotive lightweighting

- Advantages
 - Fuel consumption and emissions
 - 10% weight reduction => 7% increase in fuel economy
 - Performance
 - Less inertia => better acceleration
 - Passive safety
 - Lighter thrust, optimal weight distribution
 - Active safety
 - Increased braking stability and efficacy
 - Acoustics
 - Dynamic alleviation
- FIVE KEY Challenges
 - Cost reduction
 - Manufacturability
 - Design data and test methodologies
 - Joining
 - Recycling and repair.

Cost Analysis

- Continuous casting vs direct chill cast sheets
 - 25% energy savings in CC
 - 14% economic saving in CC
- Manufacturability
 - Formability of CC is lower than DC (FLD)

Alloy composition and processing

5754 Alloy	Mg wt%	Mn wt%	Cr wt%	Fe wt%	Si wt%
DC	3.0	0.25	0.01	0.18	<0.10
TBC	3.1	0.25	<0.01	0.24	<0.10
TRC-I	2.8	0.01	<0.01	0.25	0.10
TRC-II	2.9	0.01	<0.01	0.24	0.08



Di

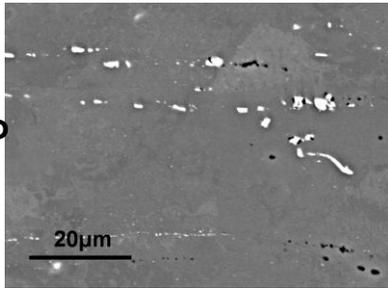
Co

Co

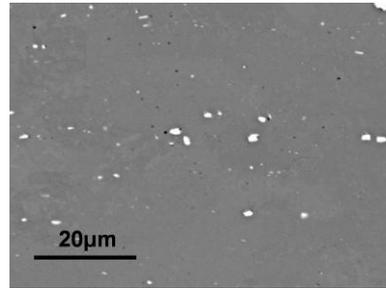
Batch #

Typical microstructure of various 5754 alloys

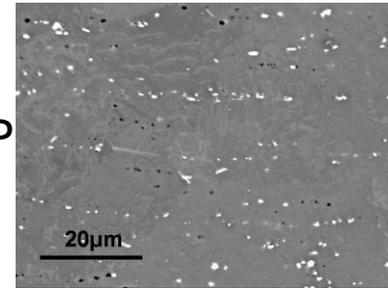
TBC



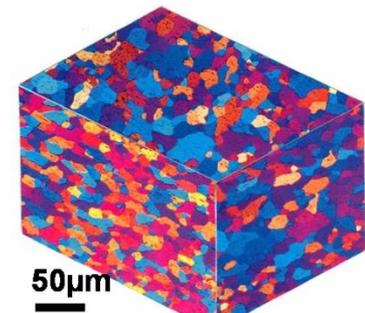
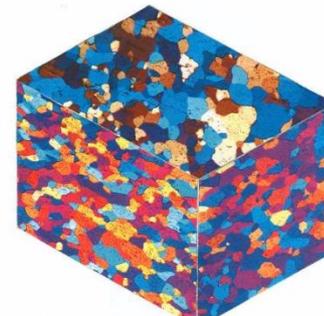
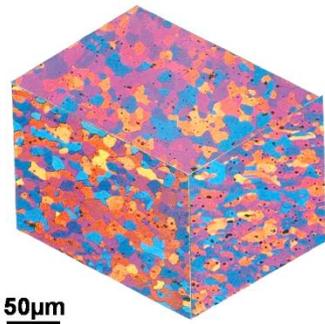
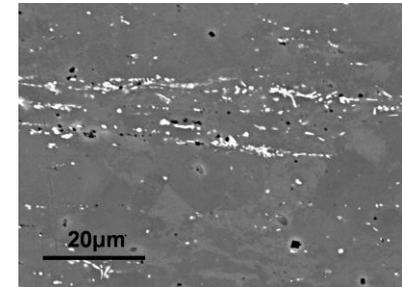
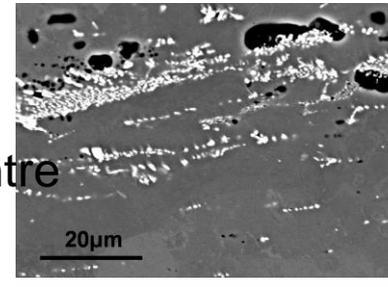
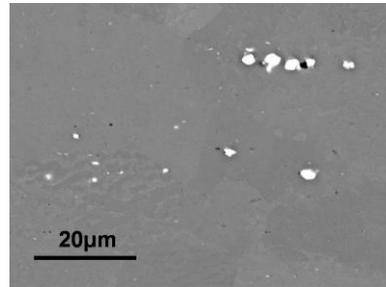
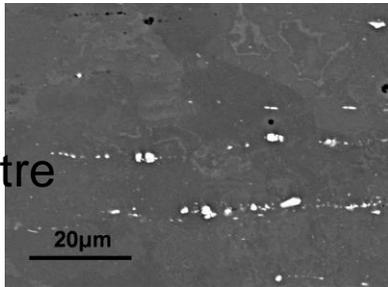
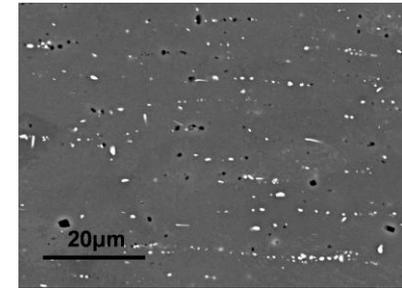
DC



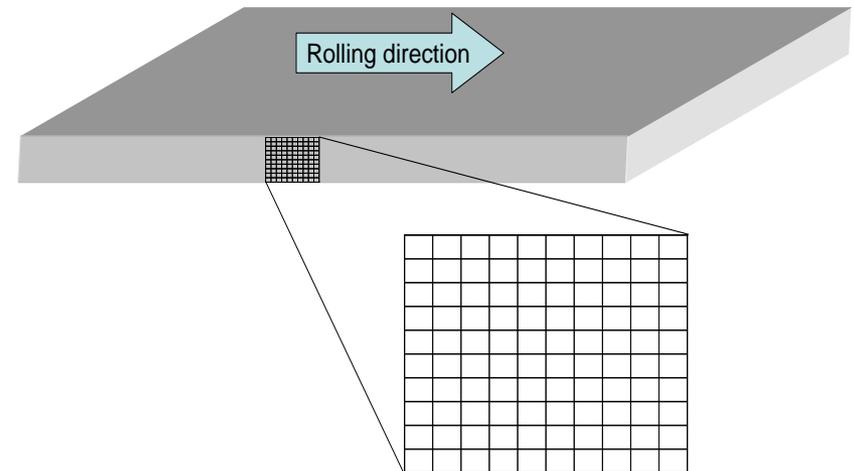
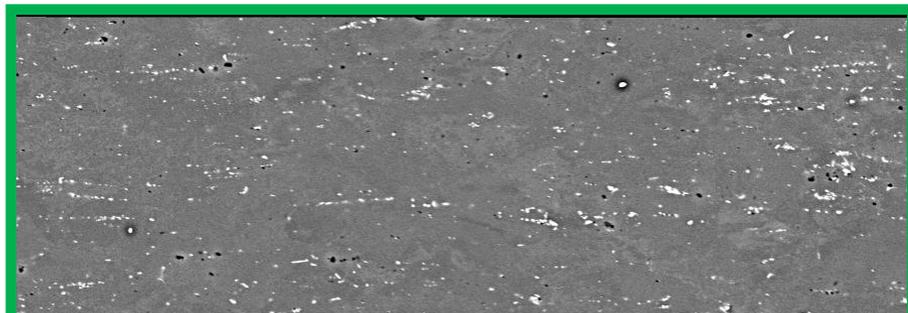
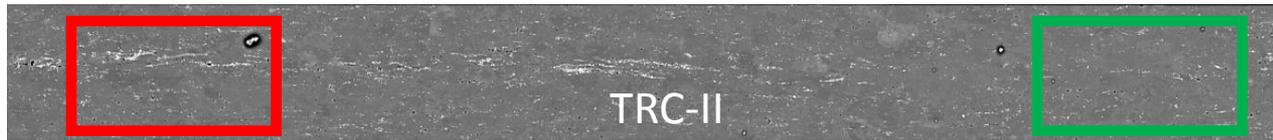
TRC-I



TRC-II

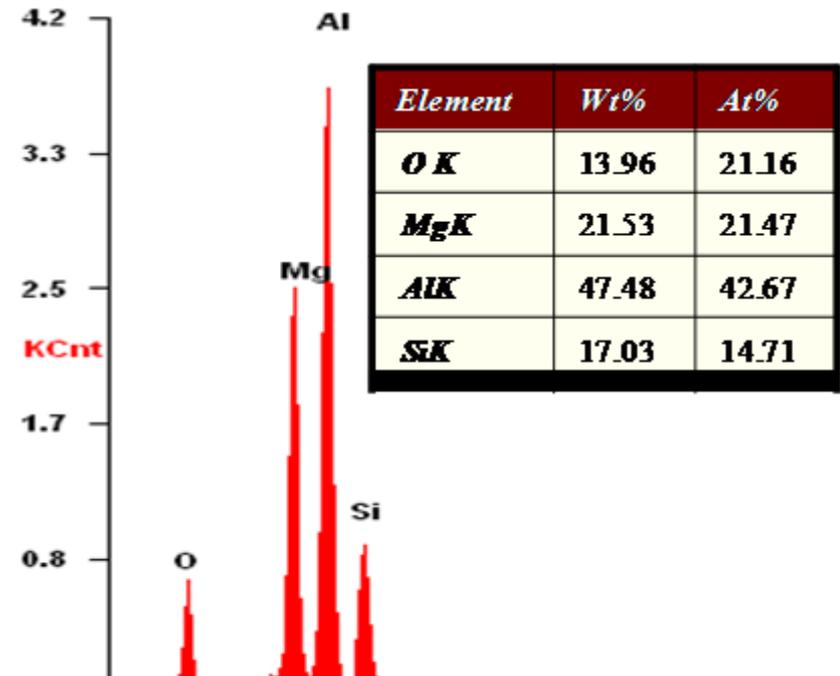
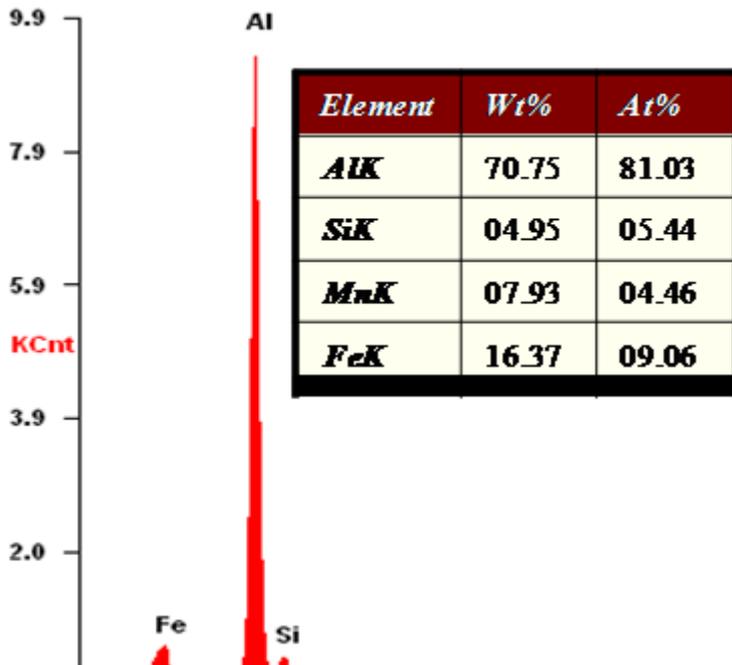
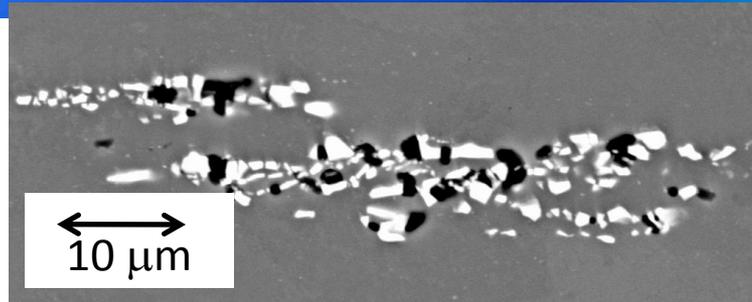


Center-line Segregation



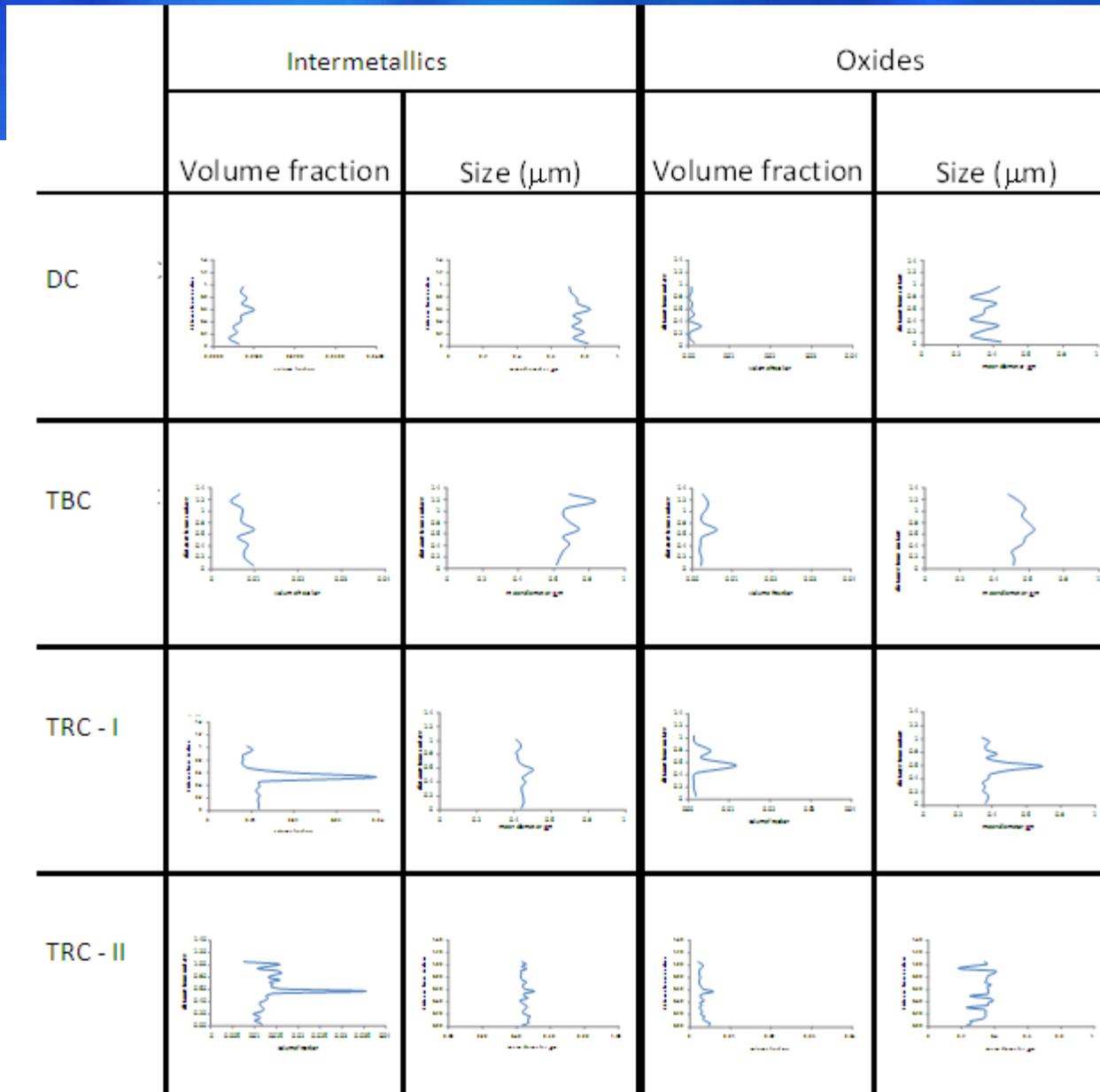
Discontinuous centerline segregation in TRC-II

Second phase particles

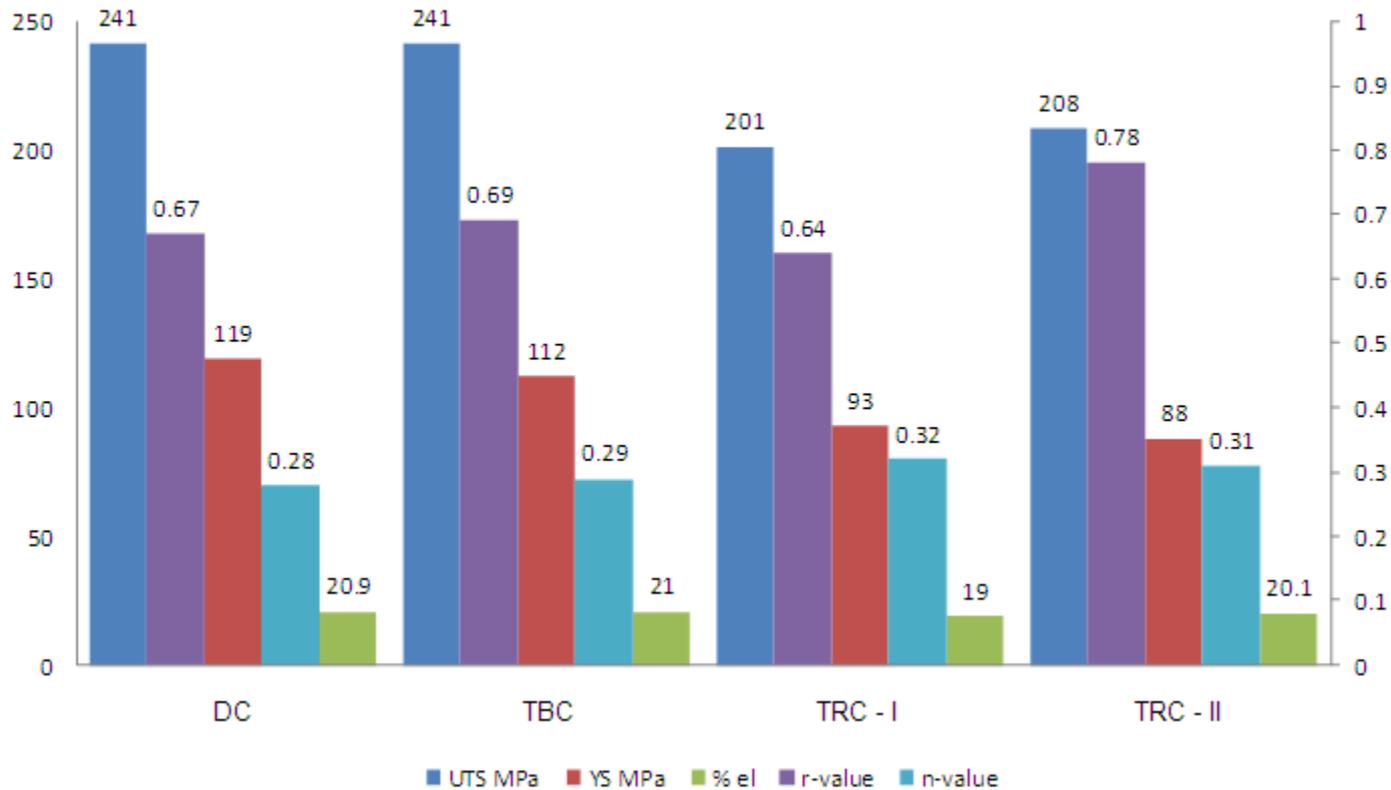


Two type of second phase particles are present

Through thickness microstructure variation

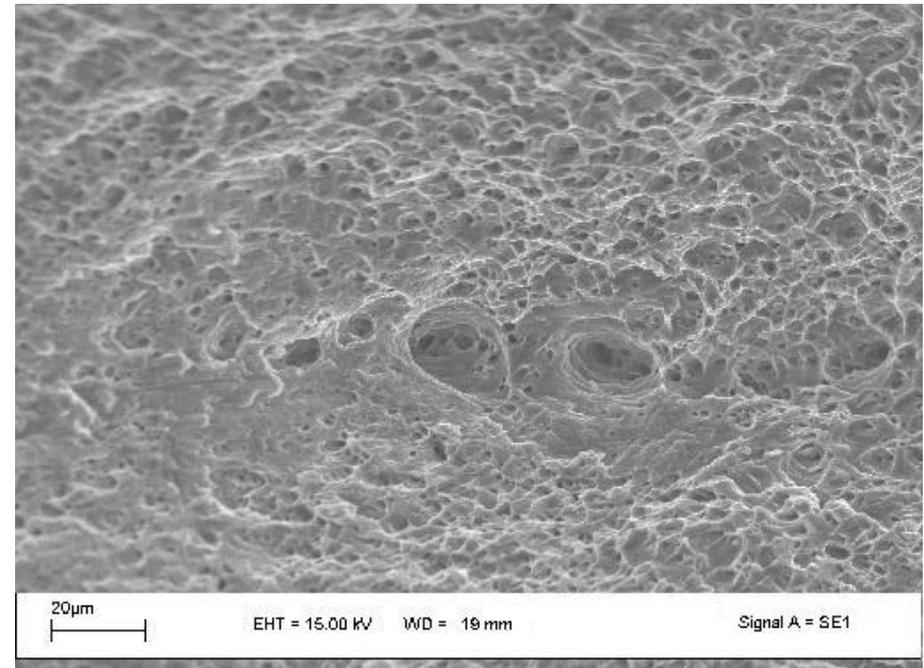
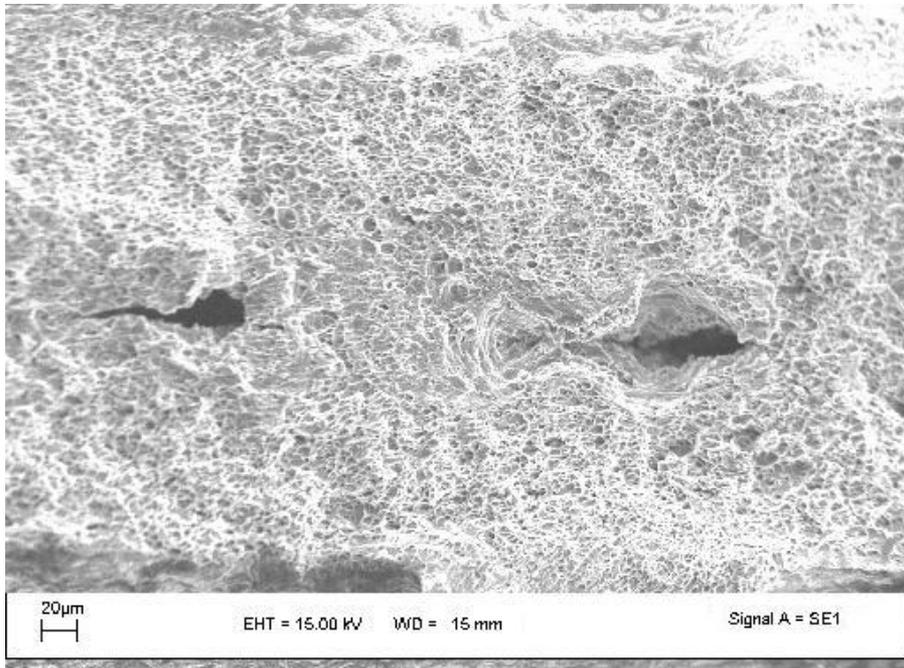


Mechanical properties along the rolling direction



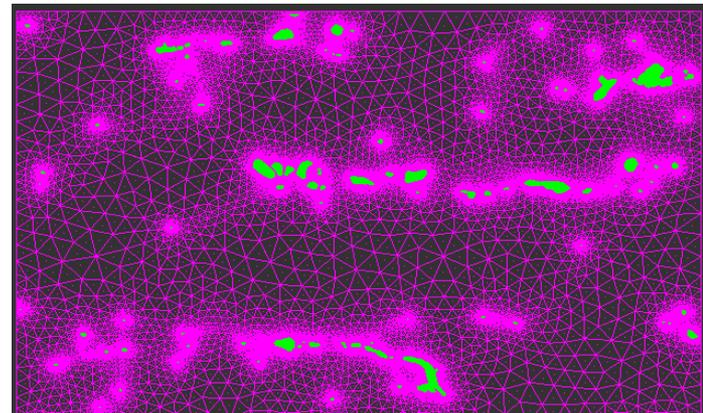
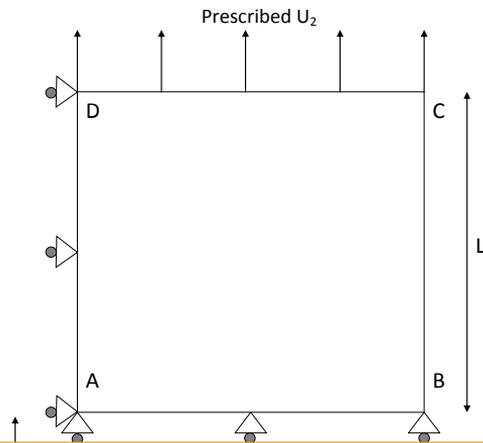
TRC has lower YS and UTS than TBC or DC

Fractographic investigation (TRC-I)



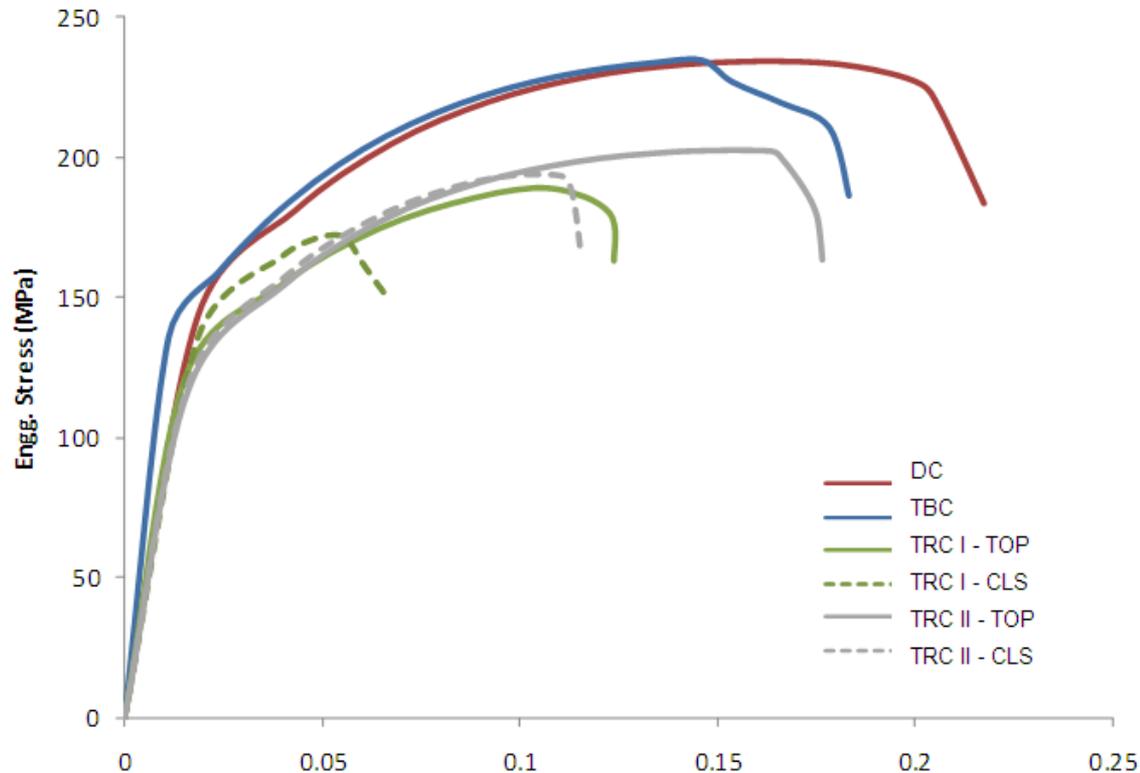
Microvoid formation at particle clusters

Microstructure based FEA



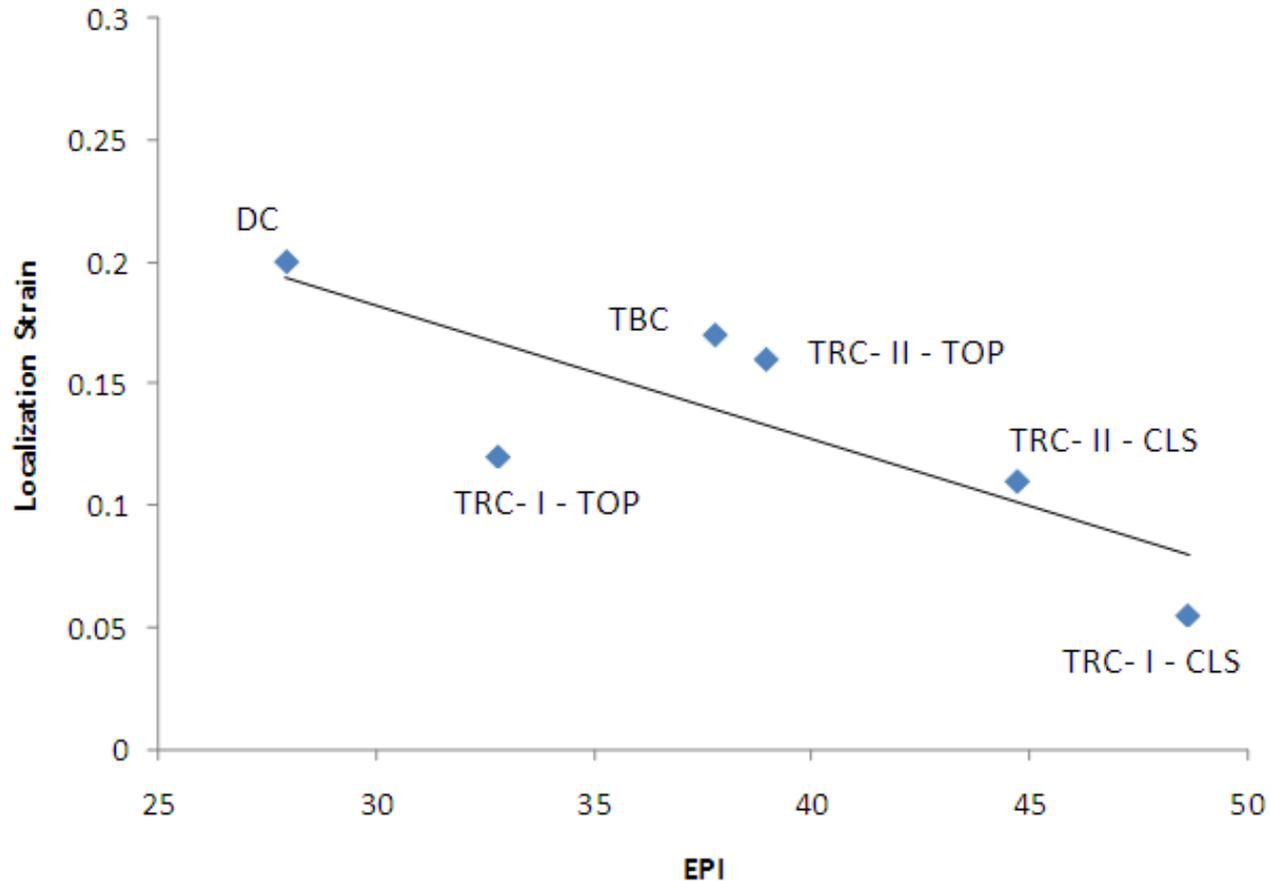
Modeling particles as intersecting ellipses is a good approximation

FE predictions of uniaxial stress-strain behavior



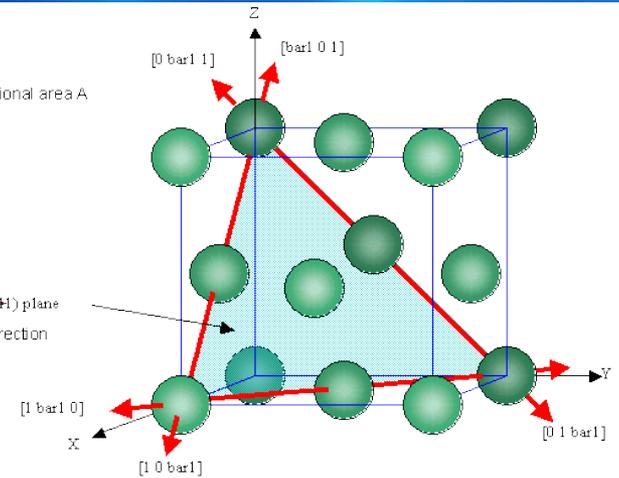
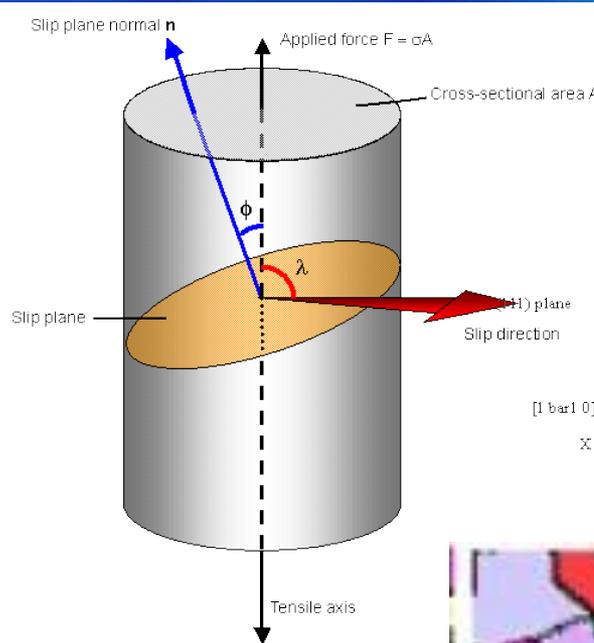
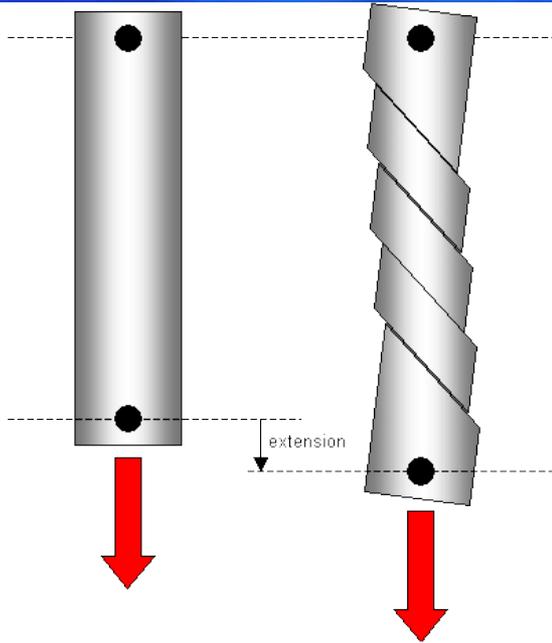
Novelis has higher localization strain than Assan
With in Assan, center region has lower localization strain than top

Correlation of localization strain and Extreme Property Index (EPI)



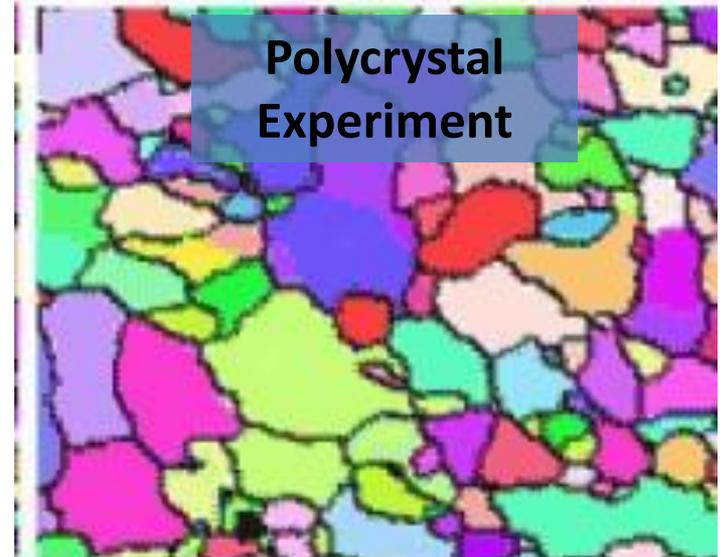
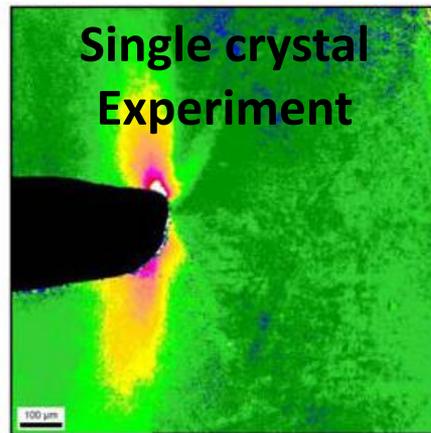
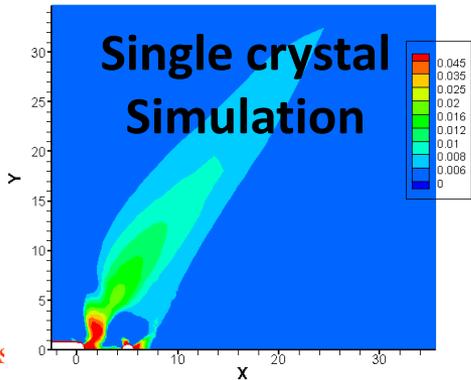
EPI is identified as a key microstructural attribute

Plastic deformation by slip

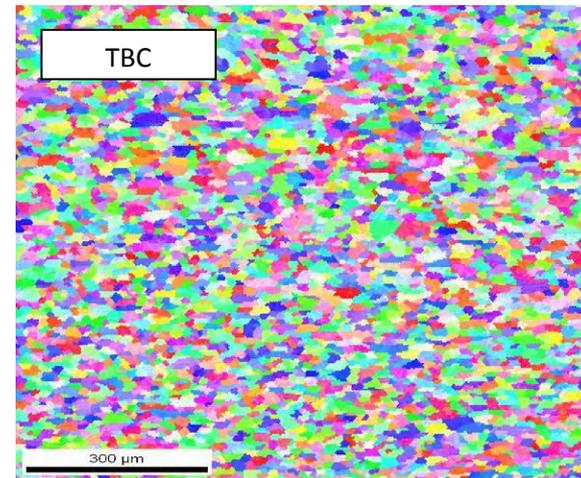
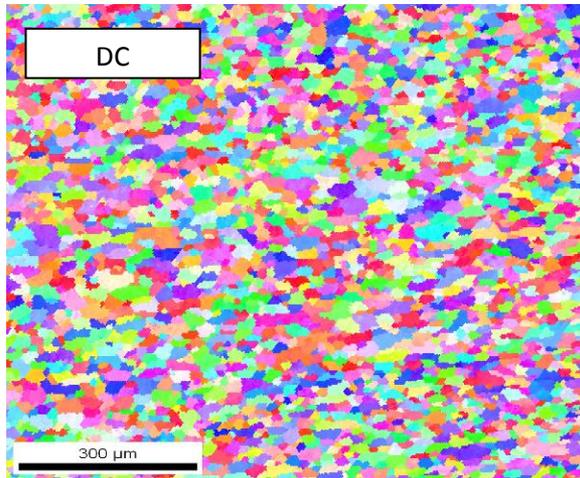


Unslipped single crystal fixed at top end.

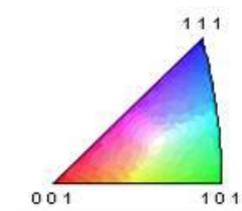
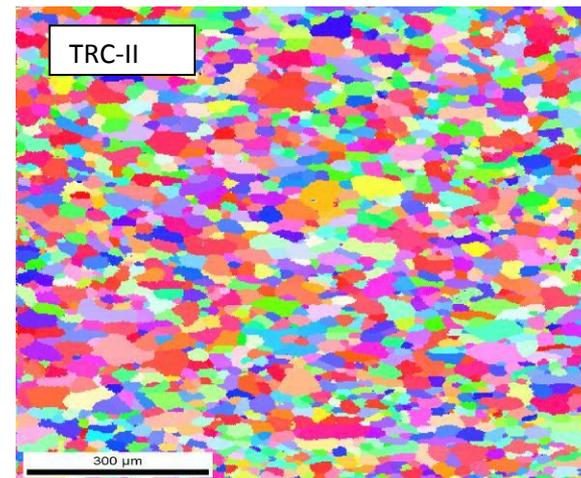
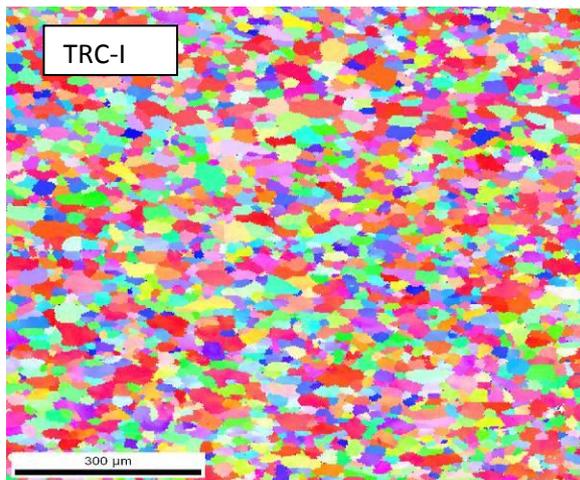
Single crystal after plastic deformation by tensile stress in the direction of the arrow. Slip occurs on distinct parallel planes.



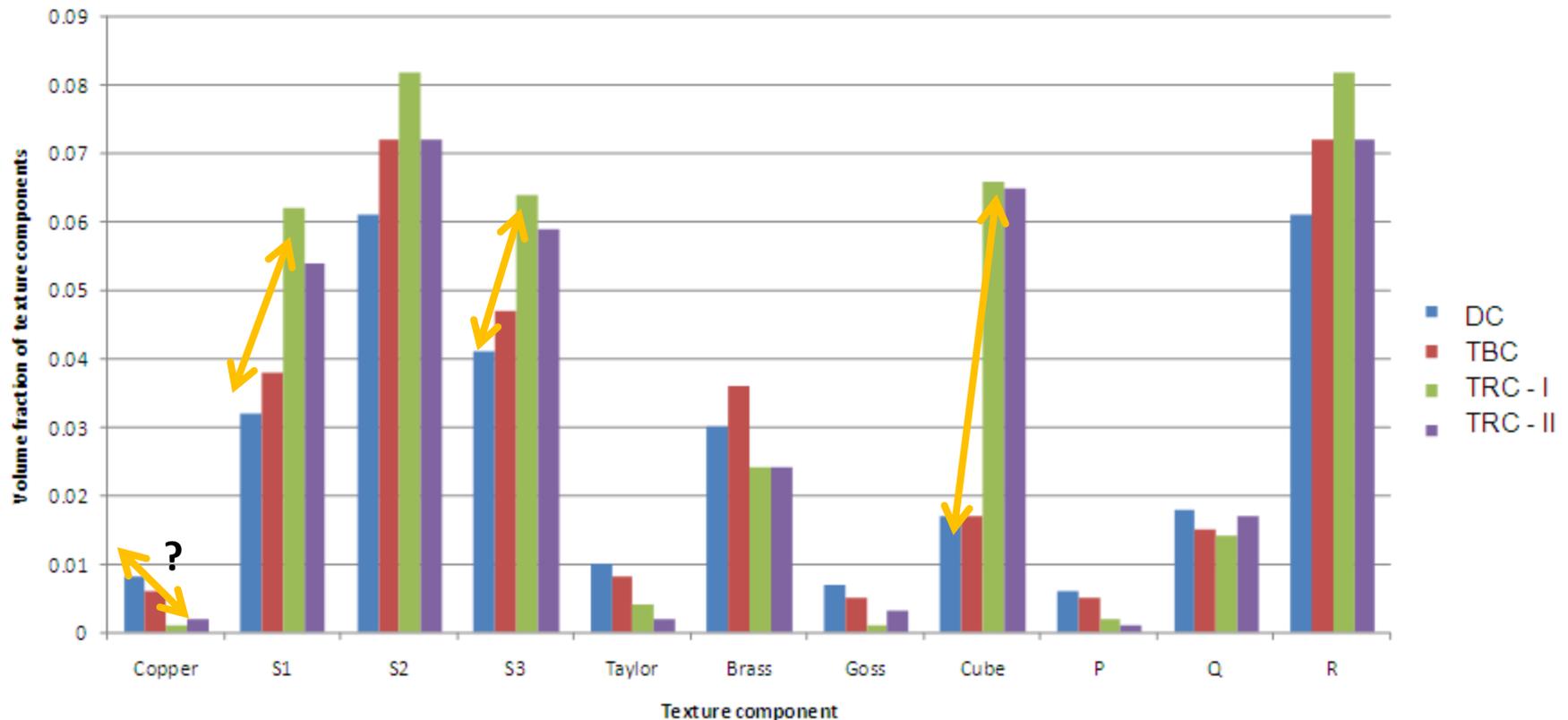
Inverse pole figure maps



Rolling Direction \rightarrow

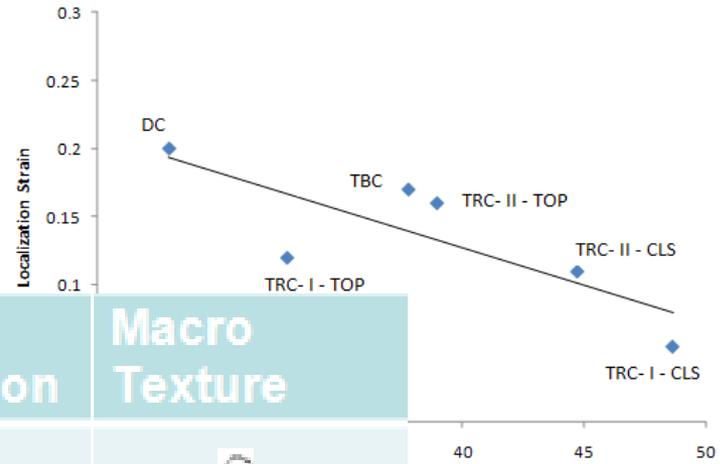
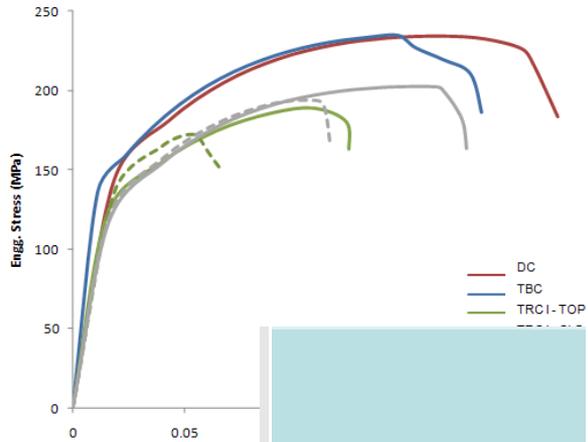


Fraction of various texture components

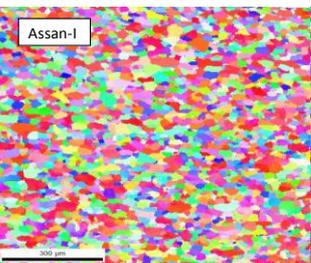
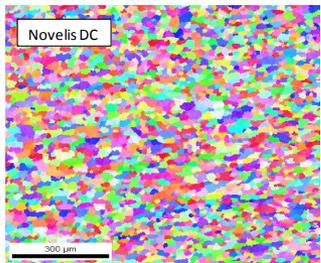


TBC has more rolling texture while TRC has more re-crystallization texture

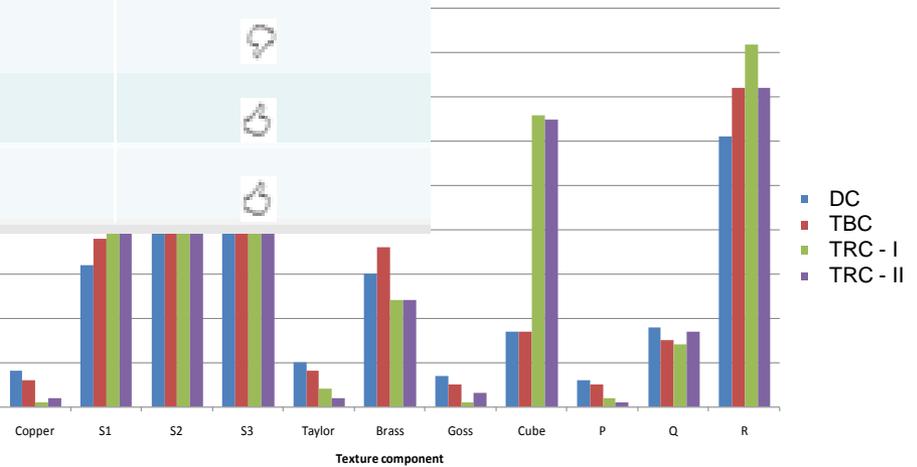
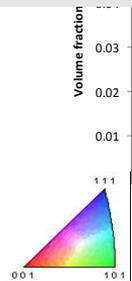
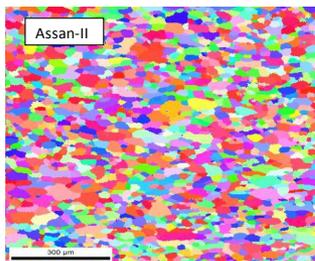
Summary



	Particle distribution	Macro Texture
DC		
TBCC		
TRCC-I		
TRCC-II		



Rolling Direction

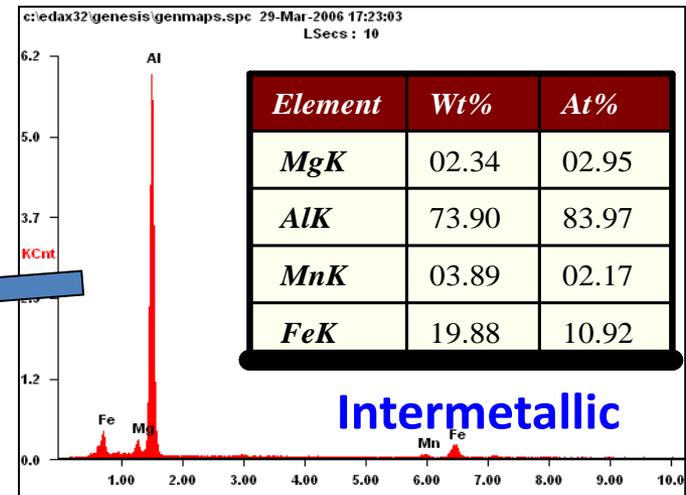
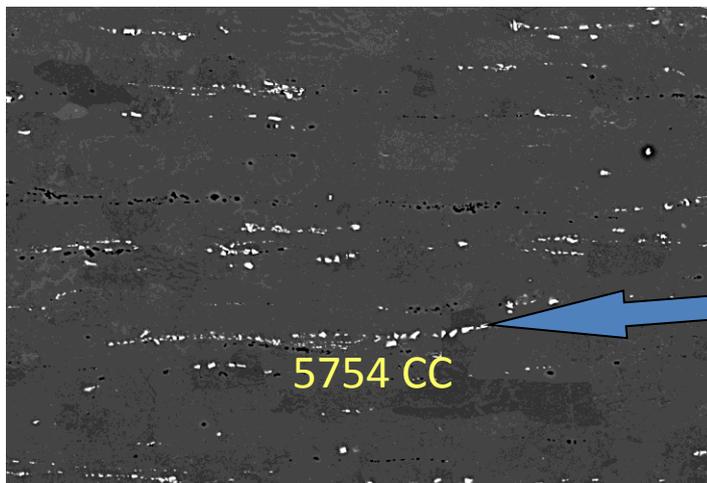


Case Study 3

Large scale formability simulations

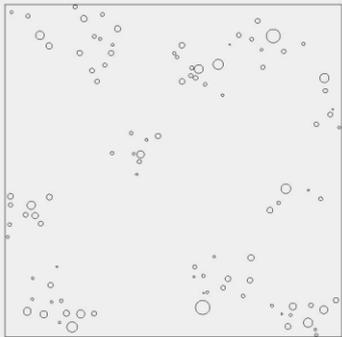
Microstructural features in 5754 Al

Alloy	Mg	Mn	Cr	Fe	Si	Cu	Al
DC	3.0	0.25	0.01	0.18	<0.1	0.01	Bal.
CC	3.1	0.25	<0.01	0.24	<0.1	0.02	Bal.

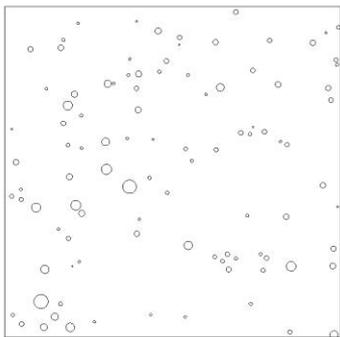


Effect of Spatial arrangement of second phase

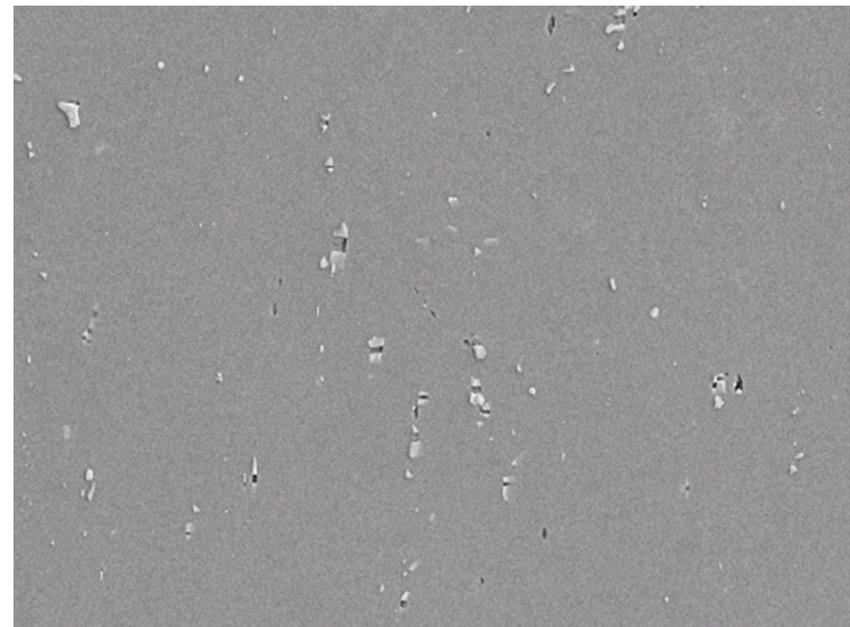
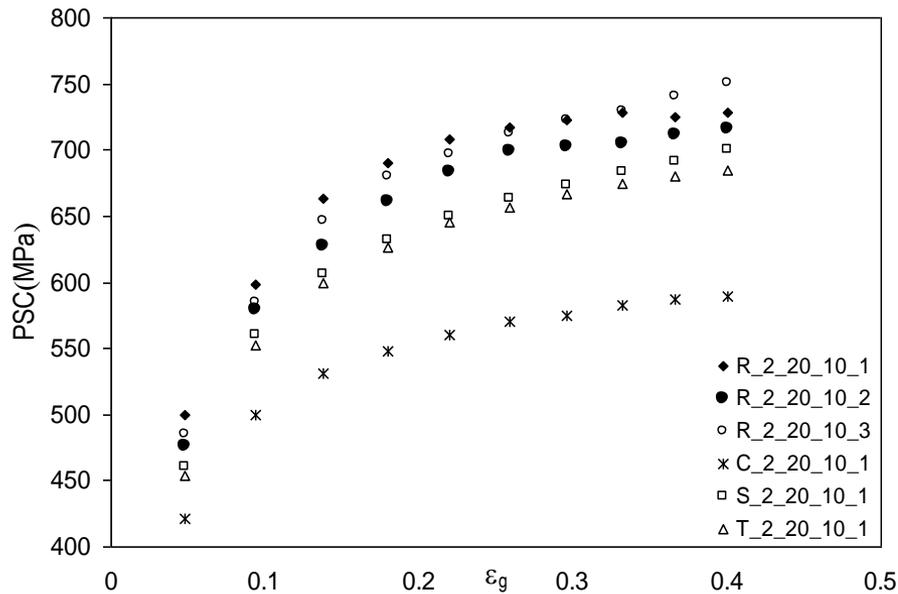
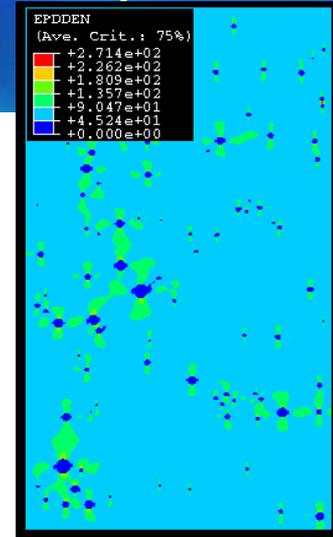
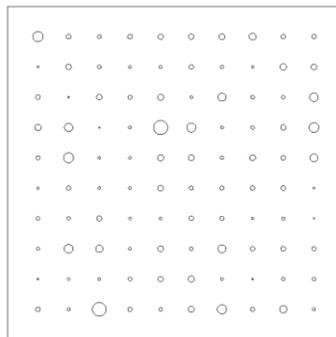
Clustered



Random

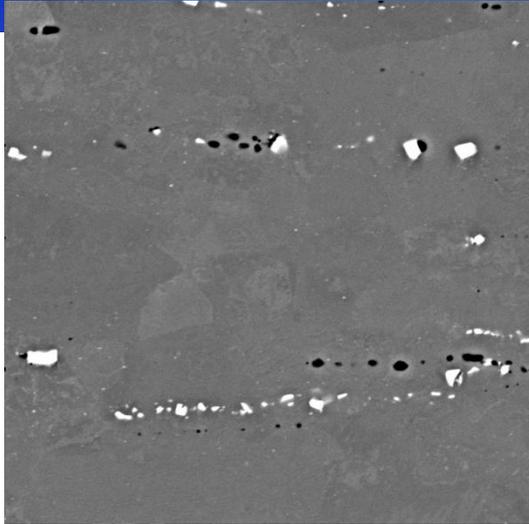


Ordered

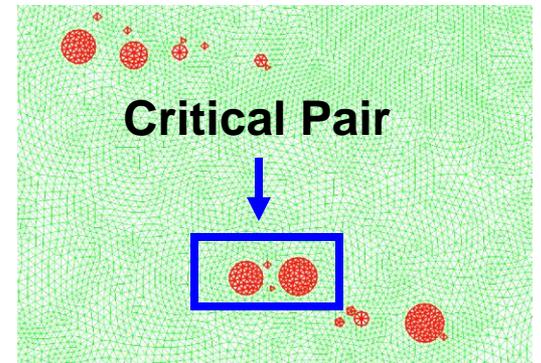
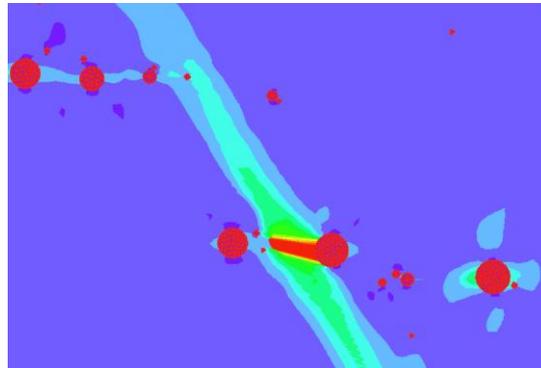
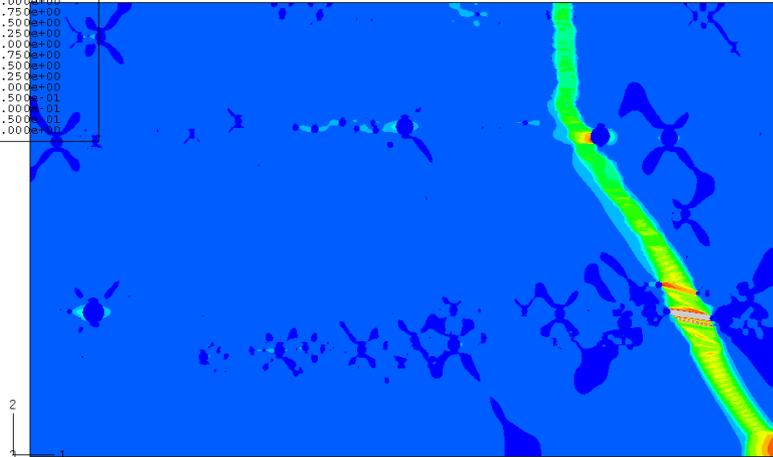
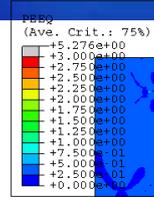
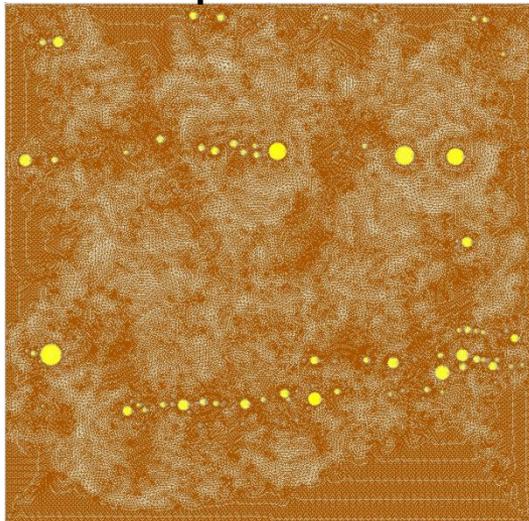


Virtual tensile test

Real Microstructure

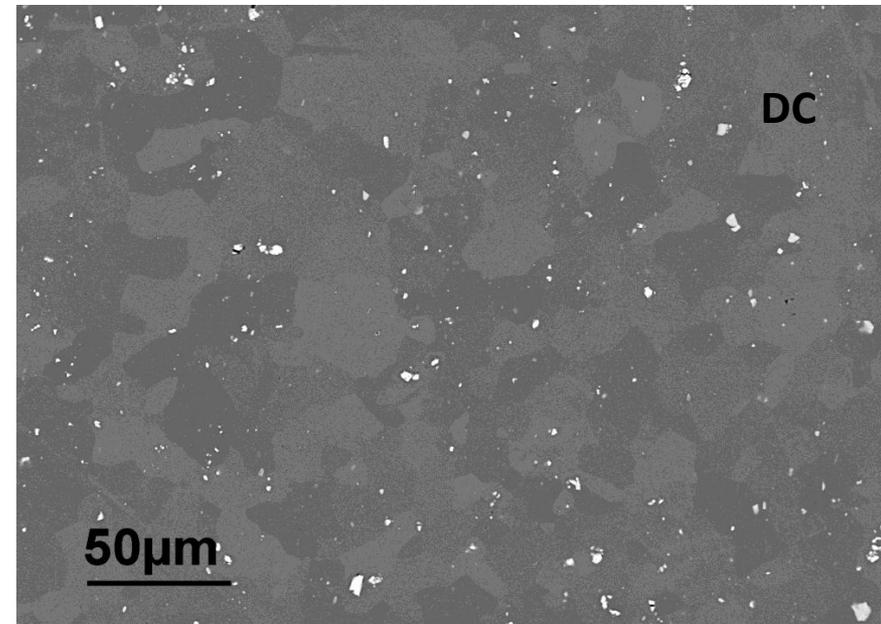
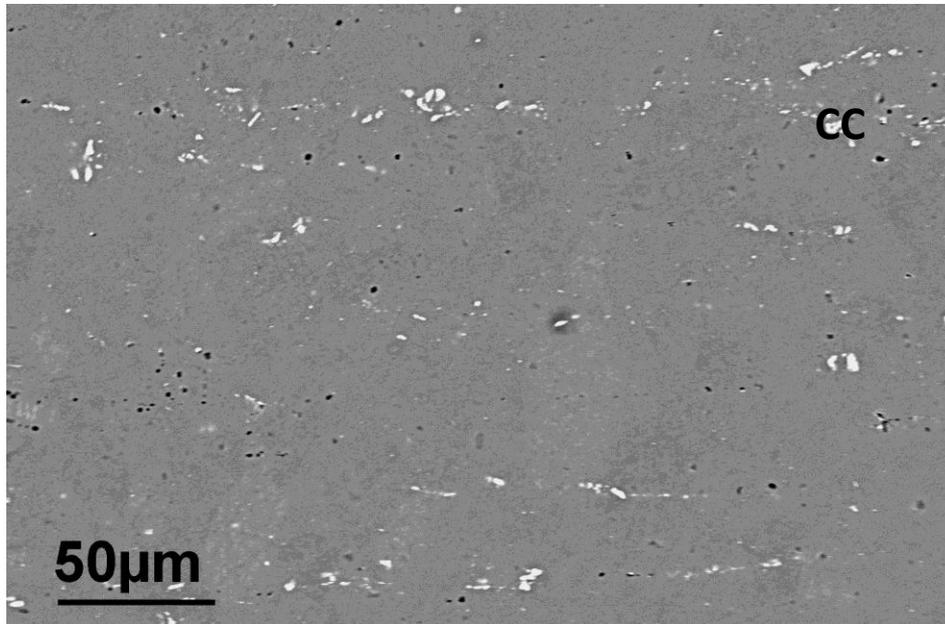


FE Representation



Comparison of DC vs CC alloy

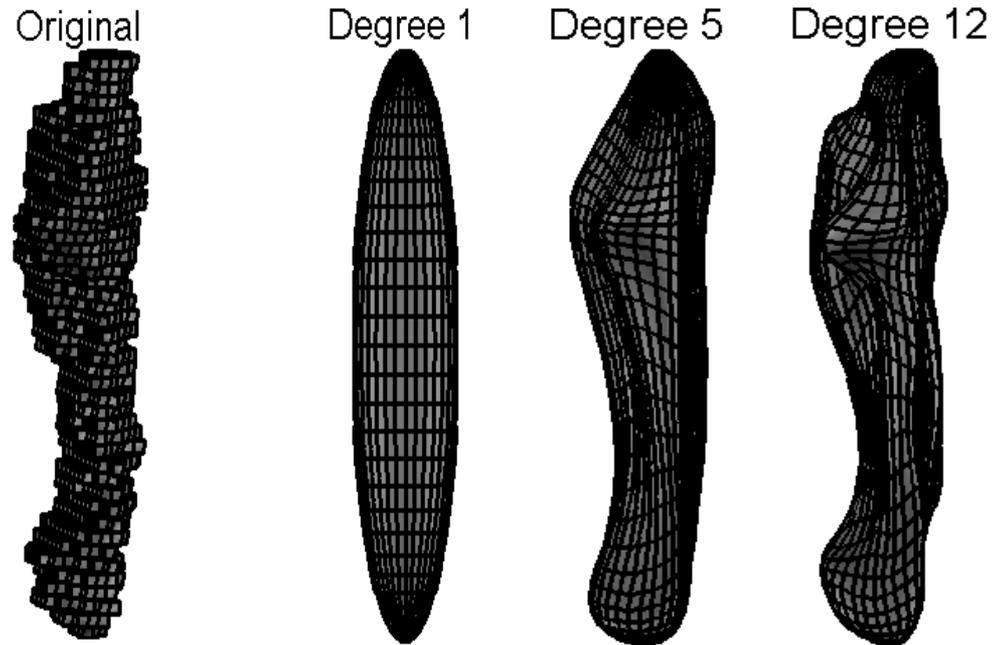
Alloy	V_V	$S_V (\mu\text{m})^{-1}$	$\lambda(\mu\text{m})$	$L_3 \mu\text{m}$
DC	0.0095 ± 0.0005	0.038 ± 0.002	104.6	1.01
CC	0.0095 ± 0.0010	0.045 ± 0.005	87.5	0.84



Vectorization approximation

- More emphases on spatial arrangement
- Partial shape parameterization
 - PCA
 - Distance transformation maps
 - SPHARM*

Orthonormal spherical harmonics of the solutions to Laplace's equation represented in spherical coordinates

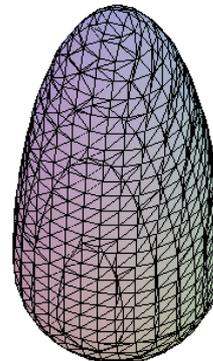
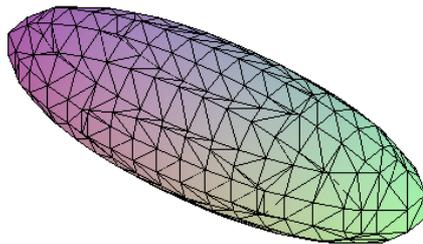
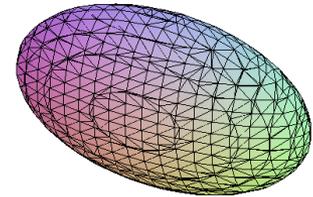
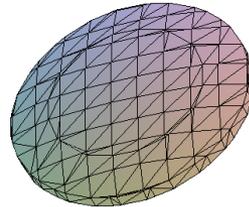
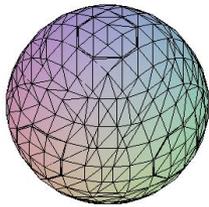


Ellipsoid

*L. Shen, J. Ford, F. Makedon, and A. Saykin, Intl Con Com Vis Patt Recog Img Proc, NC, 2003.

Ellipsoid shape approximation

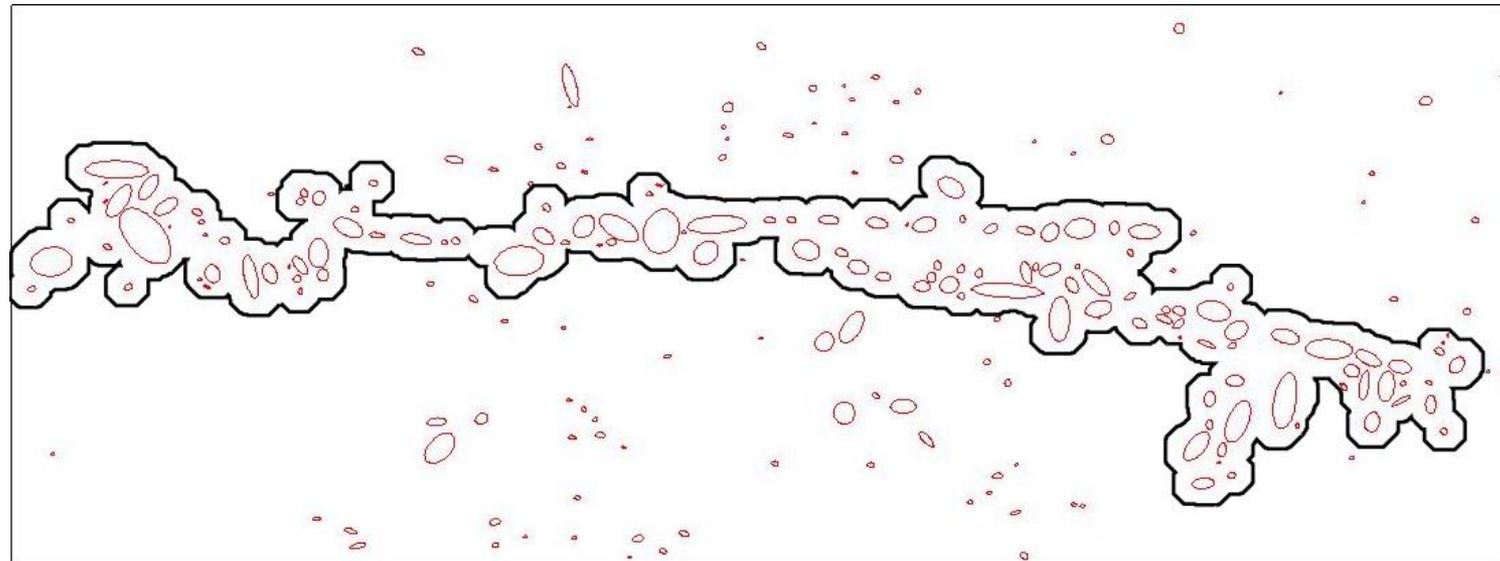
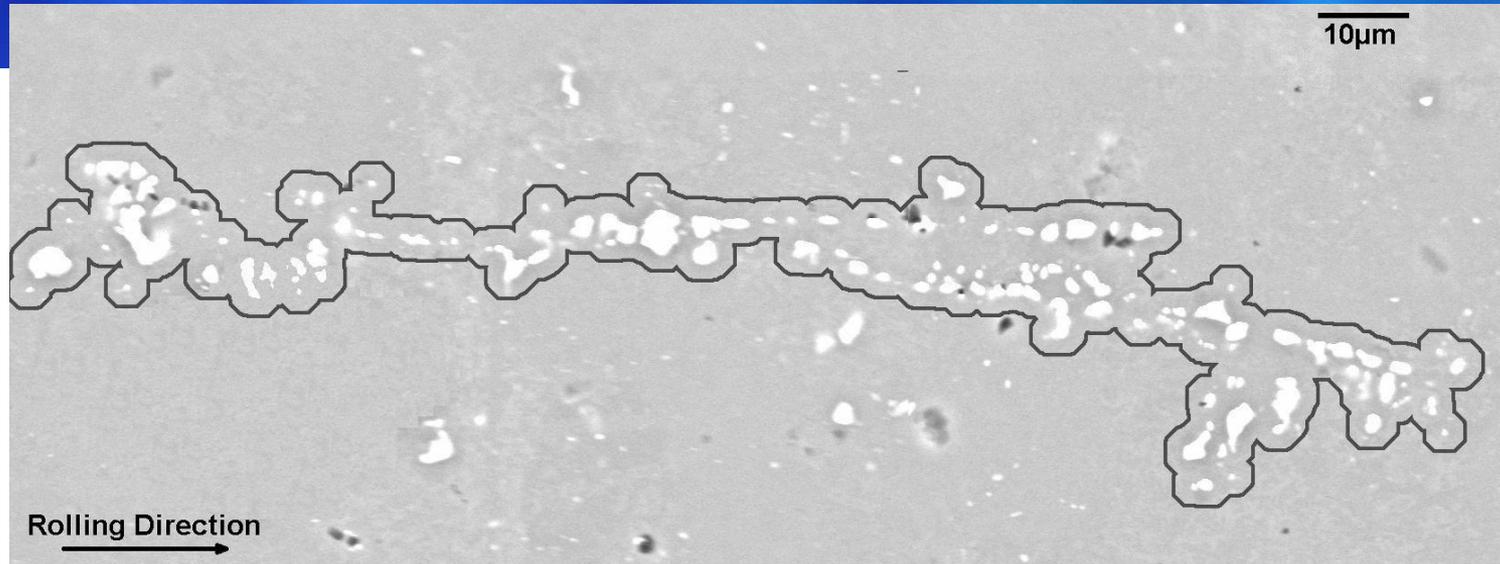
– Sphere, prolate, oblate, scalene, egg



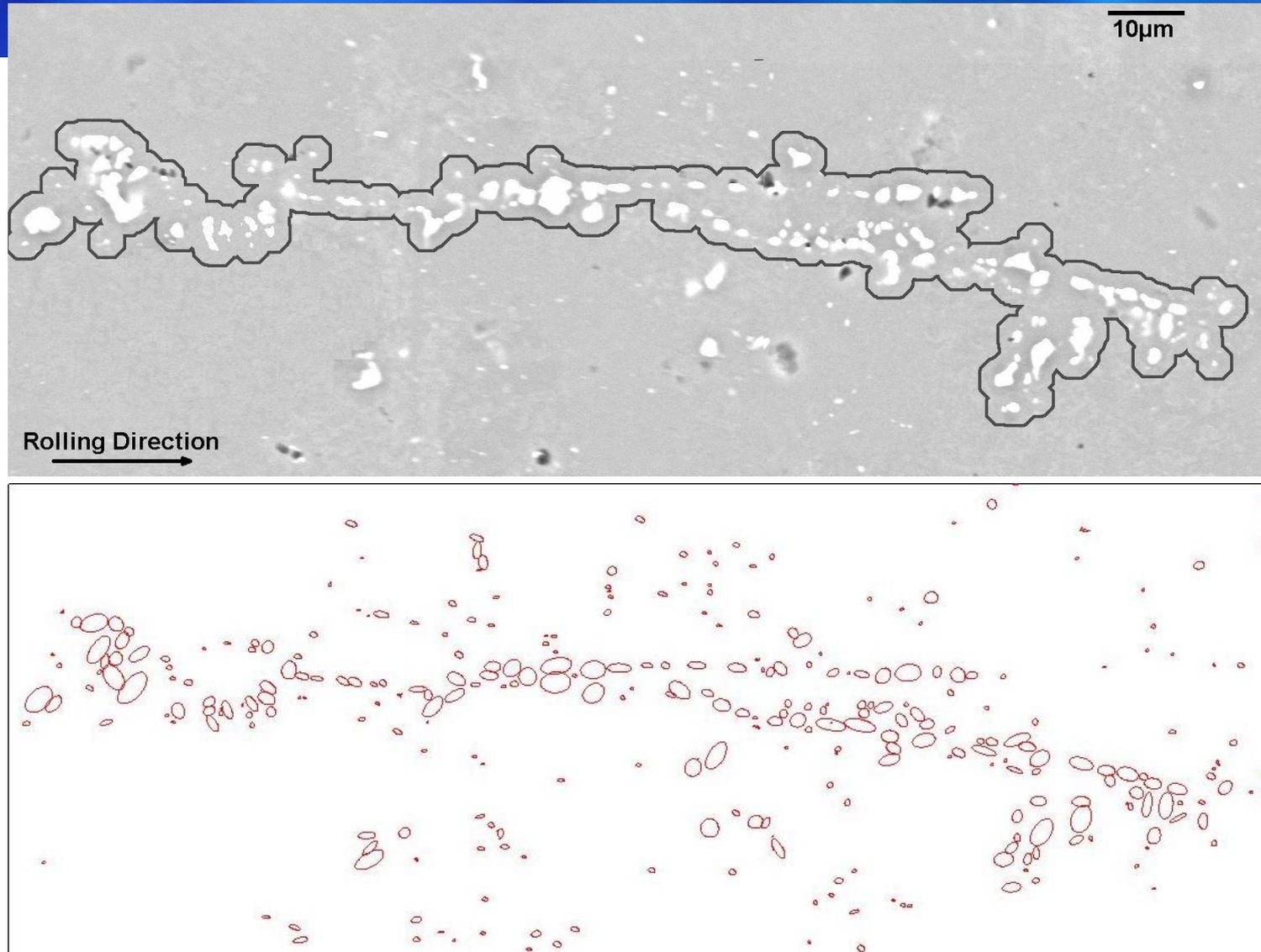
Ellipsoid shape approximation

Shape	Number of variables	Variables
Generalized ellipsoid	9	Centriod (h,k,l) Radii a, b, and c Euler angles ϕ_1, Φ, ϕ_2
Generalized spheroid	7	Centriod (h,k,l) Radii a and b Angles θ and ϕ
Axisymmetric Spheroid	6	Centriod (h,k,l) Radii a and b Angles θ
Sphere	4	Centriod (h,k,l) Radii a

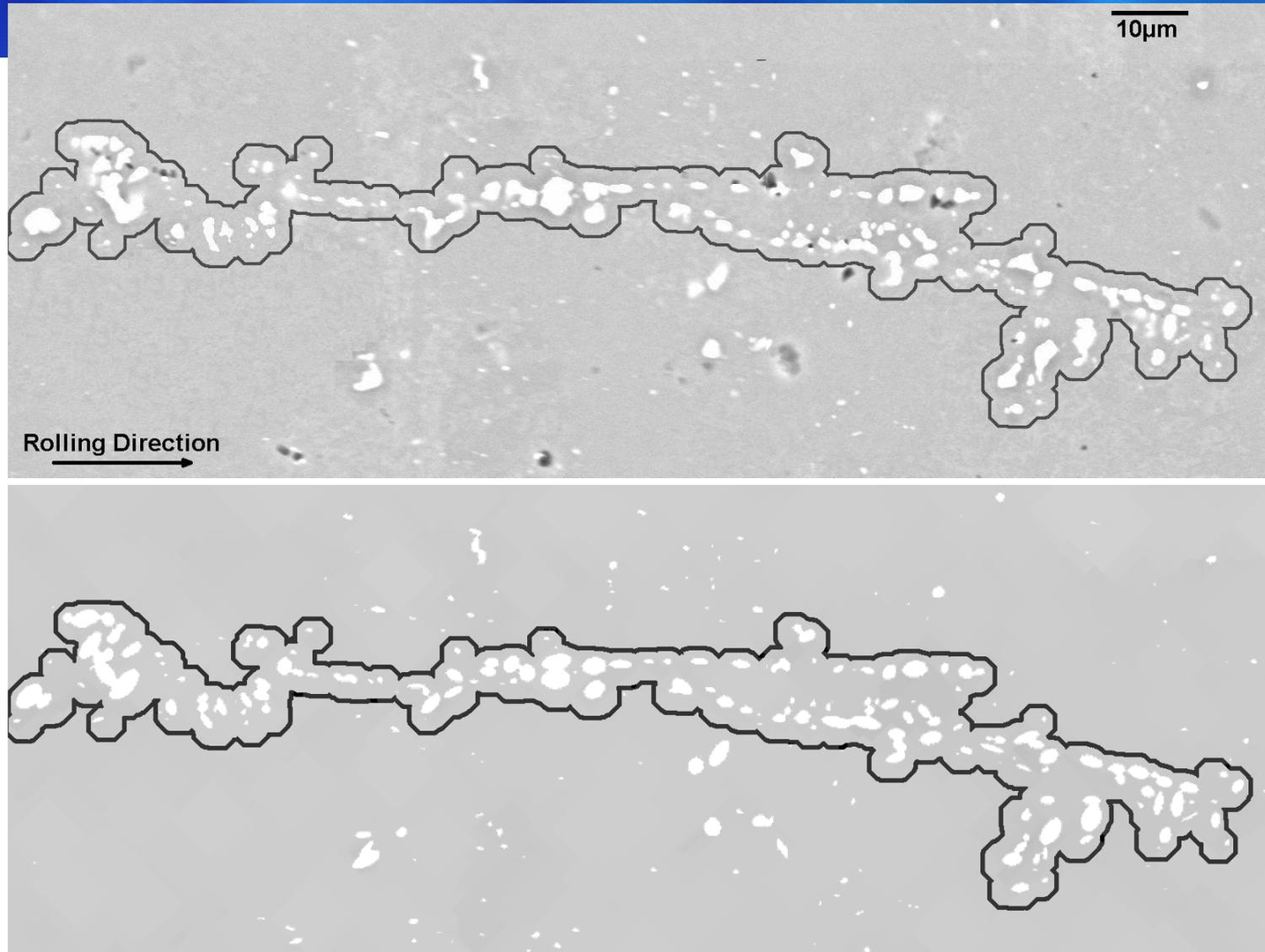
2D vector image



2D vector image



2D vector image



Intrinsic Volumes

- Minkowski Functions

$$W_k(Y) = \frac{b_d}{b_{d-k}} \int_{L_k} \nu_{d-k}(P_s \perp Y) U_k(dS)$$

d+1 intrinsic volumes in d dimensional space

In \mathbb{R}^3

W_0, W_1, W_2, W_3

Hadwiger theorem

All additive, motion-invariant, and continuous functions of convex sets are linear combinations of these four characteristics.

For \mathbb{R}^d this can be written as

$$h(Y) = \sum_{k=0}^d a_k W_k(Y)$$

Extension to convex rings

Convex Ring A

$$A = \bigcup_{i=1}^n Y_i \text{ for } Y_i \in C(K)$$

$$W_K(A) = \frac{b_d}{b_{d-k}} \int_{L_k} \int_S \chi(A \cap Ss) \nu_{d-k}(ds) U_k(ds)$$

Location and orientation transformation

- Eulerian rotation and translation

$$\mathbf{E} = \mathbf{Z}_2 * \mathbf{X}_1 * \mathbf{Z}_1 * \mathbf{T} * \mathbf{X}$$

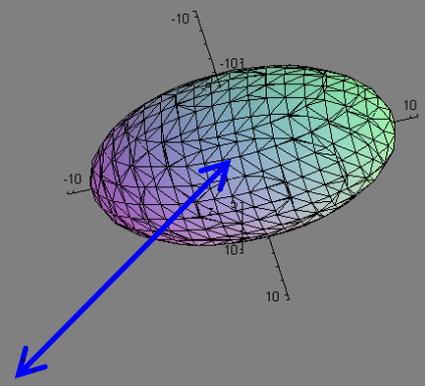
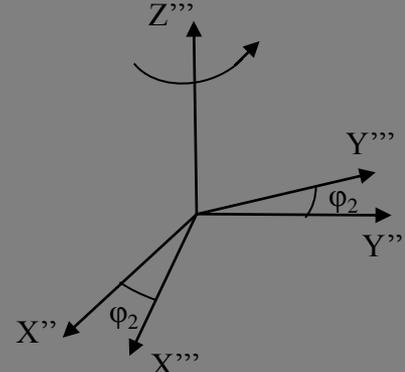
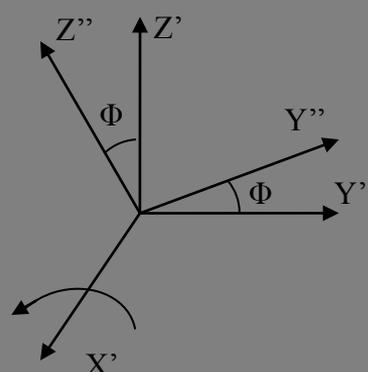
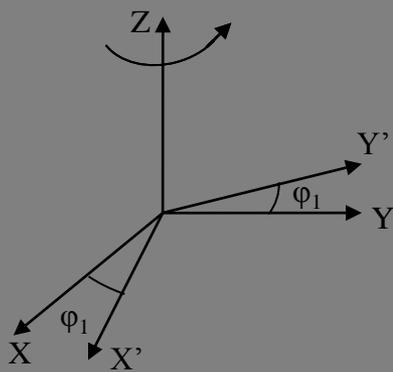
$$\mathbf{E} = \begin{bmatrix} e1 \\ e2 \\ e3 \\ 1 \end{bmatrix} \quad \mathbf{X} = \begin{bmatrix} x \\ y \\ z \\ 1 \end{bmatrix}$$

$$\mathbf{Z}_2 = \begin{bmatrix} \cos \phi_2 & \sin \phi_2 & 0 & 0 \\ -\sin \phi_2 & \cos \phi_2 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{X}_1 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos \phi & \sin \phi & 0 \\ 0 & -\sin \phi & \cos \phi & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{Z}_1 = \begin{bmatrix} \cos \phi_1 & \sin \phi_1 & 0 & 0 \\ -\sin \phi_1 & \cos \phi_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

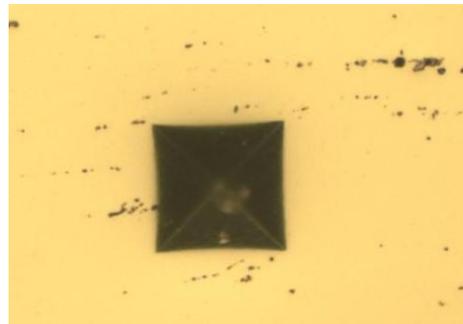
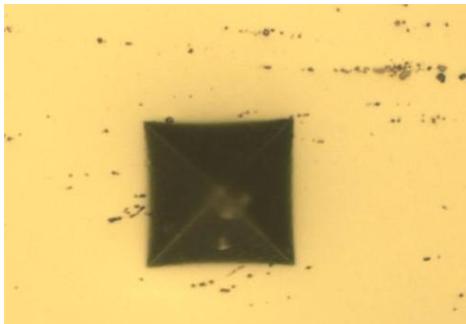
$$\mathbf{T} = \begin{bmatrix} 1 & 0 & 0 & -h \\ 0 & 1 & 0 & -k \\ 0 & 0 & 1 & -l \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



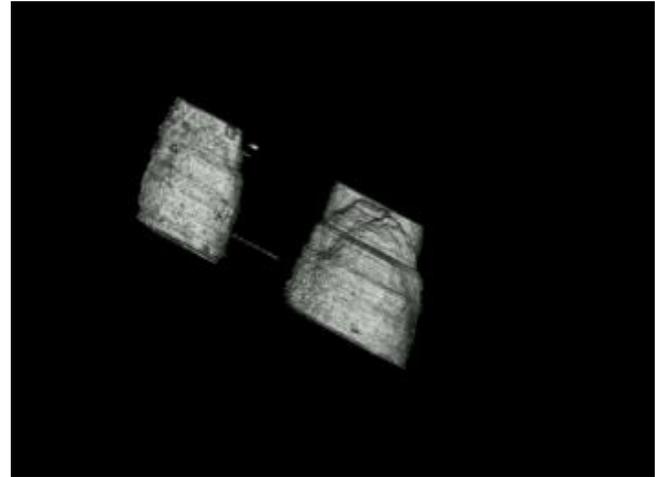
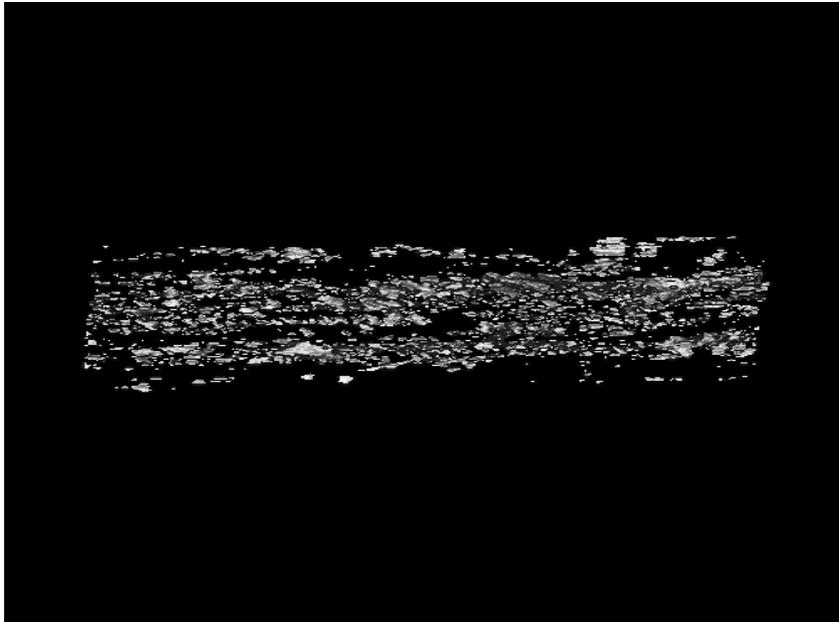
True 3D microstructural reconstruction

Serial sectioning

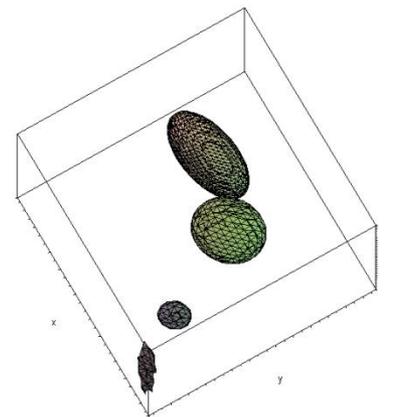
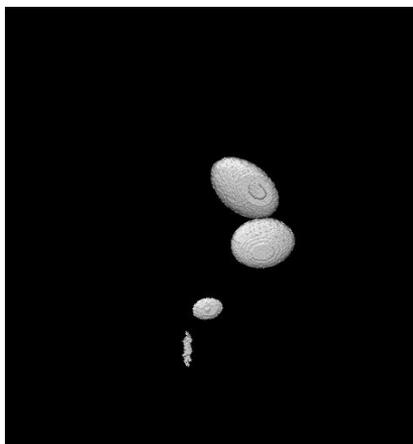
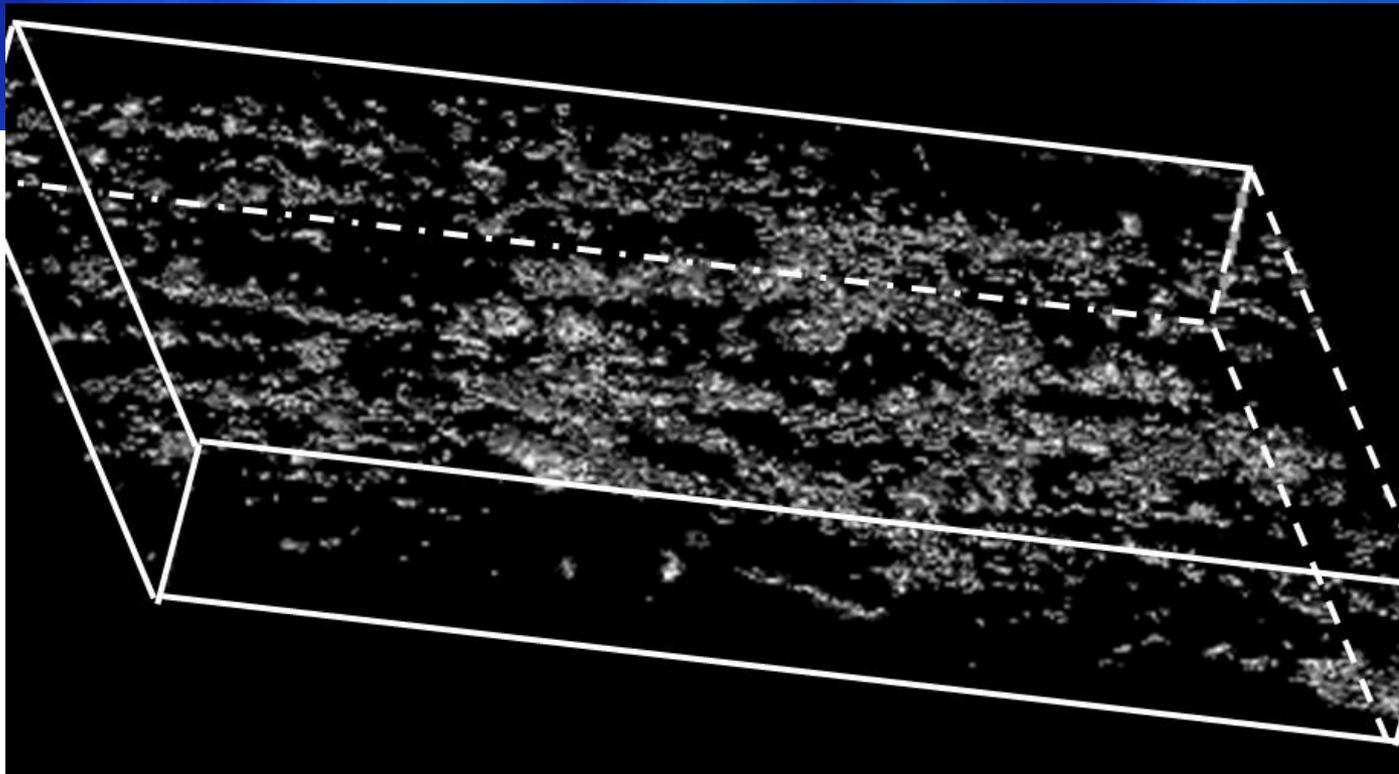
- Micro hardness indents
- Section alignment (Affine transform)
- 3D rendering



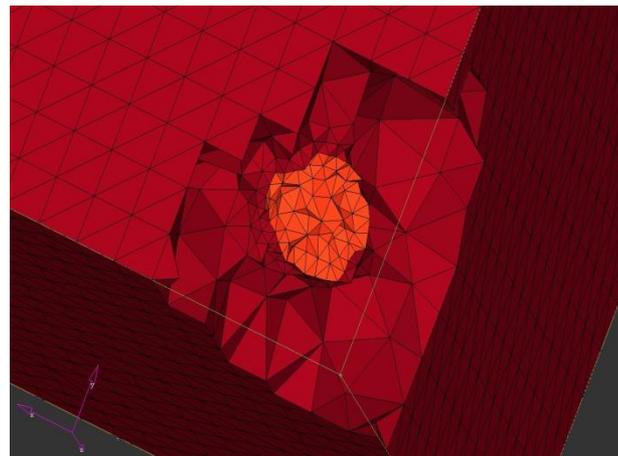
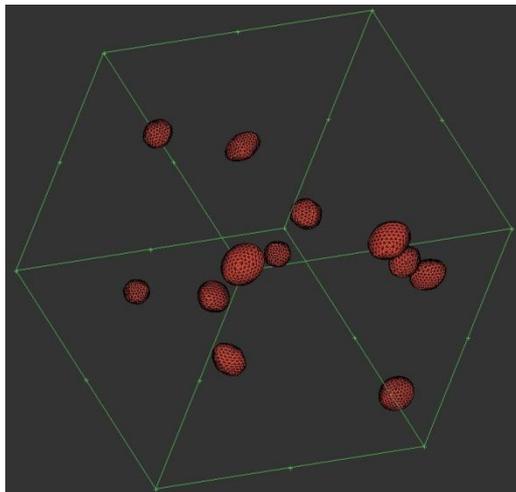
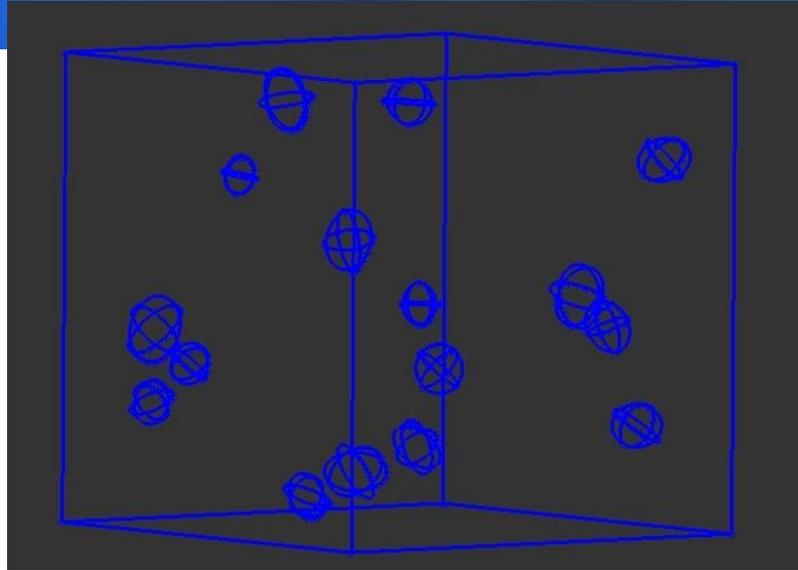
3D voxel data



3D Vectorized Image



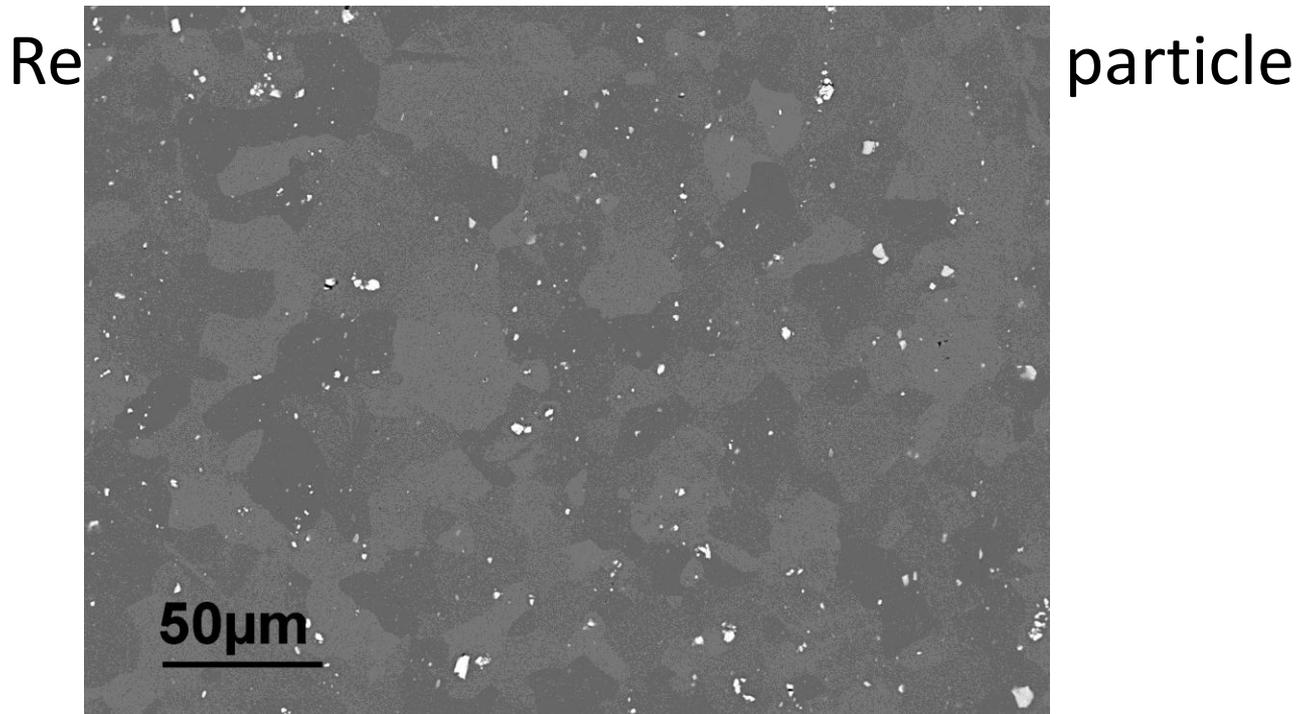
3D Graded FE mesh



Typical microstructure

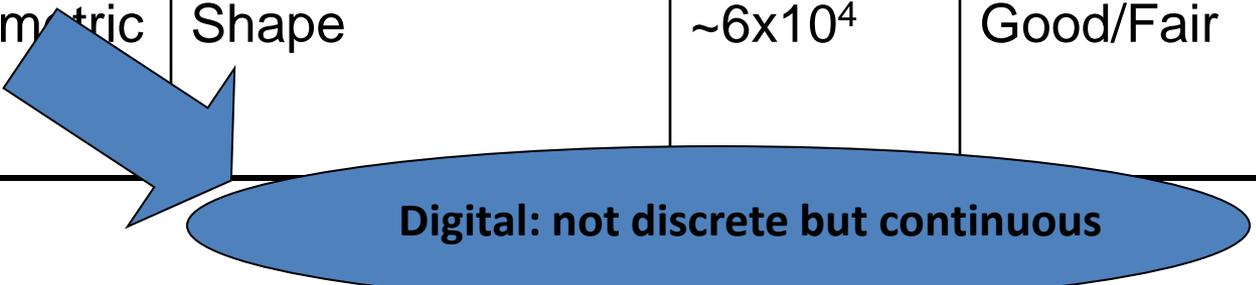
- Particle size $\sim 1 \mu\text{m}$
 - $\lambda \sim 100 \mu\text{m}$

Simulation size: $(200 \mu\text{m})^3$



FEM Model size

Technique	Assumptions	Size	Data recovery
Brute force	None	$\sim 5 \times 10^8$	Perfect
Autocorrelation	Hilbert space Stationarity	$\sim 5 \times 10^8$ *	Good
Eigenvalue space	Hilbert space	$\sim 10^6$	Not possible
Vectorized geometric primitives	Shape	$\sim 6 \times 10^4$	Good/Fair



Digital: not discrete but continuous

Summary

- Spatial arrangement of second phase play an important role in plastic localization
- Intersecting ellipsoids form Convex rings (extension of convex sets)
- Reduction of storage by ~ 4 orders
- Automated graded mesh generation

Future Directions

- Incorporation of other geometric primitives
- Parameterization of grains by four dimensional Poisson polyhedrons (and ordered texture triplets)
- Preserves three intrinsic volumes in 3D

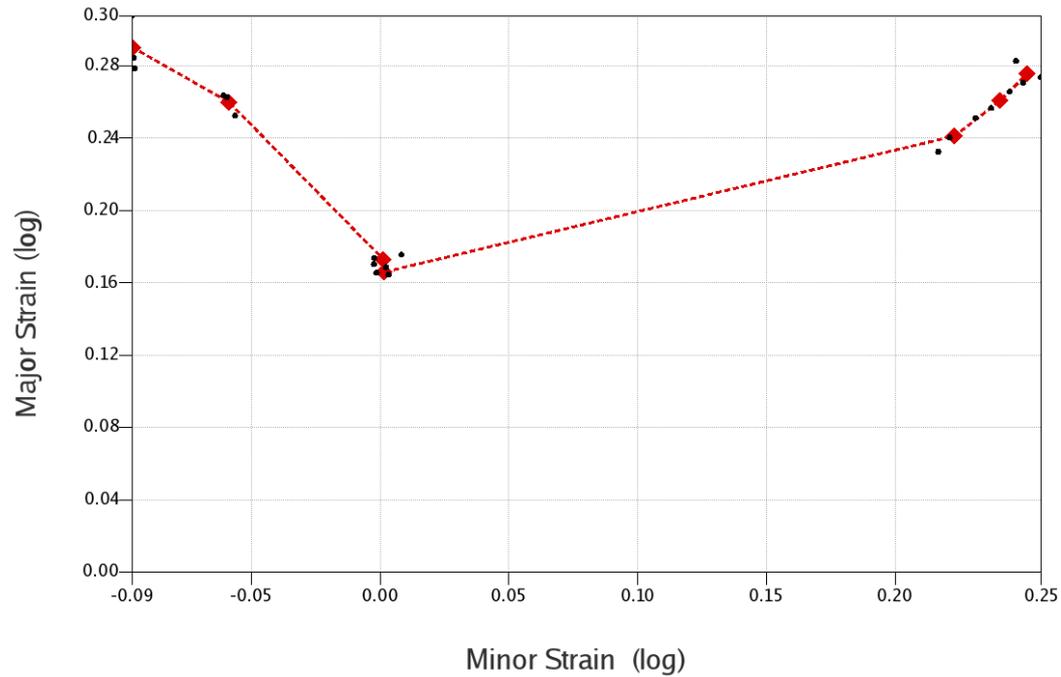
Future is Digital but not discrete

- Modeling with meshless and finite point methods

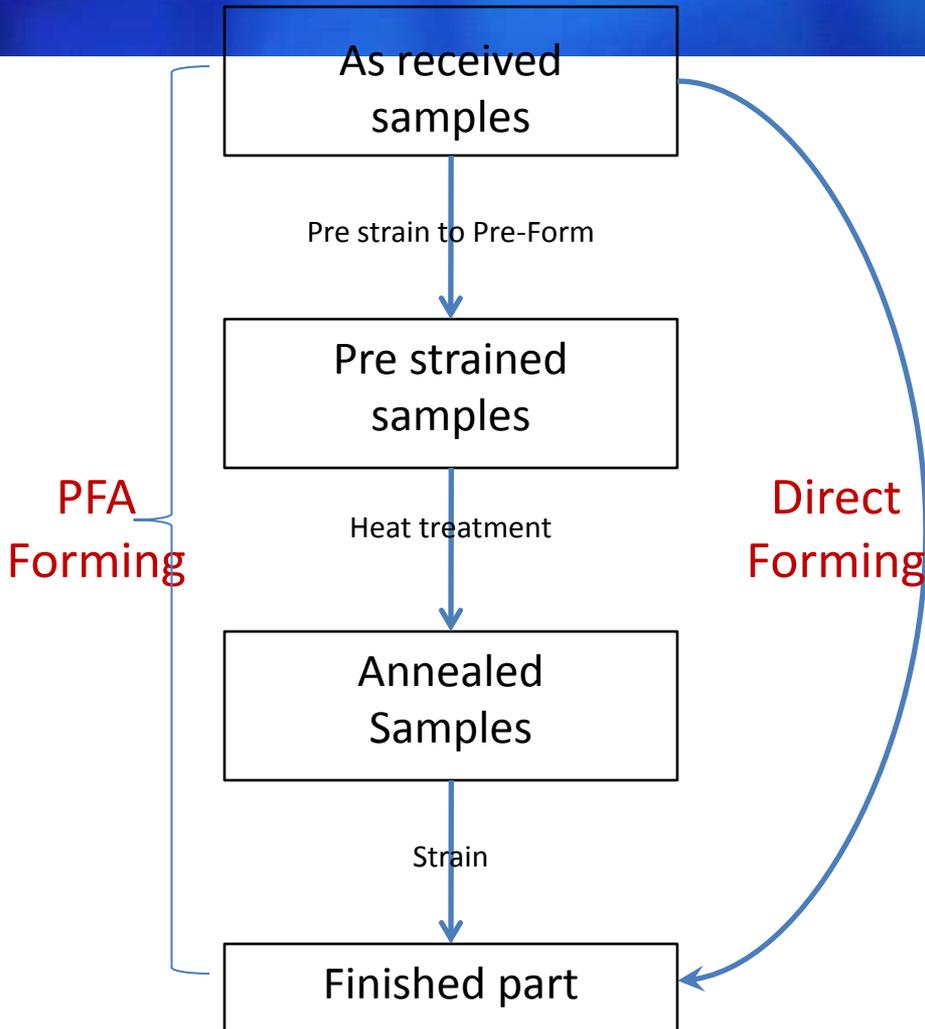
Case Study 4

Nano structure modification using pre-form annealing

Experimental FLD (AA 6061)

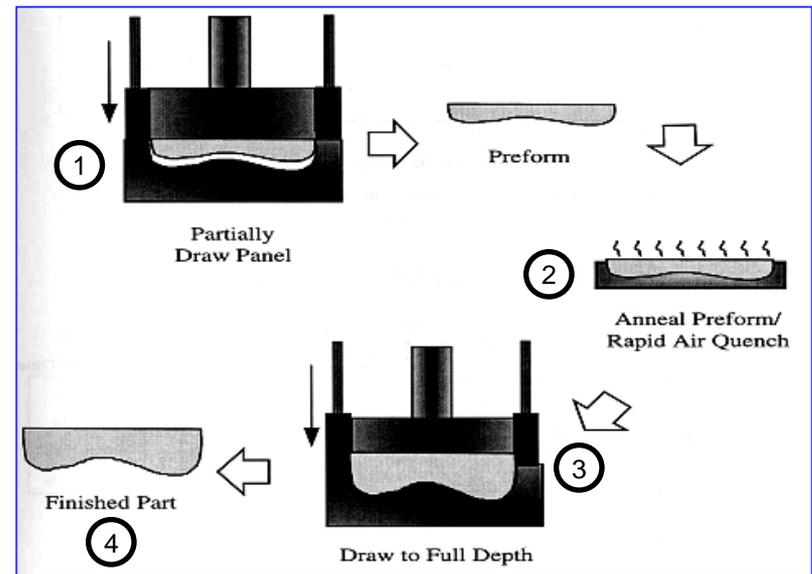


PFA Technology for Al 5000 series

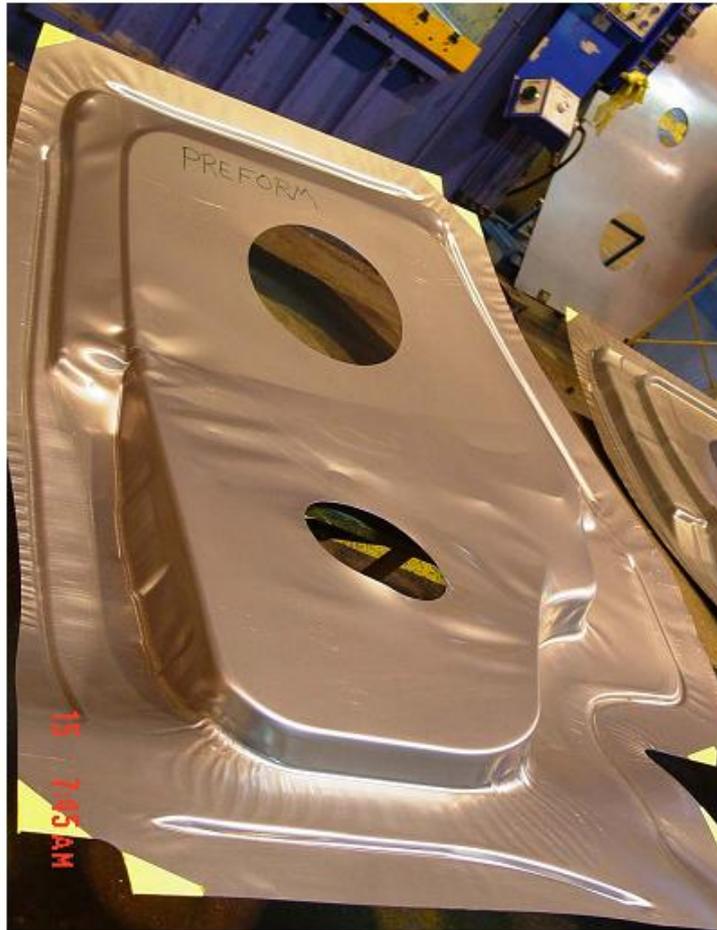


Heat Treatment:

- Direct Forming (1 and 4)
- PFA (Pre-Form Annealing) Forming (1, 2, 3 and 4)



Pre-Form Annealing of Door Inner of SUV

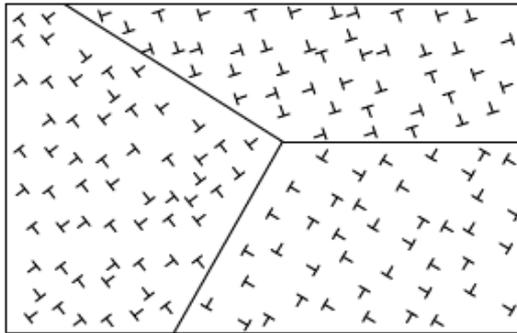


Theresa Lee et. al. SAE Int , 2006

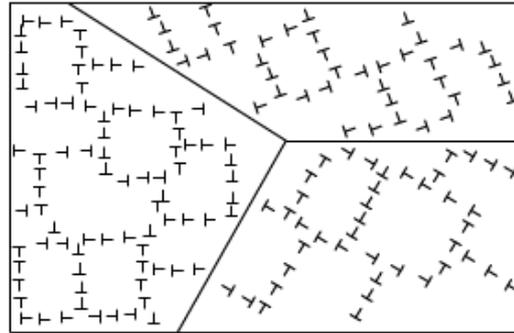
Scientific challenges

- Multiple-precipitate variants
- Multiple precipitation pathways
- Various states of coherency
- Role of dislocation landscape on thermodynamics and kinetics of precipitates
- Simultaneous recovery and precipitate overaging
- Early recrystallization

Recovery



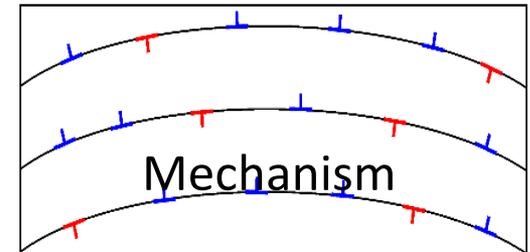
After straining



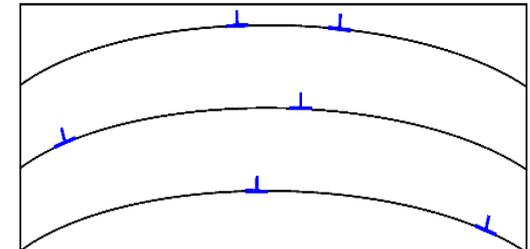
Annealing
After straining

Process to reduce the total number of dislocations by:

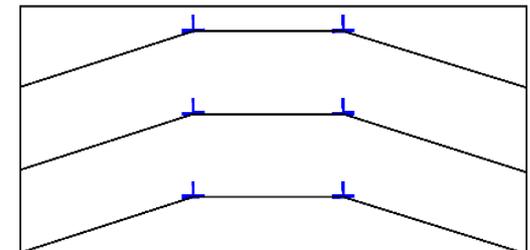
- Annihilation
- Re-arrangement into lower energy configuration/s



a) Bent lattice with dislocations of both sign



b) Annihilation of dislocations with opposite sign



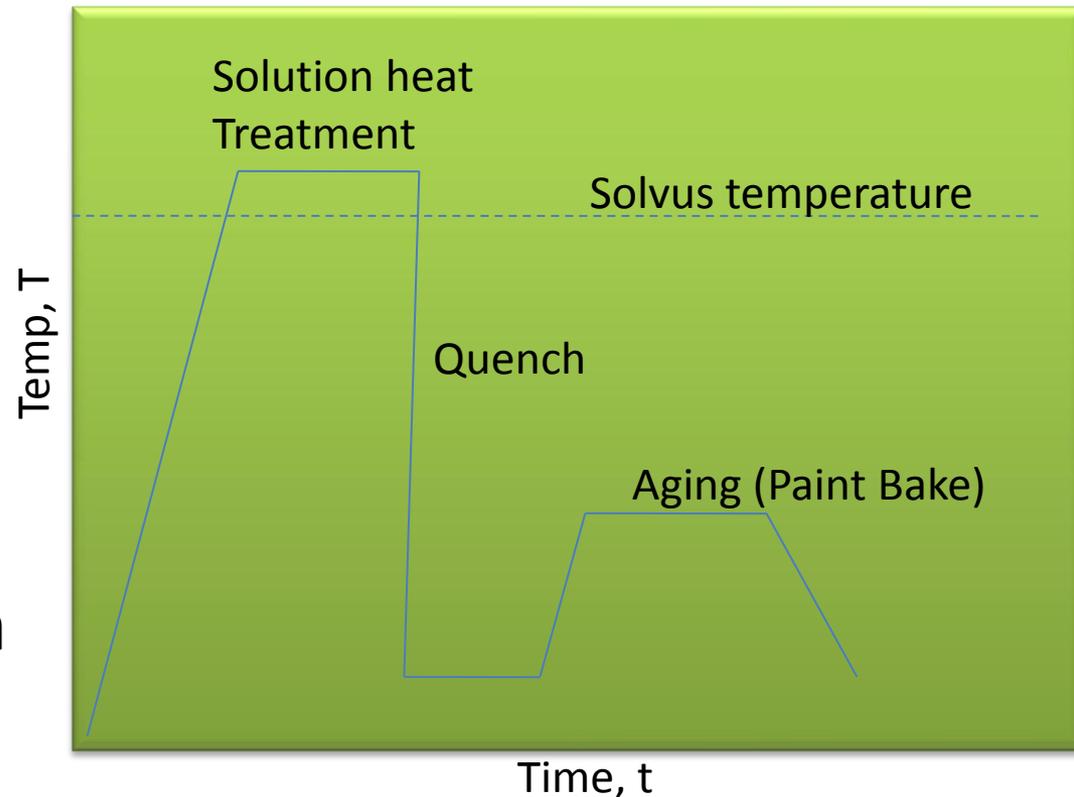
c) Polygonization of the lattice



Precipitation hardening

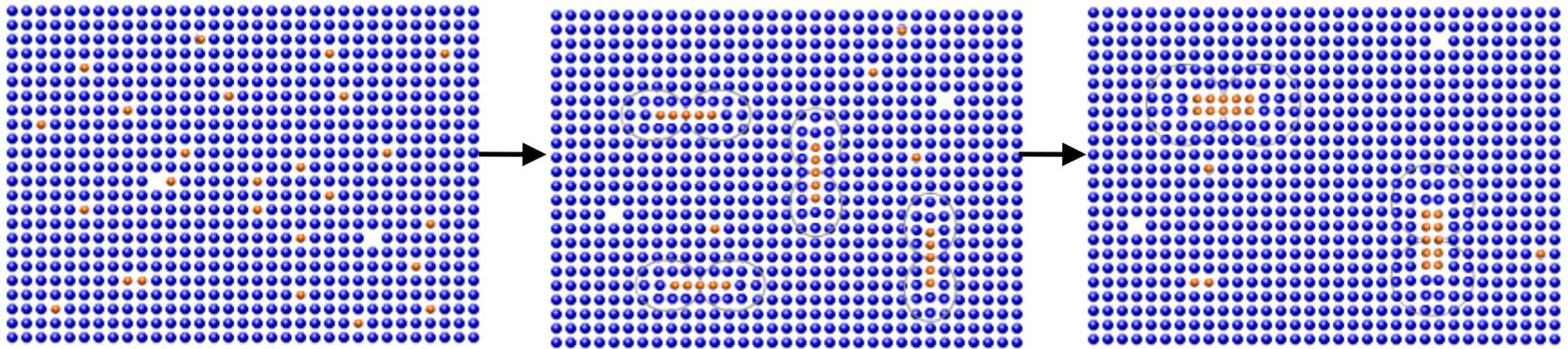
3 step heat treatment:

- Solution heat treatment, to dissolve the alloying elements
- Quenching, to form SSSS
- Aging, the controlled decomposition of the supersaturated solid solution (SSSS) to form a fine dispersion of precipitates

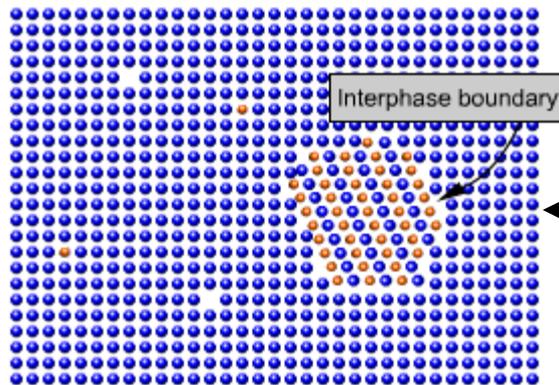


Microstructure Development: Aging

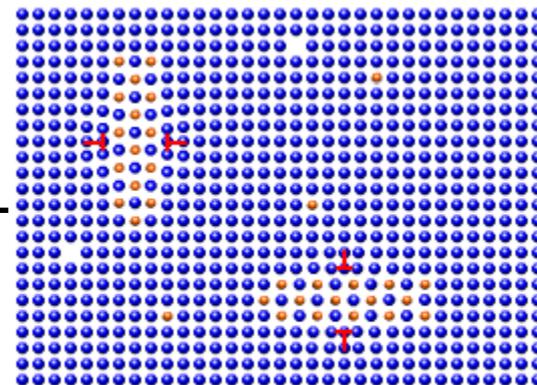
Coherent Precipitates



A • B •



A • B •



A • B •

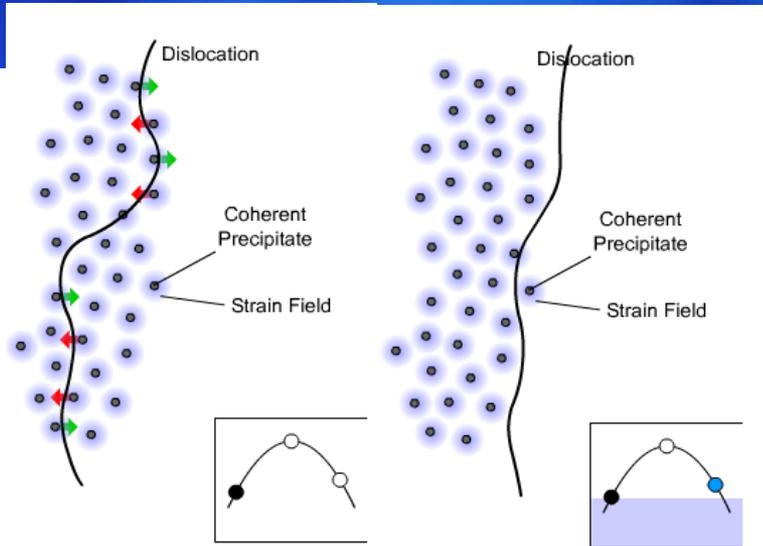
Incoherent Precipitates

A • B •

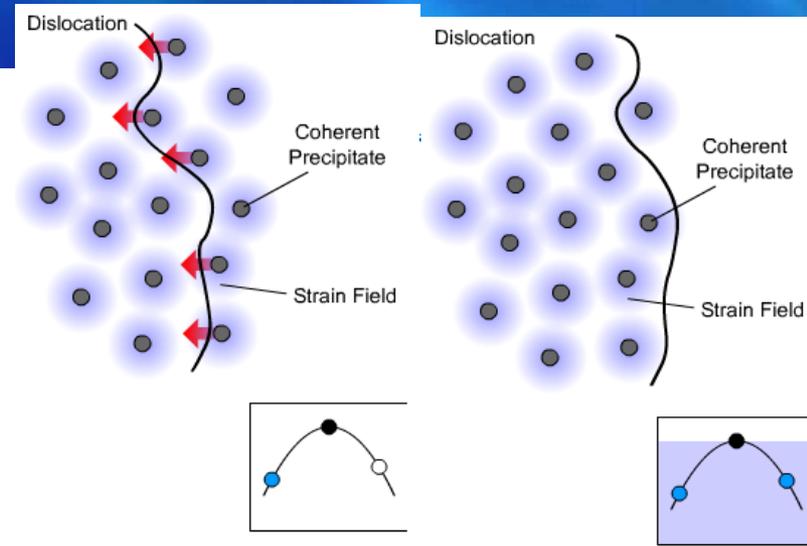
A • B •

Semi-coherent Precipitates

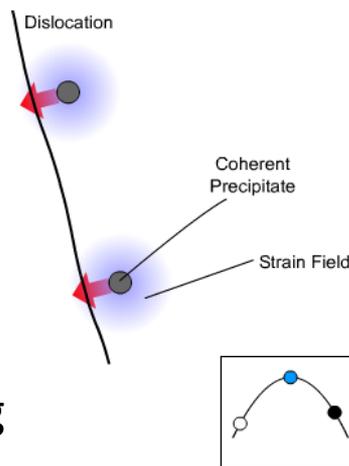
Strengthening Process



1. Fine Zone Spacing



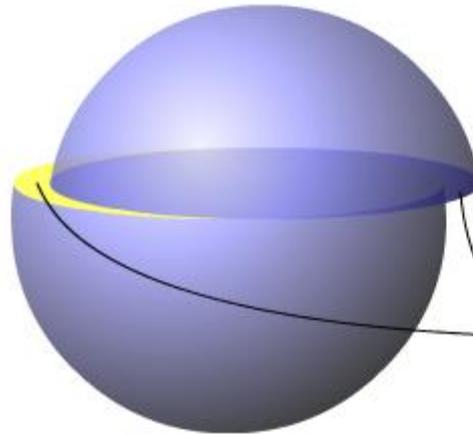
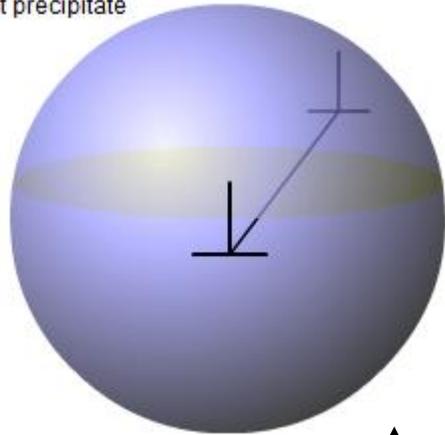
2. Medium Zone Spacing



3. Coarse Zone Spacing

Strengthening Process

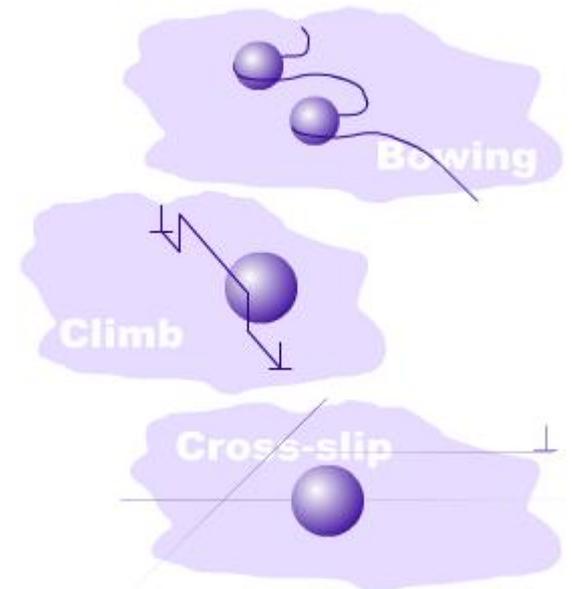
Coherent precipitate



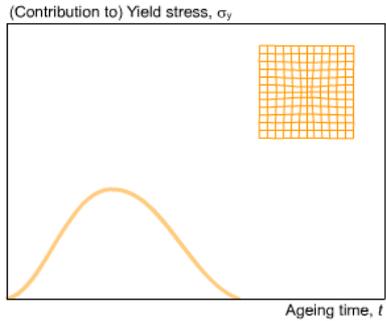
New interfacial areas

Chemical hardening

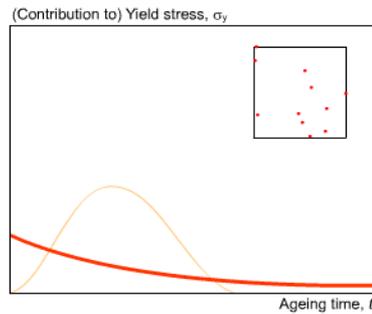
Dispersion Hardening



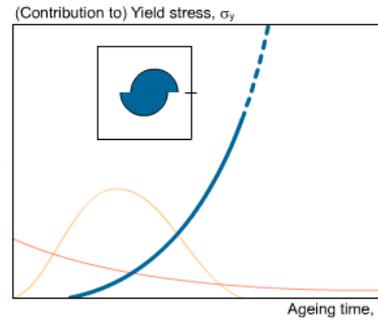
Yield strength



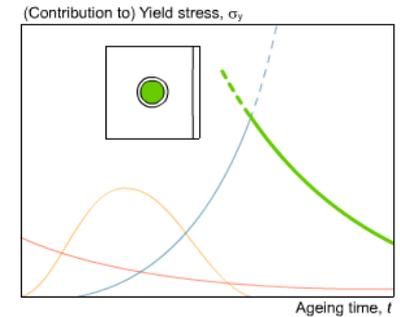
Coherency strain hardening



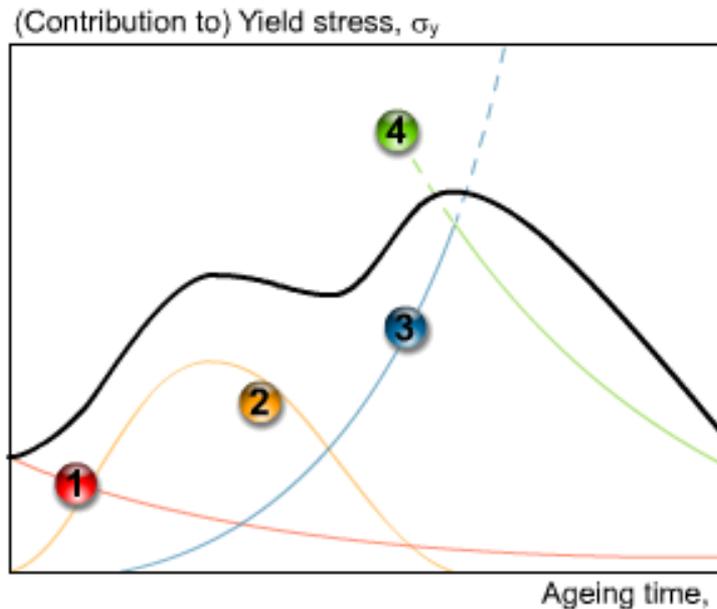
Solute hardening



Chemical hardening



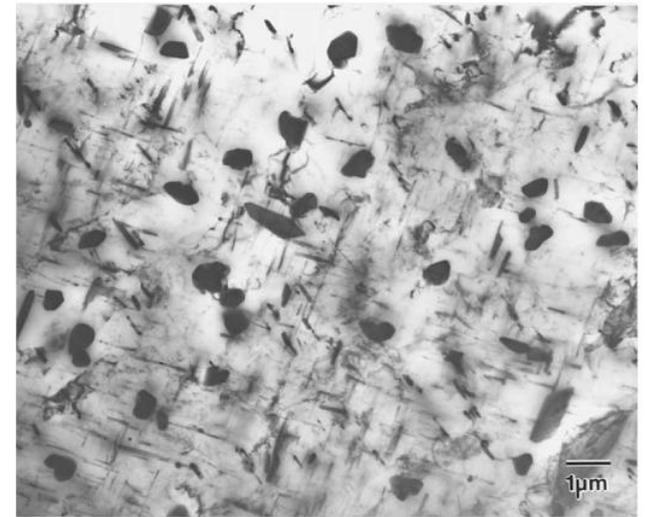
Dispersion hardening



Cumulative yield strength curve

Texture Evolution: Al 6xxx and 5xxx

- Depends on the time/temperature history
- Main difference is due to the precipitation of Mg_2Si in 6xxx alloys
- Mg_2Si impedes the progress of recrystallization by inhibiting Particle Simulated Nucleation (PSN)
- Leads to pronounced cube texture

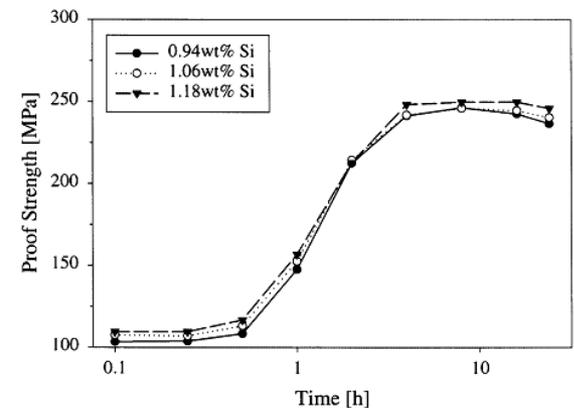
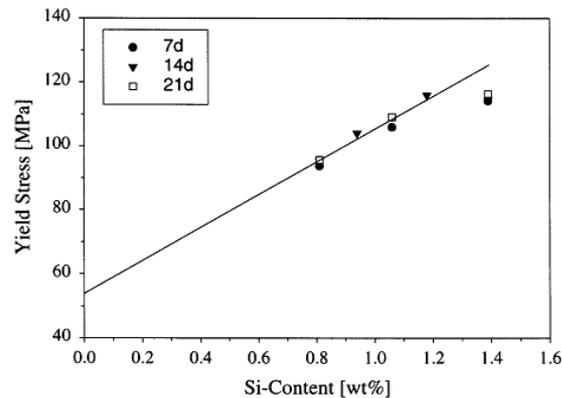
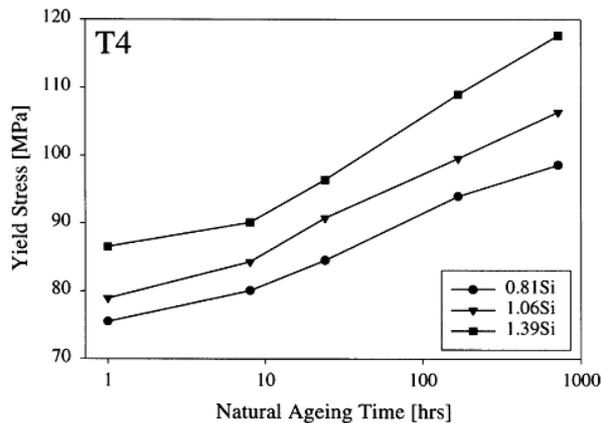


Ref [2]: Olaf Engler et. al.

*Below 300 C, recrystallization patterns are unobserved,
In order to achieve that, higher temperatures are required*

Effects of Si

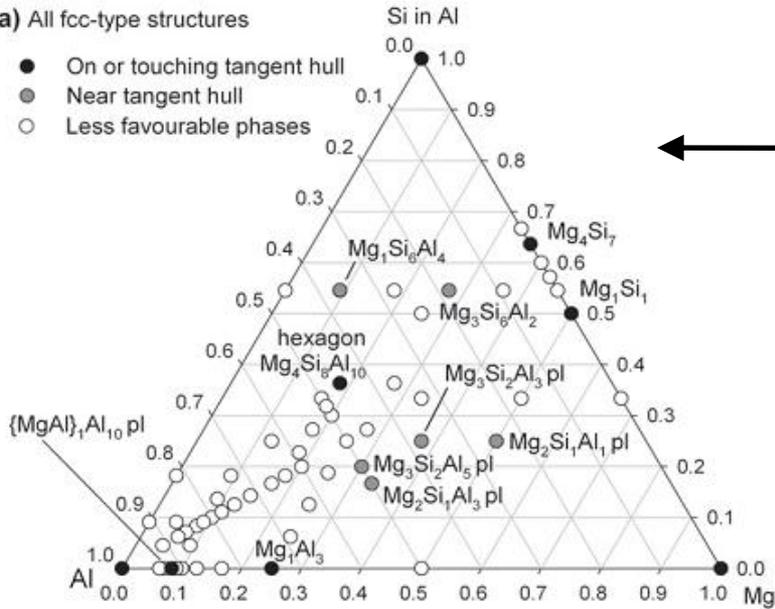
- Si level does not have a significant influence on the aging kinetics but primarily affects the initial strength level
- Exception of the very highest Si level, the strength increases linearly with Si content
- Only a small offset in strength, which increases with increasing Si content



Al-Si-Mg Phase diagram

a) All fcc-type structures

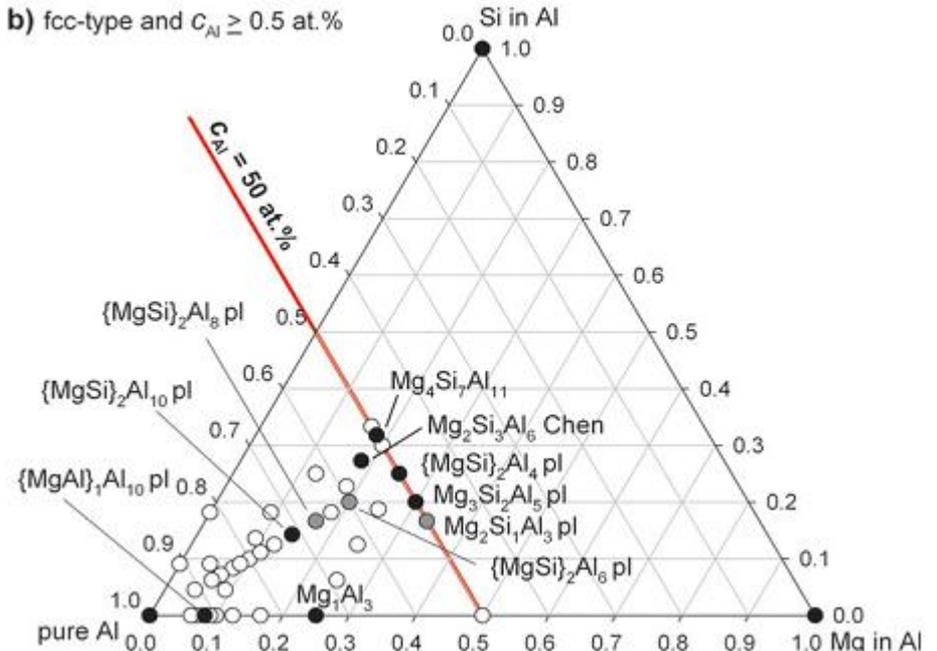
- On or touching tangent hull
- Near tangent hull
- Less favourable phases



Most stable structures

Metastable structure in early stages of precipitation

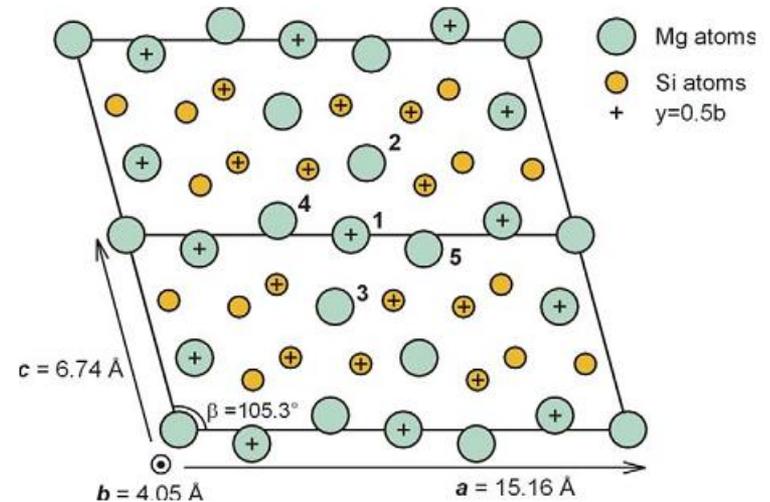
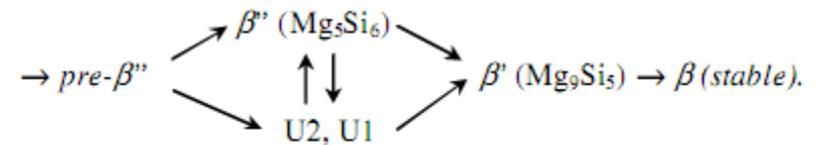
b) fcc-type and $C_{Al} \geq 0.5$ at. %



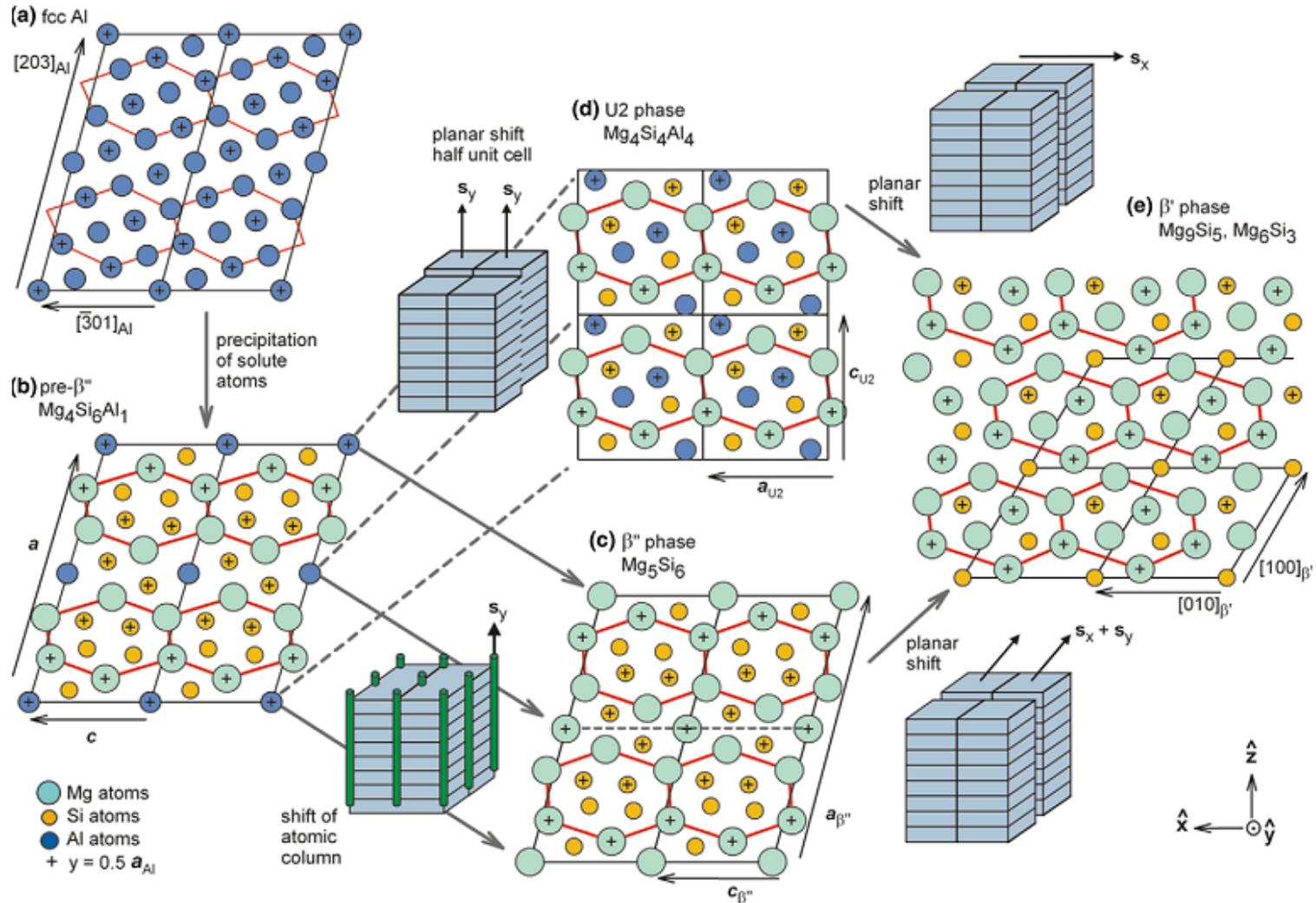
Metastable states

Phase	Composition	Structure	Exp. Lattice parameters
GP zone	Mg ₁ Si ₁	Monoclinic P2/m	a= 4.05 Å b= 4.05 Å c= 4.05 Å β= 90.0
Pre β''	(Mg + Al) 5Si6 before 0.5b shift	Monoclinic C2/m	a= 14.78 Å b= 4.05 Å c= 6.74 Å β= 106.8
Pre β''	Mg ₄ Si ₇ before 0.5b shift	Monoclinic C2/m	a= 14.6 Å b= 4.05 Å c= 6.40 Å β= 105.3
β''	Mg ₅ Si ₆ after 0.5b shift	Monoclinic C2/m	a= 15.16 Å b= 4.05 Å c= 6.74 Å β= 105.3
β''	(Mg + Al) 5Si6 after 0.5b shift	Monoclinic C2/m	a= 14.78 Å b= 4.05 Å c= 6.74 Å β= 106.8
U1	Mg ₁ Si ₂ Al ₂	Trigonal P3m1	a= 4.05 Å c= 6.74 Å
U2	Mg ₄ Si ₄ Al ₄	Orthorhombic Pnma	a= 6.75 Å b= 4.05 Å c= 7.94 Å
U3	Mg ₄ Si ₈	Imma	a= 6.40 Å b= 4.05 Å c= 7.46 Å
B'	Al ₃ Mg ₉ Si ₇	Hexagonal P6	a= 10.4 Å c= 4.01 Å
β'	Mg ₉ Si ₅	Hexagonal P6 ₃ /m	a= 7.15 Å c= 12.15 Å
β	Mg ₆ Si ₃ Mg ₂ Si	Anti-flourite Fm3m	a= 6.39 Å

SSSS → clusters → initial-β''

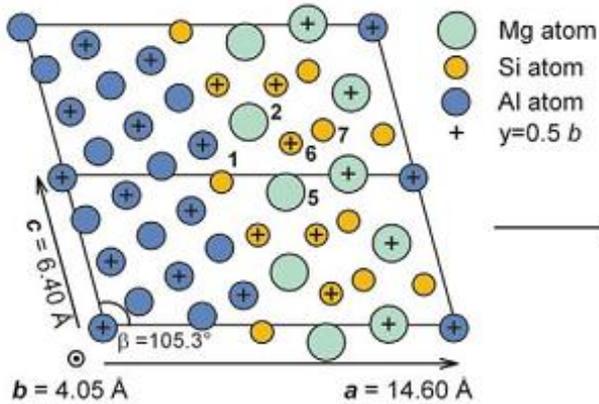


Precipitation Phases

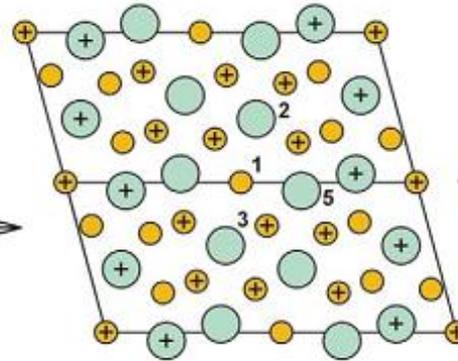


Phase transformation

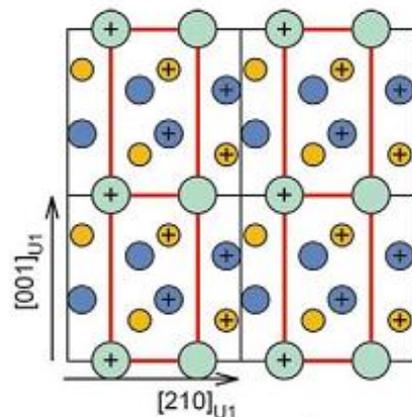
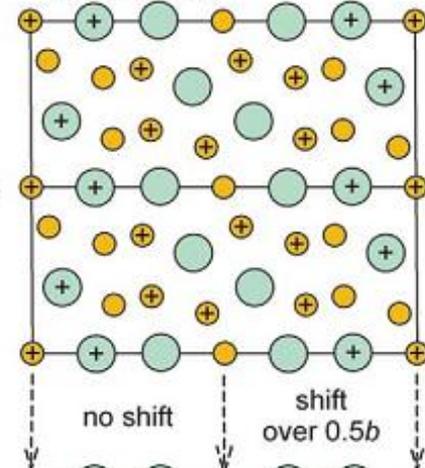
(a) $\text{Mg}_4\text{Si}_7\text{Al}_{11}$ (P/m) hexagon planes, Al matrix confined



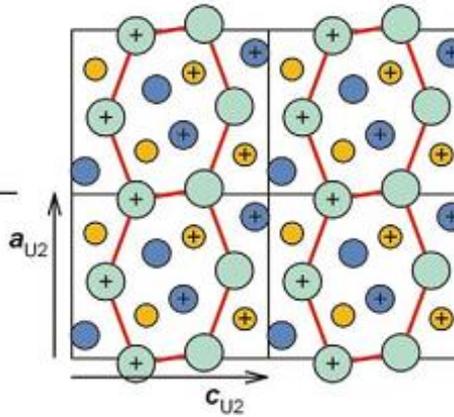
(b) pre- β'' Mg_4Si_7 (C2/m), Al matrix confined



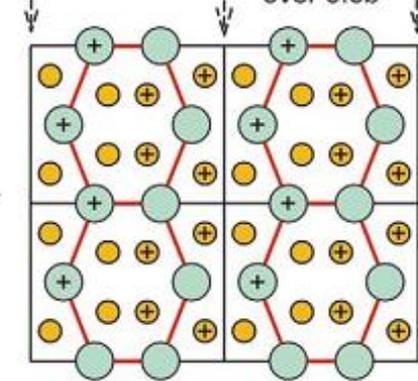
(c) pre- β'' Mg_4Si_7 (C2/m) full relaxation



(f) U1 phase $\text{Mg}_1\text{Si}_2\text{Al}_2$ ($P\bar{3}m1$)



(e) U2 phase $\text{Mg}_4\text{Si}_4\text{Al}_4$ ($Pnma$)

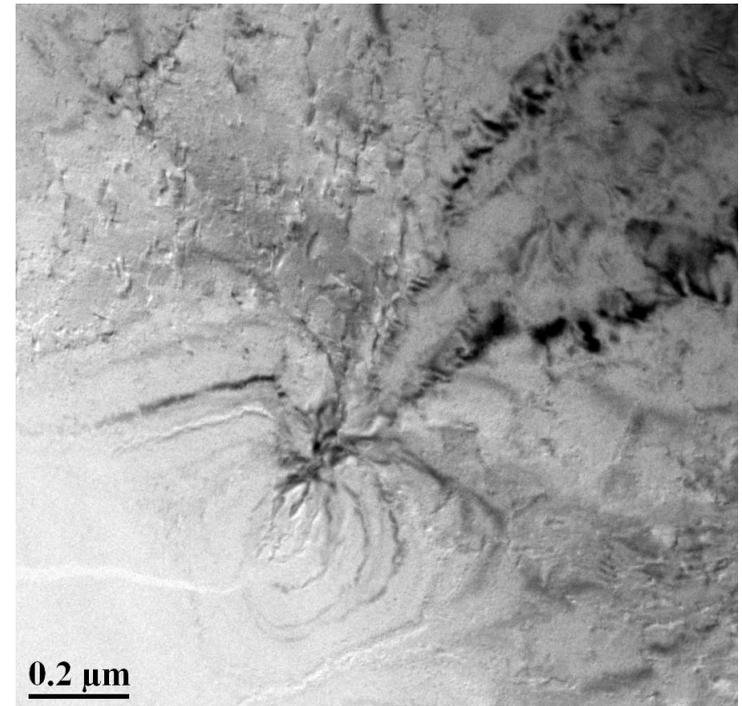
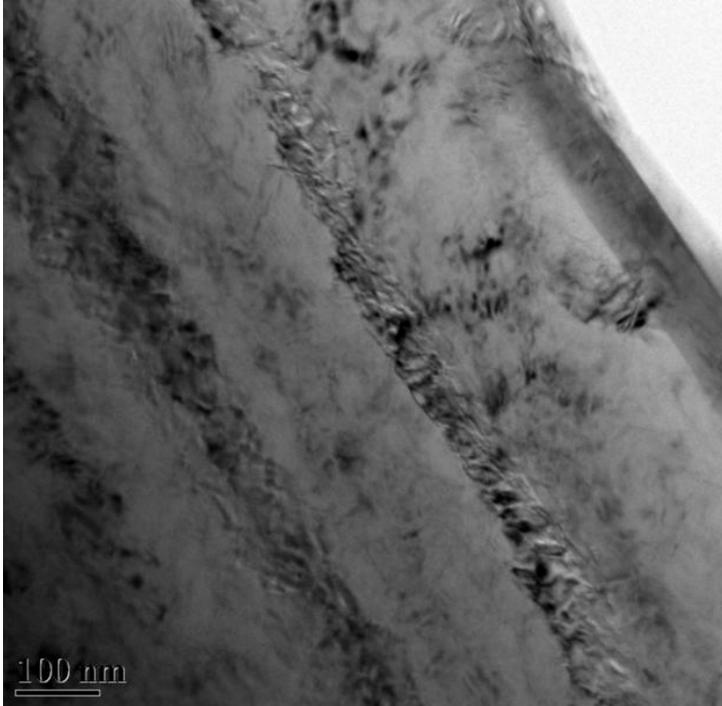


(d) U3 phase Mg_4Si_8 ($I4mma$)

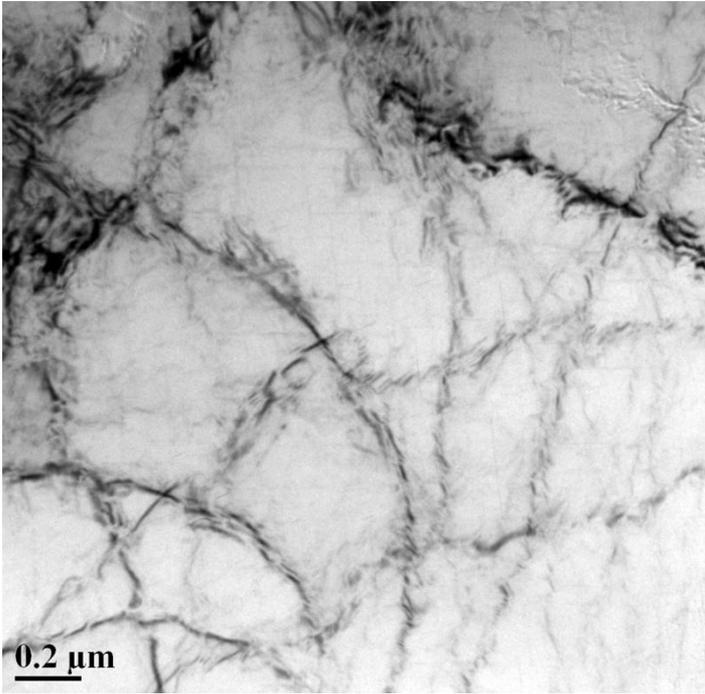
TEM experiments

Sample	Pre-Strain	Annealing time	Annealing temp.	Annealing source
Sample 1	15%	0	NA	NA
Sample 2	15%	10 s	250°C	SALT BATH
Sample 3	15%	60 s	250°C	SALT BATH
Sample 4	15%	5 min	250°C	SALT BATH
Sample 5	15%	60 min	250°C	SALT BATH
Sample 6	15%	5 min	250°C	FURNACE
Sample 7	15%	60 min	250°C	FURNACE
Sample 8	0%	0	NA	NA

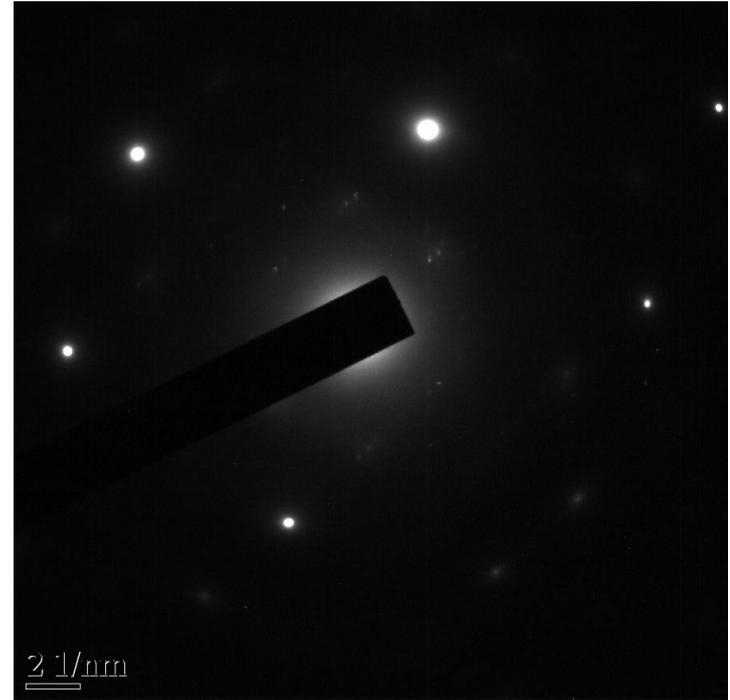
15% prestrain with no annealing



15% prestrain with annealing (sub-grain structure)

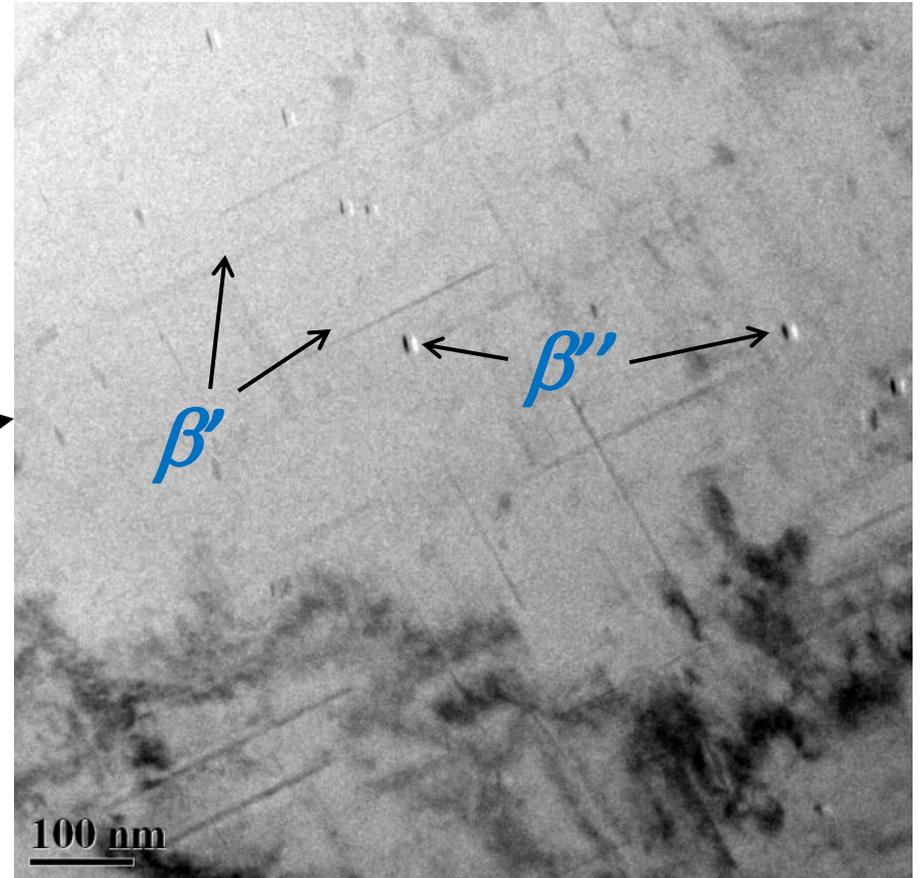
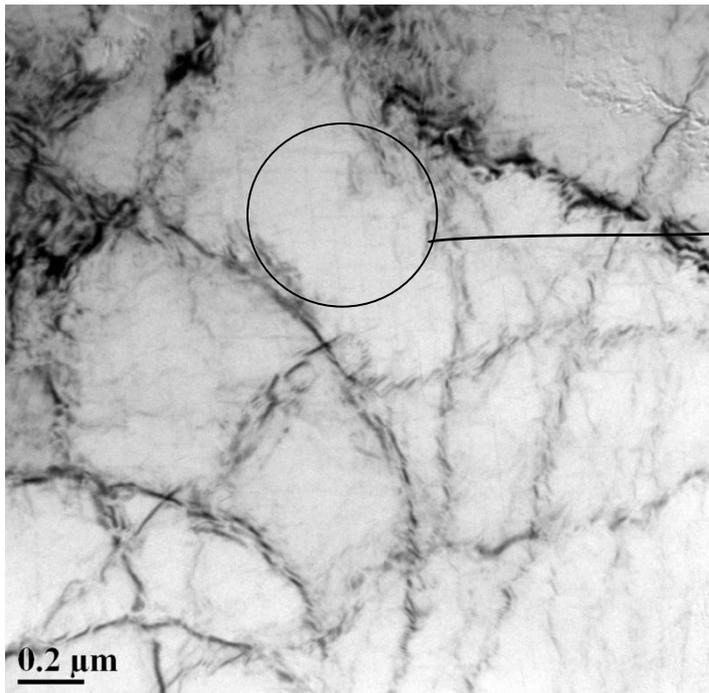


Sub-structure

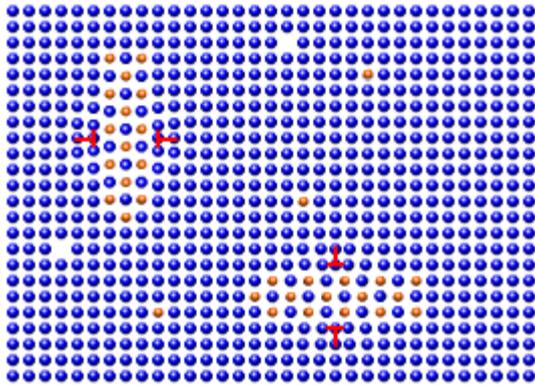


Diffraction pattern of left
micrograph

15% prestrain with annealing (β'' and β' observed)

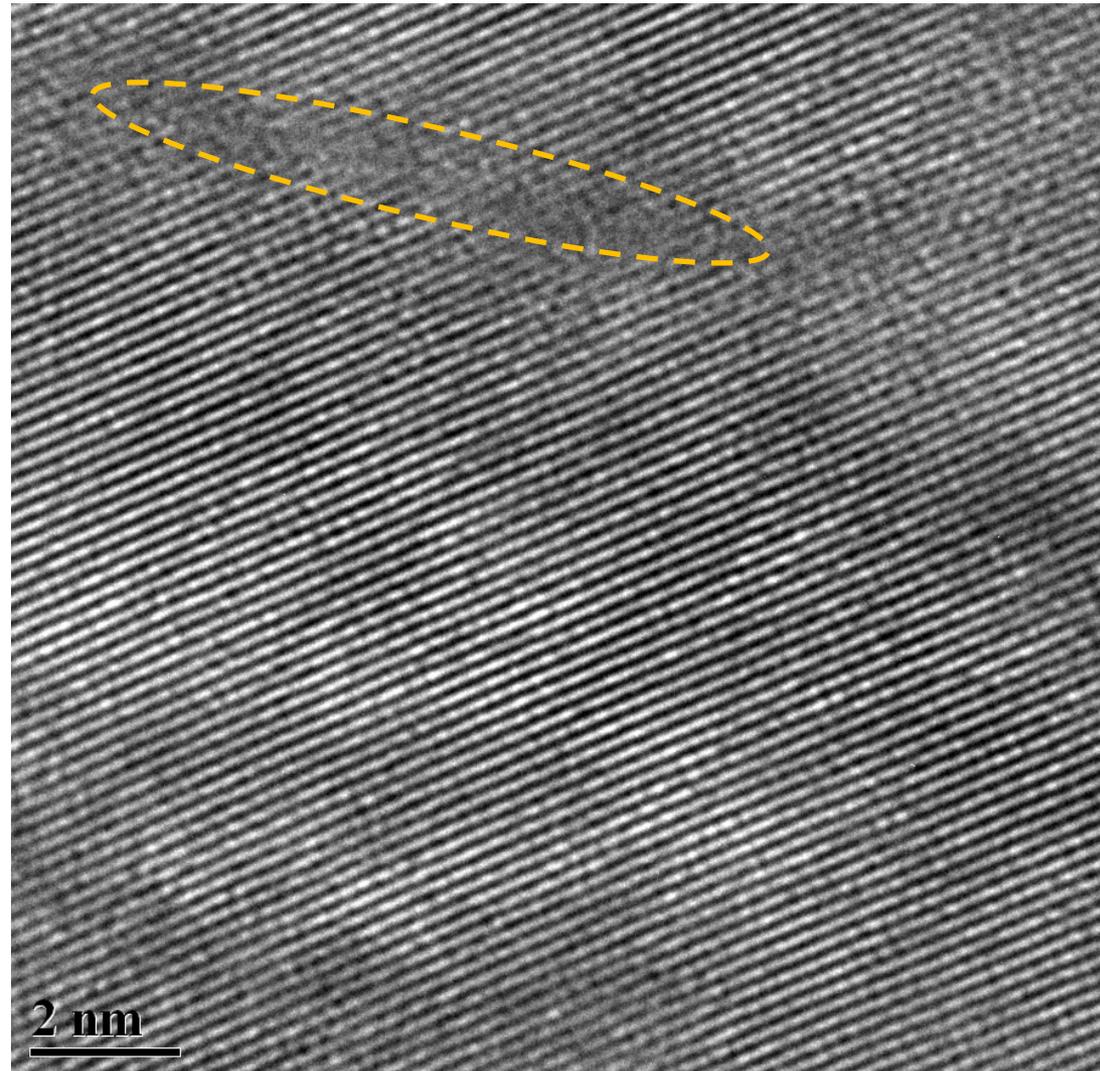


15% prestrain with annealing (β')



A • B •

Semi-coherent Precipitates



Summary

- Large localized shear zones in pre-straining
- Evidence of recovery (sub-grain structure) on annealing
- Presence of both plate-like β' and needle-like β'' on annealing
- Stoichiometry of β' and β'' (start and end Temp)?