

# Role of microstructure in modeling of manufacturing Processes

Asim Tewari

National Center for Aerospace Innovation and Research  
Department of Mechanical Engineering  
Indian Institute of Technology, Bombay

TEQIP, IIT Bombay Dec 22-23, 2014



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Old Guest House overlooking Pond

In a gentle way, you can shake the world - *Mahatma Gandhi*



Engages in research, education, training, technology development and related activities in most areas of technology, science & management

- 530 acres (5.3 sq. km) of campus area
- 15 Departments, 1 School, 4 IDPs & 9 Centers
- ~600 fulltime faculty & 90 adjunct faculty
- ~1300 support staff
- ~9600 students (P.G ~ 6000; PhD~2000)
- ~750 project research staff



Patents (India and Foreign) 2012-2013	>100
Number of industries which come to us for projects	>2000
Research funding in INR (Governmental & Industrial, 2012-13)	~300 Cr
Number of technology spinoffs from IITB technologies	>50

# Overview of NCAIR

## Vision

- ❖ Create a World Class Aerospace Ecosystem in India

## Mission

- ❖ To be a catalyst for collaboration between industry, Academia, R&D Organizations and Government
- ❖ To provide economically viable and sustainable solutions
- ❖ To promote Innovation, Knowledge Creation and Entrepreneurship
- ❖ To disseminate knowhow and develop human resources

## Inception

19<sup>th</sup> November 2010

## Key Strategic Technologies

Machining

Forming

Casting

## Scope of Materials

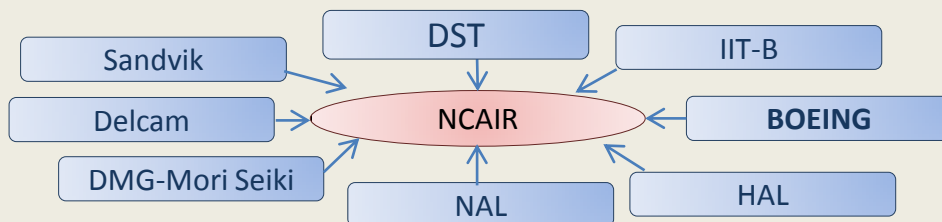
Titanium

Super Alloys

Composites

Aluminum, Magnesium, AHSS

## Stake-holders















## Services of NCAIR

### Core Services

- ✓ R&D Projects
- ✓ Technology Transfer

### Enabling Services

- ✓ Specialized Training Programs
- ✓ Adv Aero Mfg and testing facilities for R&T Activities
- ✓ Mentoring and business Services

Faculty members	Previous affiliations	Faculty members	Previous affiliations
Prof. Suhas Joshi 	IIT-Bombay, UIUC	Prof. B. Ravi 	IISc Bangalore, Purdue U
Prof. Asim Tewari 	Georgia Tech, GM Global R&D	Prof. Ramesh Singh 	Georgia Tech
Prof. S.S.Pande 	IIT-Bombay, U. Of Cincinnati	Prof. Sushil Mishra 	IIT-Bombay, GM Global R&D
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Prof. Rajneesh Bharadwaj 	Johns Hopkins University, Baltimore	Prof. Rakesh G Motwani 	Nanyang Technological University, Singapore.

# What is microstructure?

A microstructure is an arrangement of volumes, internal surfaces, lines, and points

Volumes: Voids, fibers, inclusions, particles, grains, etc.

Surfaces: Micro-crack surfaces, grain boundaries, inclusion interfaces, etc

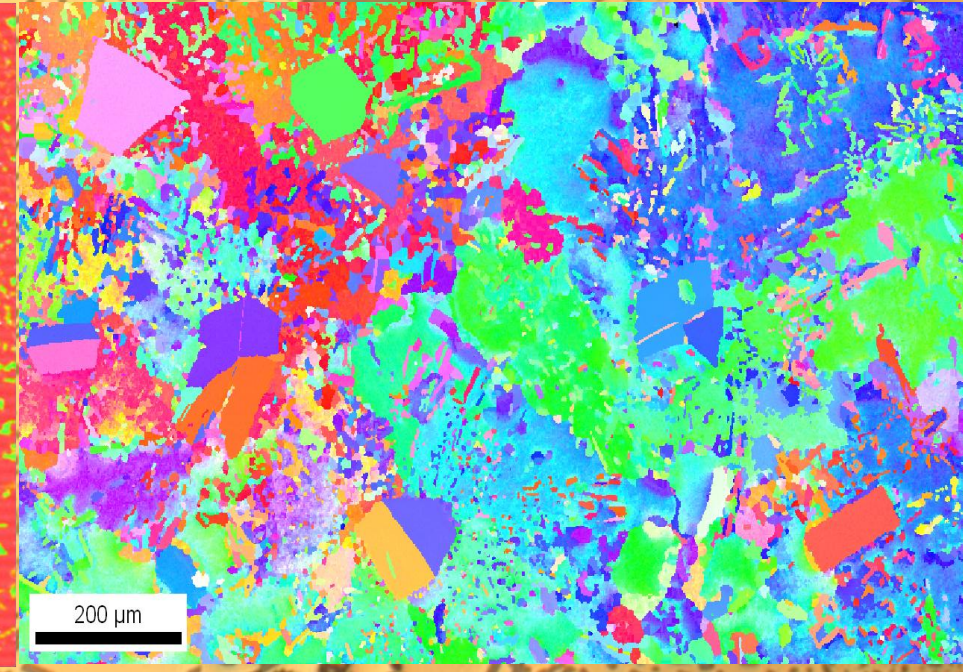
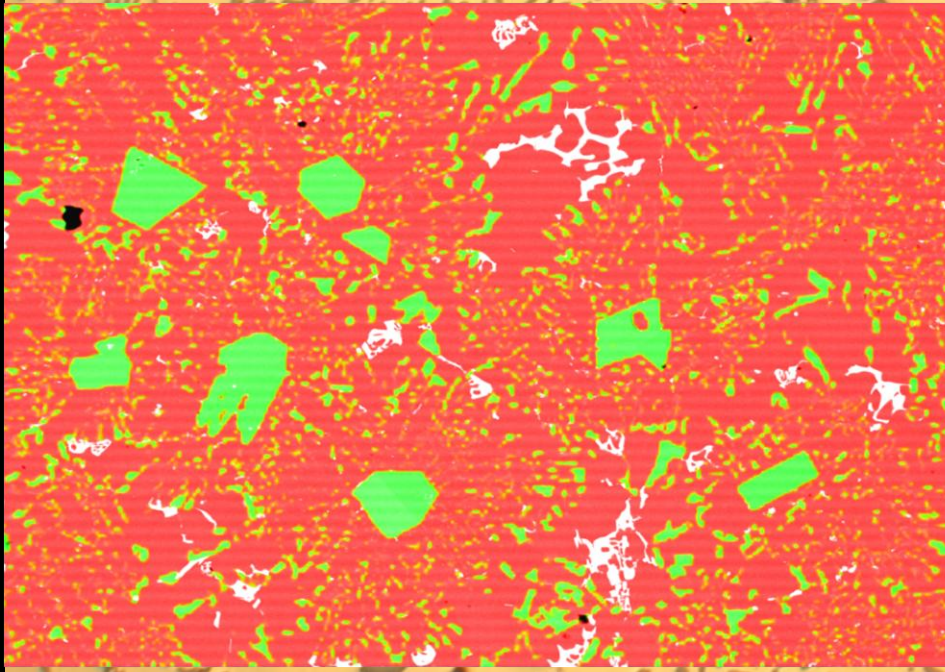
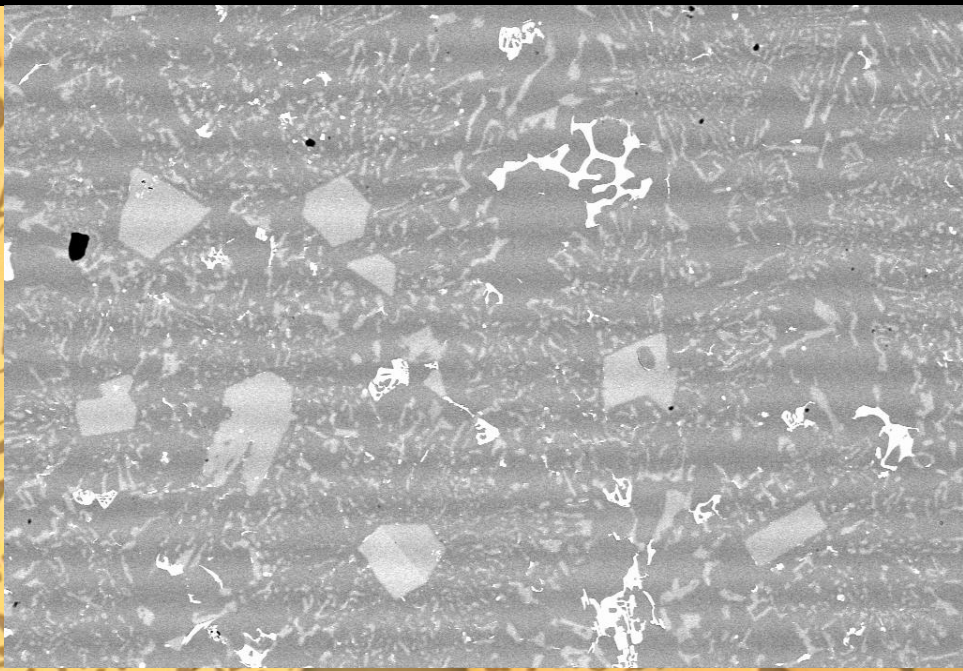
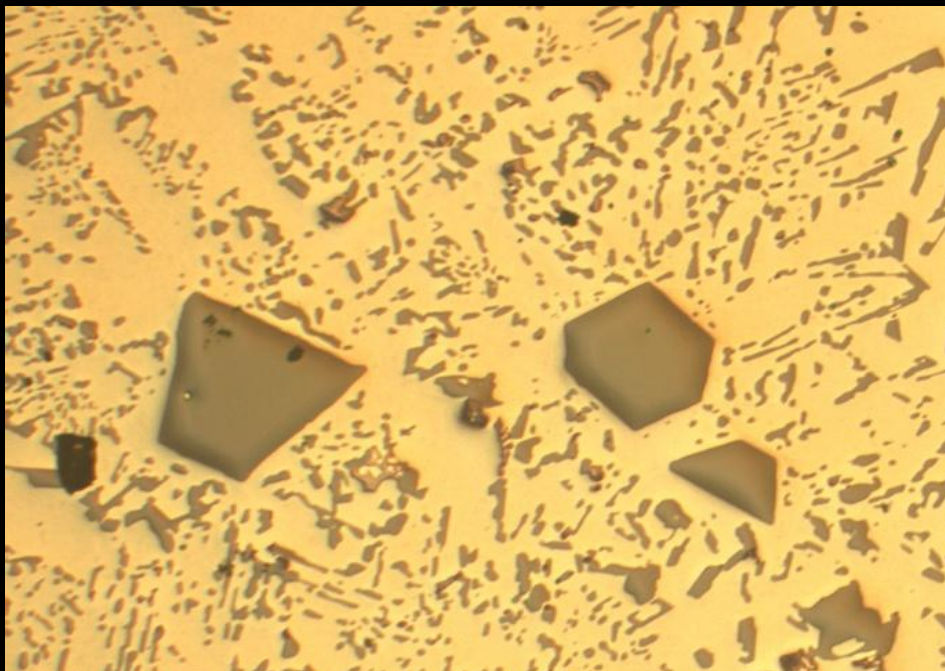
Lines: Dislocation lines, micro-crack tips, grain edges, triple lines, etc.

Points: Quadruple points, particle/grain centers, atoms, etc.

Texture is a part of structure and thus microstructure

## Most general definition

Microstructure is a spatially (and/or temporally) varying  $d$  dimensional data structure.

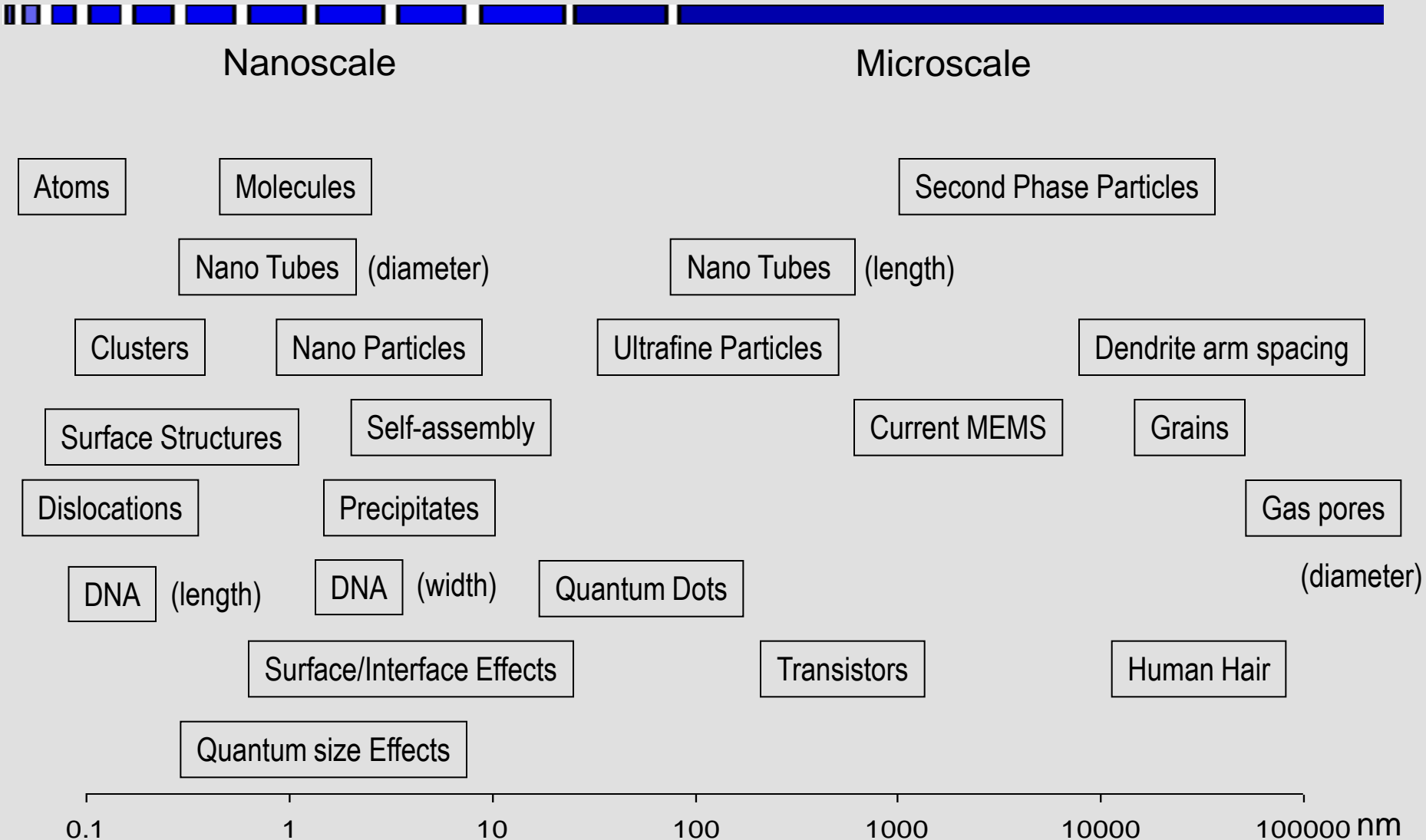


# Modalities of acquisition

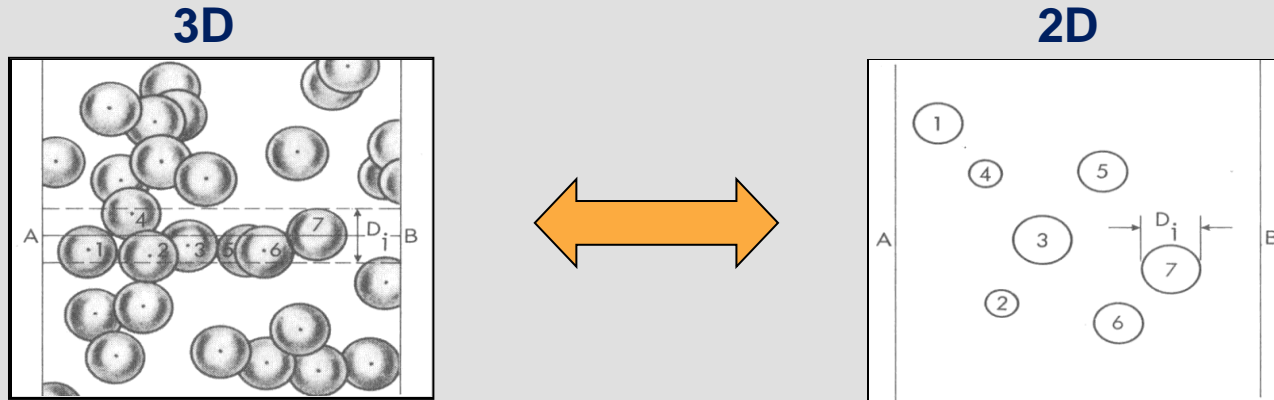
- ⦿ Optical
- ⦿ SEM
- ⦿ TEM
- ⦿ AFM
- ⦿ SPM
- ⦿ X-ray CT
- ⦿ PET, MRI, SIMS, etc.



# Larger to smaller



# Problem of spheres in 3D

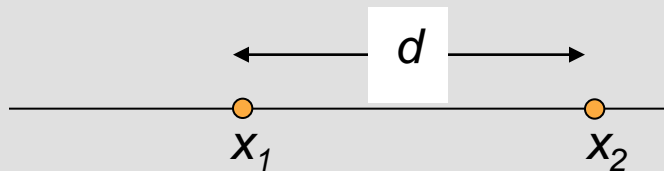


For a collection of spheres of different sizes in 3D which of the following is true:

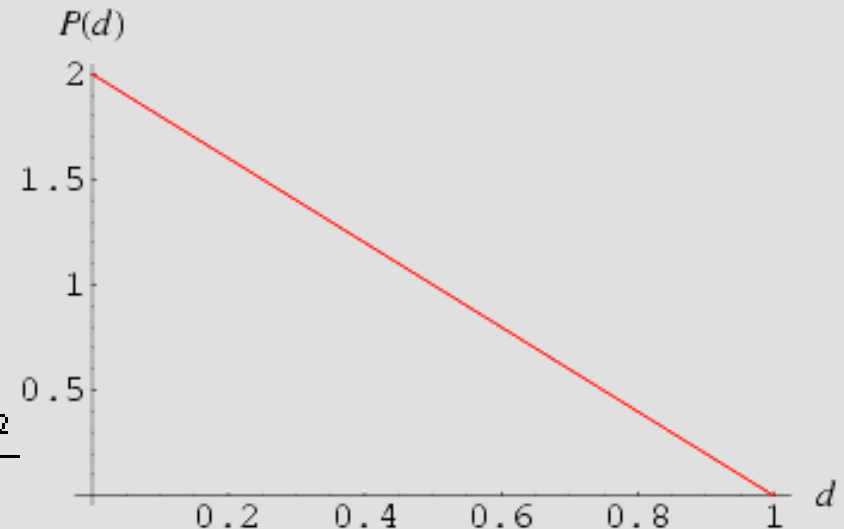
- 1.) Mean circle size in 2D is less than mean 3D sphere size
- 2.) Mean circle size in 2D is greater than mean 3D sphere size
- 3.) Mean circle size in 2D is equal to mean 3D sphere size

# Non-trivial problem

On a unit line segment choose two random points  $x_1$  and  $x_2$ . If the points are  $d$  distance apart (without regard to ordering), what value of  $d$  has the highest probability?

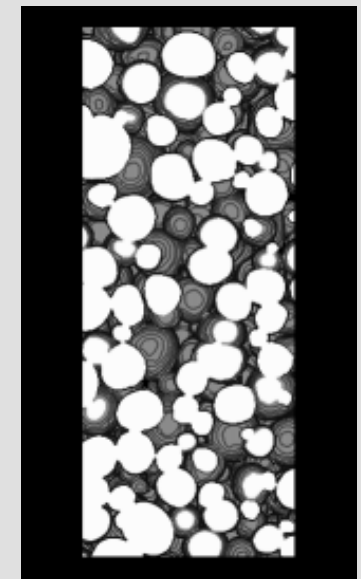
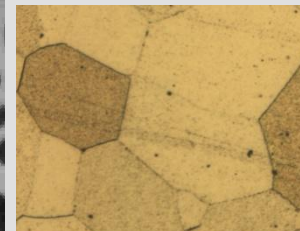
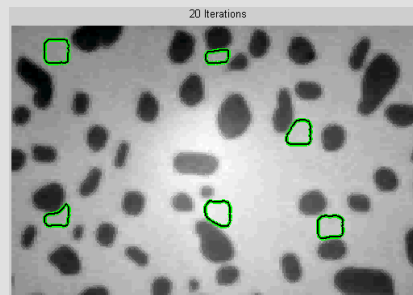
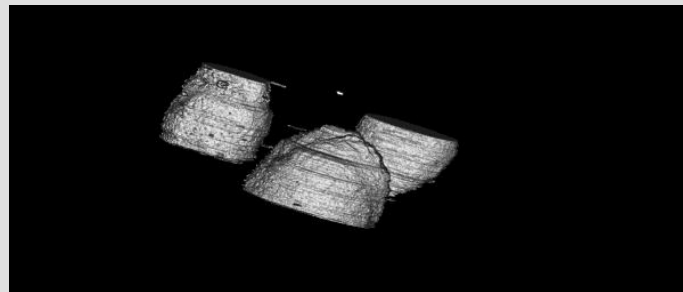
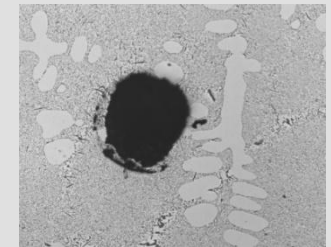
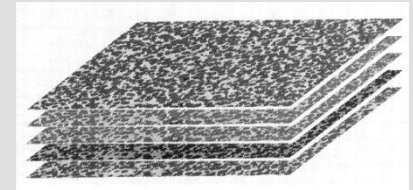
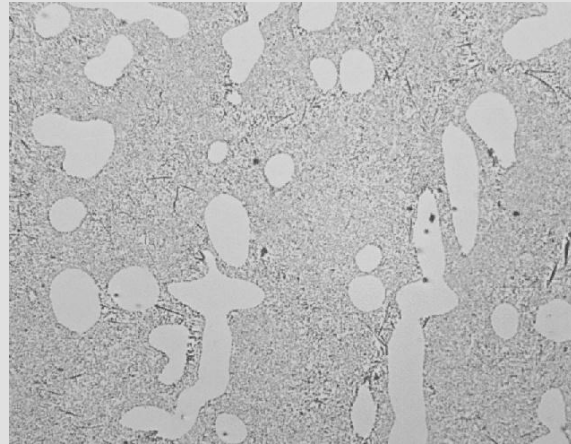


$$\begin{aligned} P(d) &= \frac{\int_0^1 \int_0^1 \delta(d - |x_2 - x_1|) dx_1 dx_2}{\int_0^1 \int_0^1 dx_1 dx_2} \\ &= 2(1-d), \end{aligned}$$



# Stereology : True three-dimensional probe

- Pioneering work on
  - 3D spatial statistics
  - topological connectivity
  - Euler-Poincare
- Approach
  - through 3D reconstruction
  - grains modeled as ext. convex rings
- Materials System
  - A356 alloy
  - AA5754 alloy
  - AZ31 alloy
  - THA

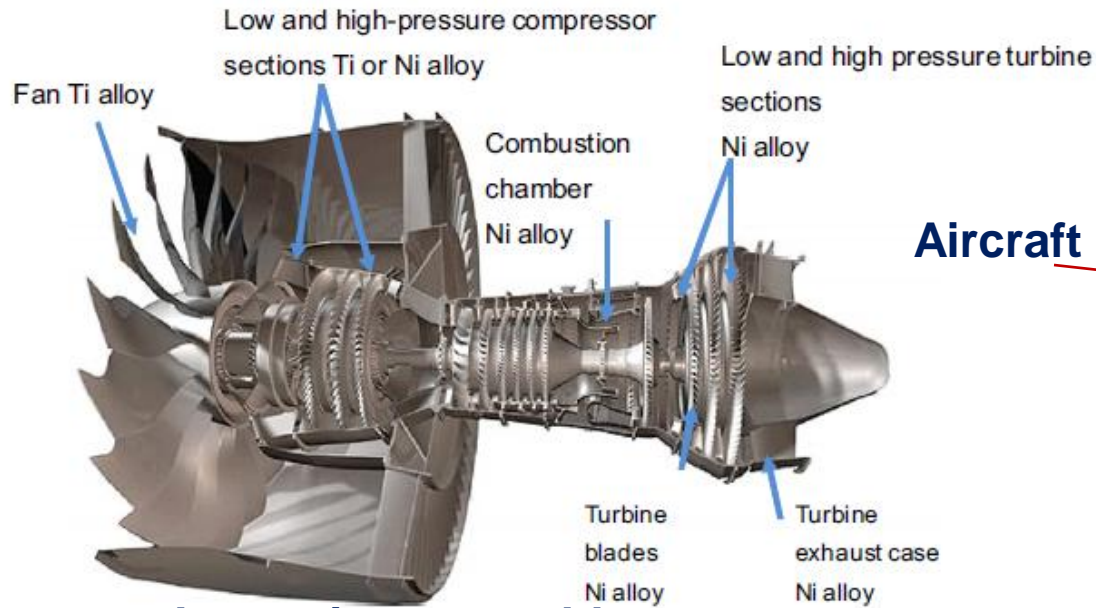


# Case Study 1

## Titanium alloy machining

# Motivation

Gas turbine engine, compressor parts, airframe structure, Landing gear disc



**Jet engine assembly**

**Aircraft bolts**

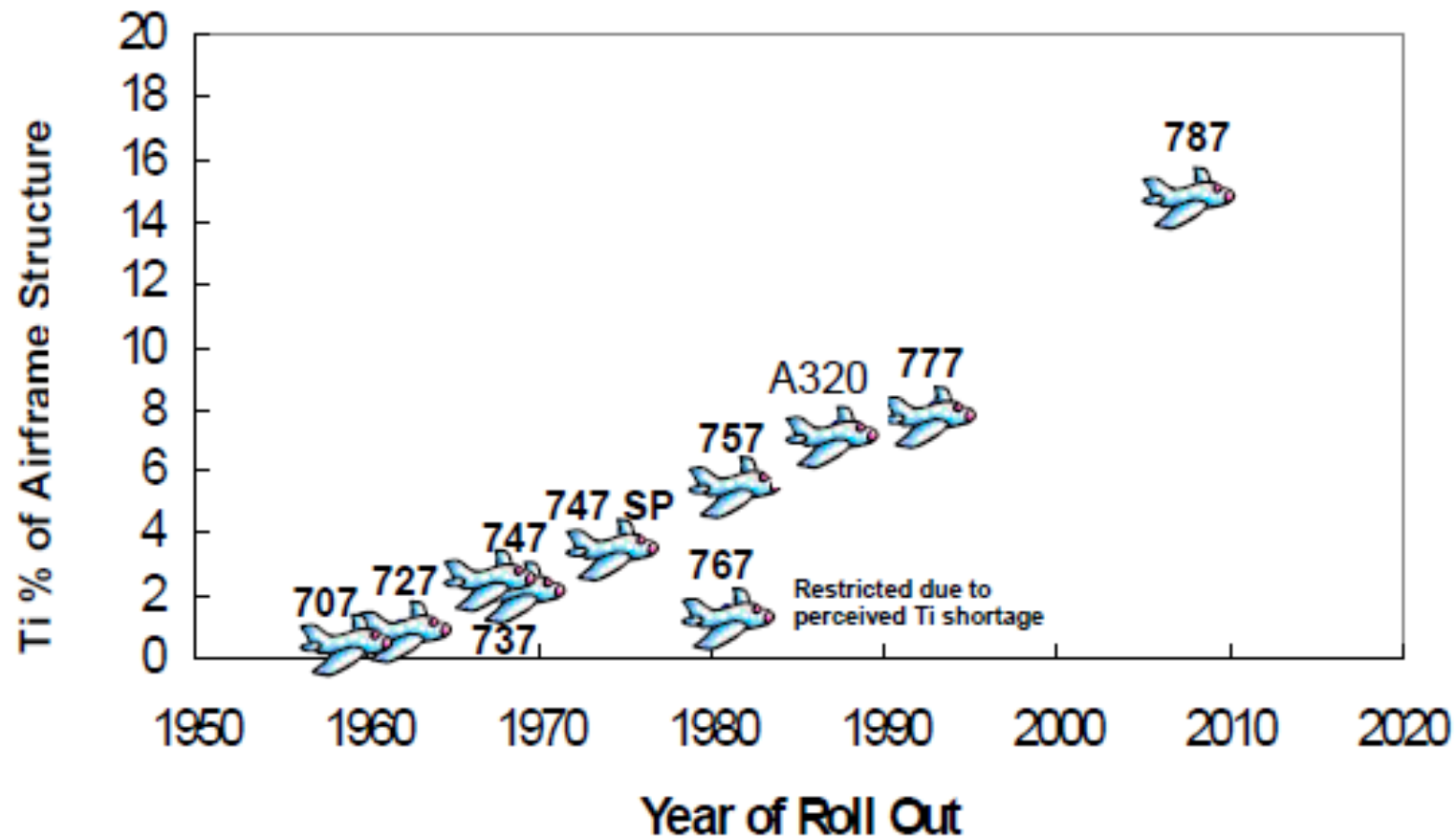


**Bladed impeller disk**

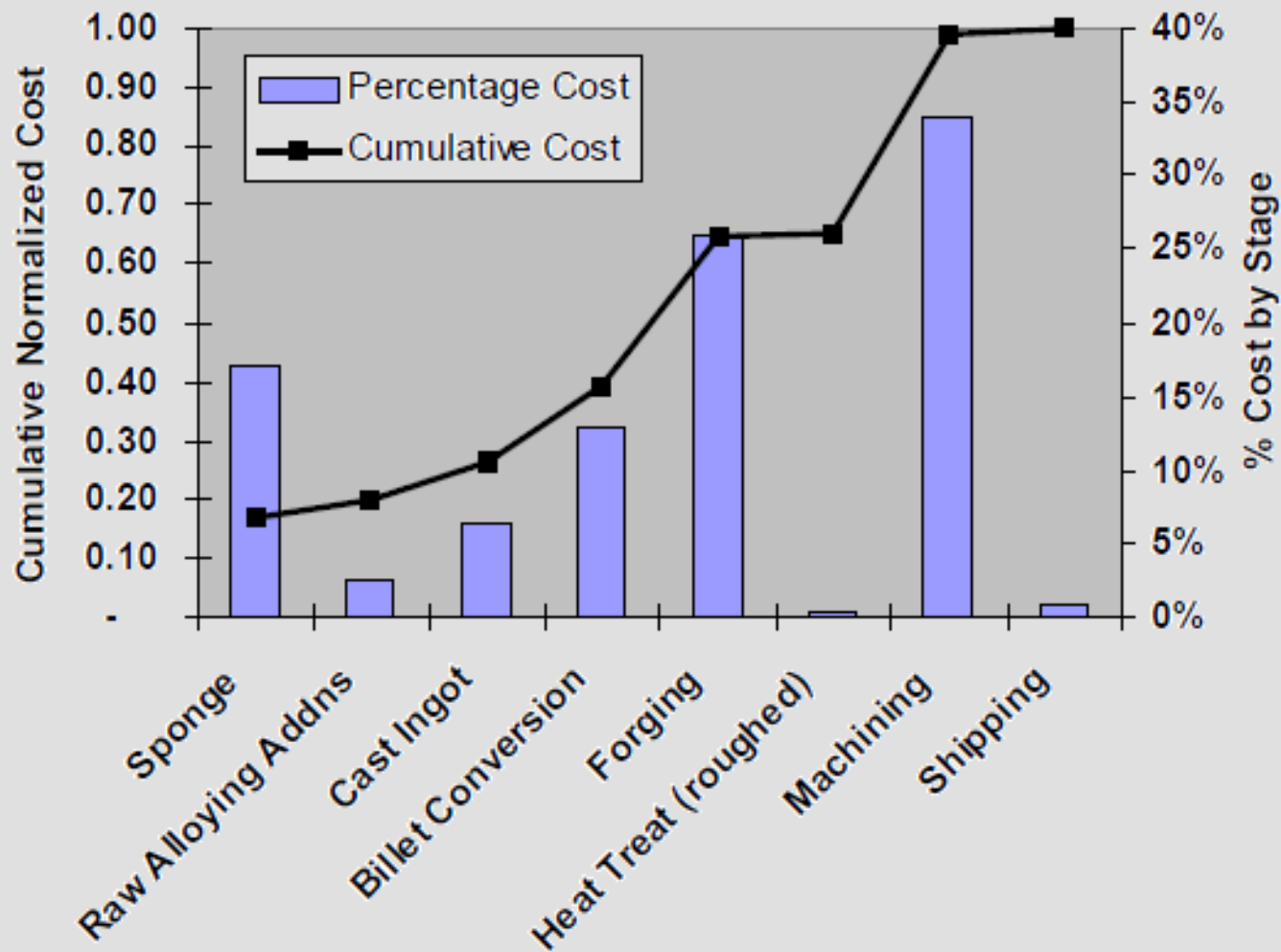
**Airframe**



# Percentage of Airframe Titanium vs. Year of Rollout—Commercial Transports

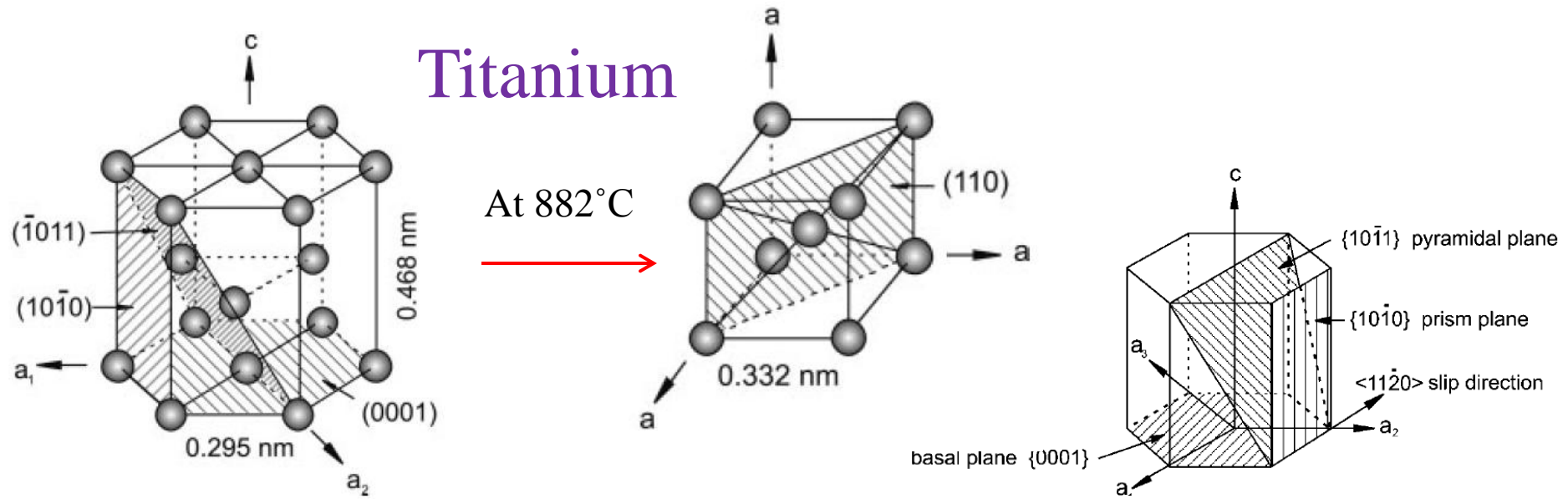


# Titanium Value Chain—Forgings





# Titanium

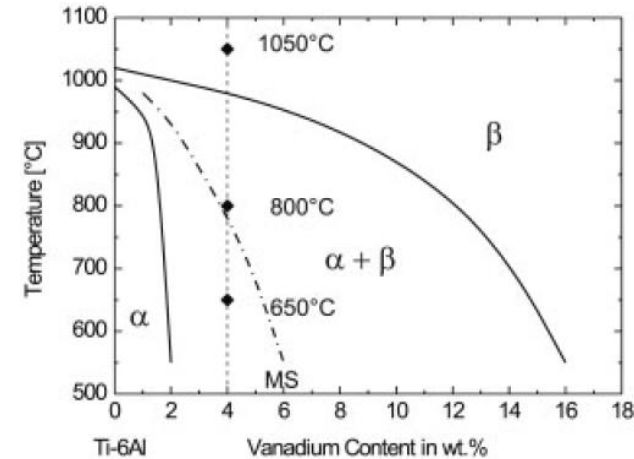
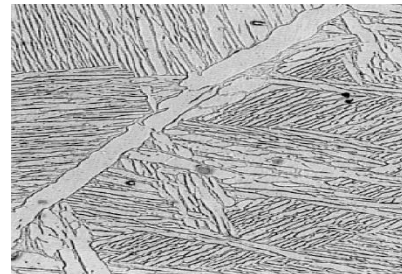
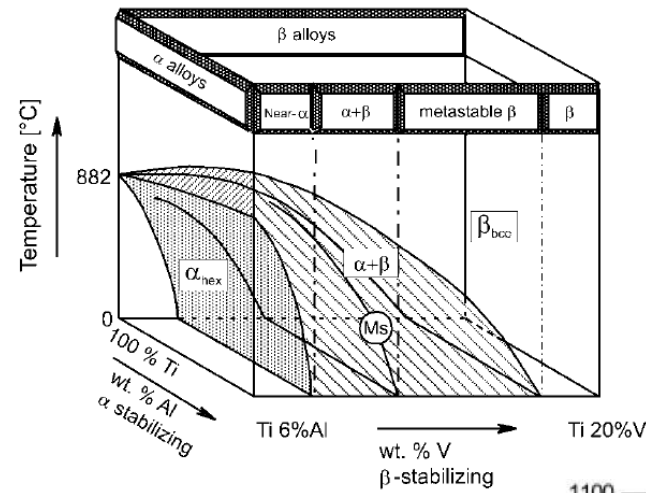
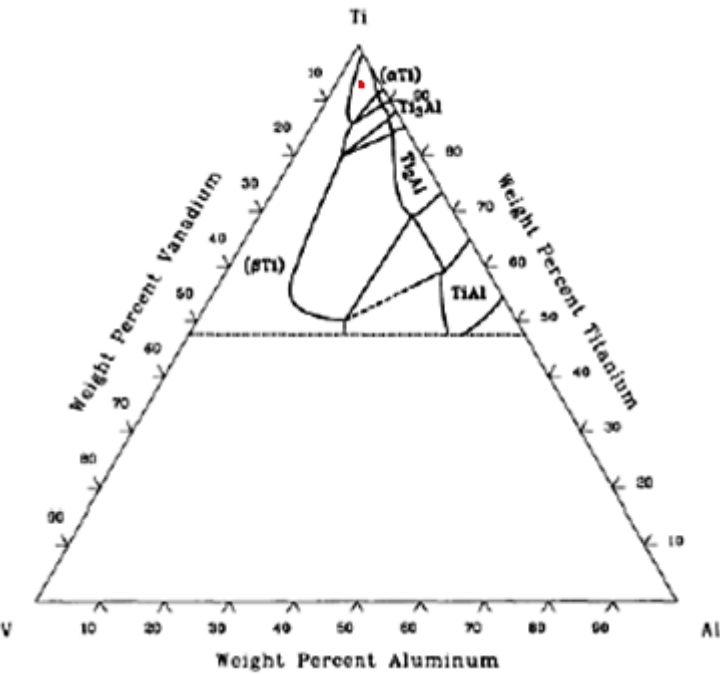


## Effect of $c/a$ Ratio on slip systems of HCP crystals

Typical slip systems observed in some HCP metals

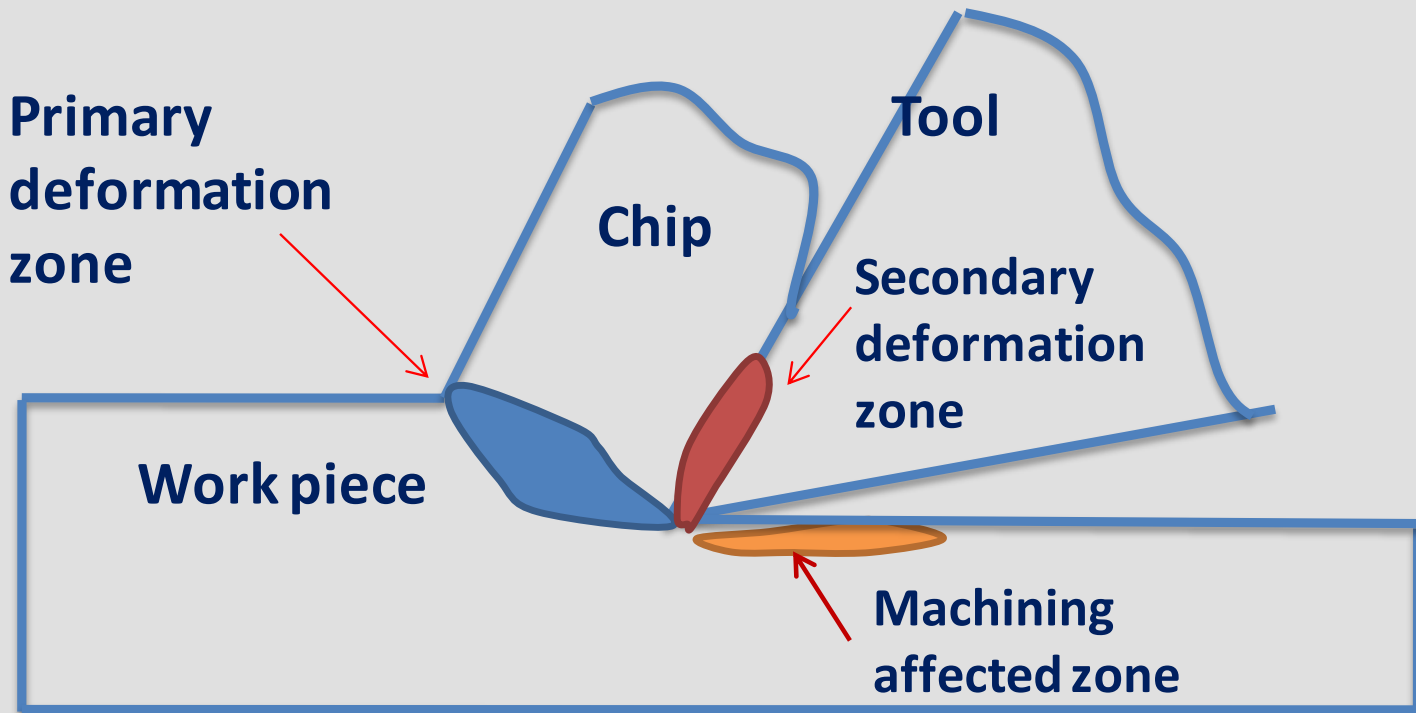
Element	$c/a$	Deviation (%) from the ideal $c/a = 1.633$	Principal slip system	Secondary slip system	Other slip system
Cd	1.886	+15.5	Basal $\{0001\}\langle 11\bar{2}0 \rangle$	Pyramidal $\{11\bar{2}2\}\langle 11\bar{2}3 \rangle$	Prismatic $\{10\bar{1}0\}\langle 11\bar{2}0 \rangle$ Pyramidal $\{10\bar{1}1\}\langle 11\bar{2}0 \rangle$
Zn	1.856	+13.6	Basal $\{0001\}\langle 11\bar{2}0 \rangle$	Pyramidal $\{11\bar{2}2\}\langle 11\bar{2}3 \rangle$	Prismatic $\{10\bar{1}0\}\langle 11\bar{2}0 \rangle$
Mg	1.624	-0.6	Basal $\{0001\}\langle 11\bar{2}0 \rangle$	Prismatic $\{10\bar{1}0\}\langle 11\bar{2}0 \rangle$	Pyramidal $\{10\bar{1}1\}\langle 11\bar{2}0 \rangle\{11\bar{2}2\}\langle 11\bar{2}3 \rangle$
Co	1.623	-0.6	Basal $\{0001\}\langle 11\bar{2}0 \rangle$	None	None
Zr	1.593	-2.4	Prismatic $\{10\bar{1}0\}\langle 11\bar{2}0 \rangle$	Basal $\{0001\}\langle 11\bar{2}0 \rangle$	Pyramidal $\{10\bar{1}1\}\langle 11\bar{2}0 \rangle\{11\bar{2}2\}\langle 11\bar{2}3 \rangle$
Ti	1.588	-2.8	Prismatic $\{10\bar{1}0\}\langle 11\bar{2}0 \rangle$	Basal $\{0001\}\langle 11\bar{1}0 \rangle$	Pyramidal $\{10\bar{1}1\}\langle 11\bar{2}0 \rangle\{11\bar{2}2\}\langle 11\bar{2}3 \rangle$
Hf	1.581	-3.2	Prismatic $\{10\bar{1}0\}\langle 11\bar{2}0 \rangle$	Basal $\{0001\}\langle 11\bar{2}0 \rangle$	
Be	1.568	-4.0	Basal $\{0001\}\langle 11\bar{2}0 \rangle$	Prismatic $\{10\bar{1}0\}\langle 11\bar{1}0 \rangle$	Pyramidal $\{10\bar{1}1\}\langle 11\bar{2}0 \rangle\{11\bar{2}2\}\langle 11\bar{2}3 \rangle$

# Ti-6Al-4V alloy

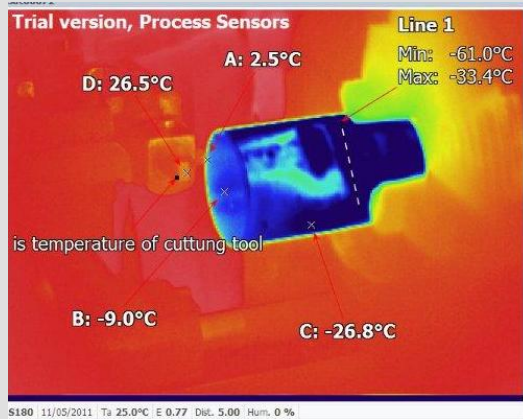


- At high cooling rate from above martensite start temp transform  $\beta$  phase completely into hcp  $\alpha$  by diffusionless transformation
- It does not lead to embrittlement but slightly increased strength compared to  $\alpha$  titanium
- Two types of martensite
  - Hexagonal  $\alpha'$  martensite- shows needle like fine basket-weave structure
  - Orthorhombic  $\alpha''$  martensite- quenching below  $900^\circ\text{C}$ , shows good deformability

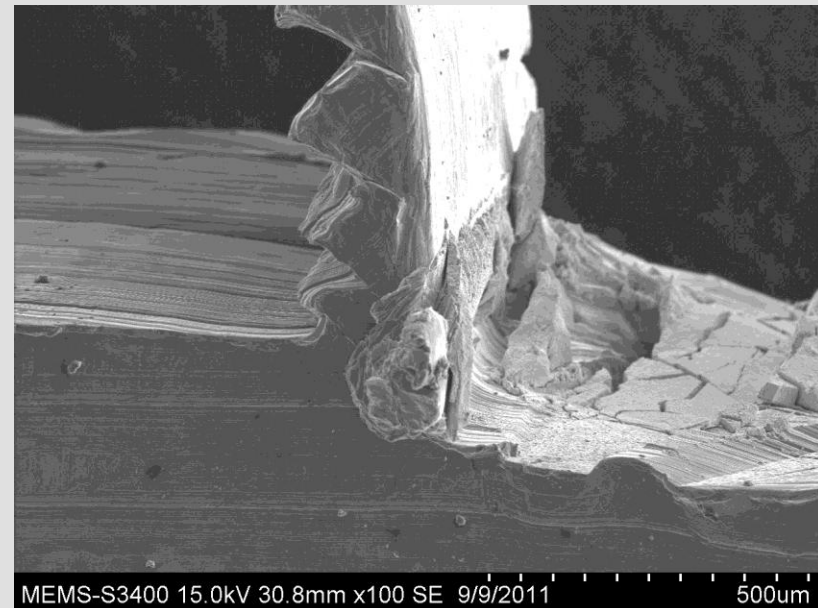
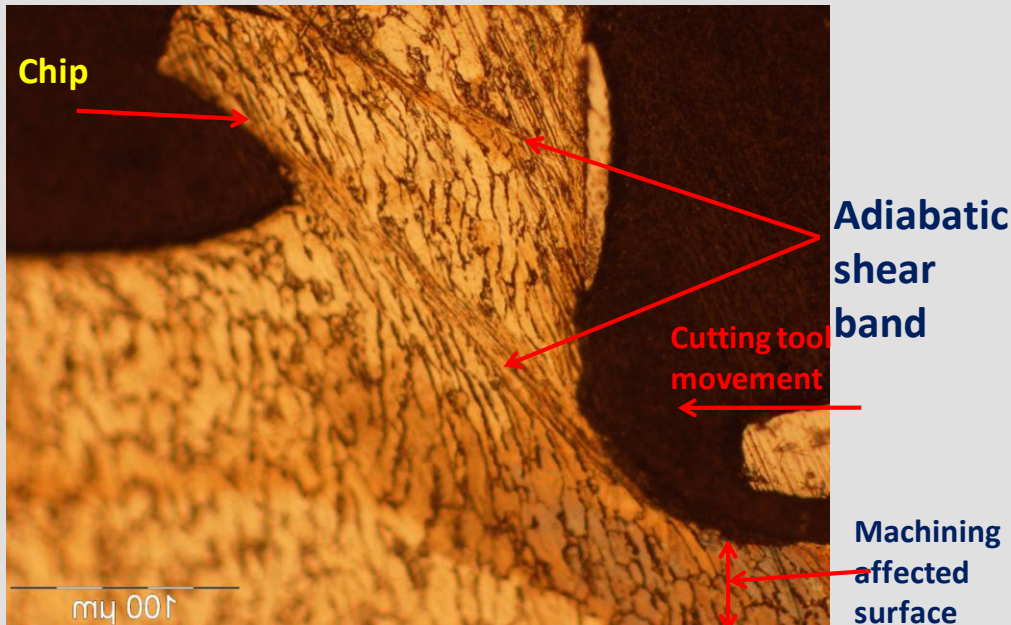
# The mechanics of machining



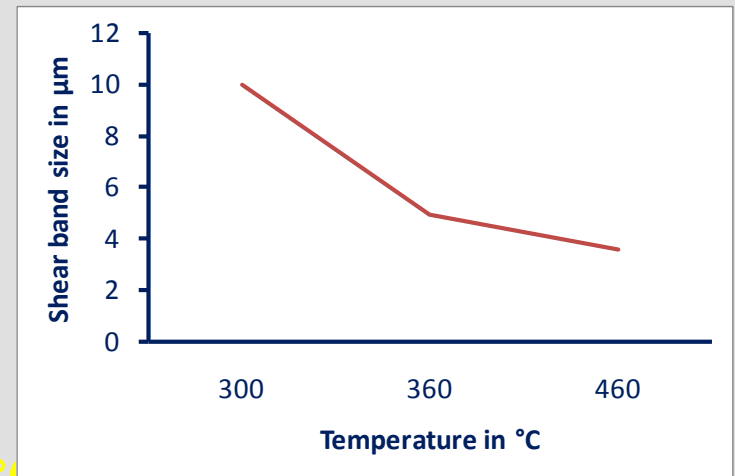
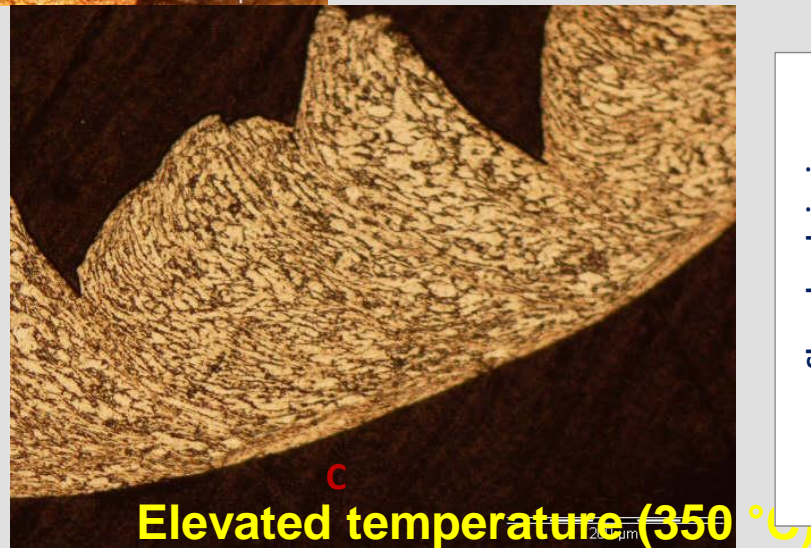
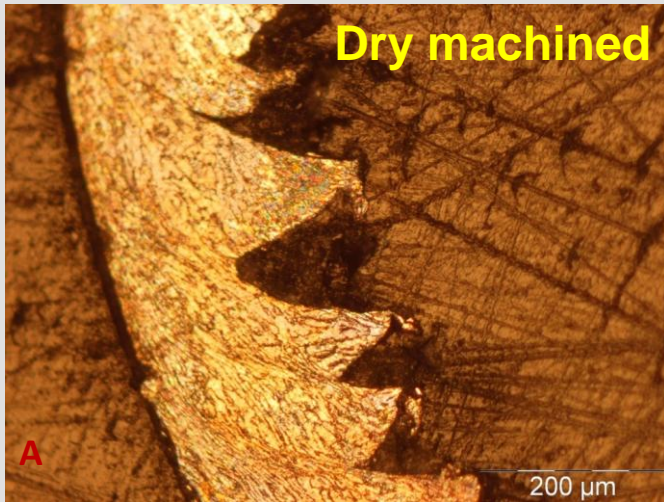
# Chip freeze experiments



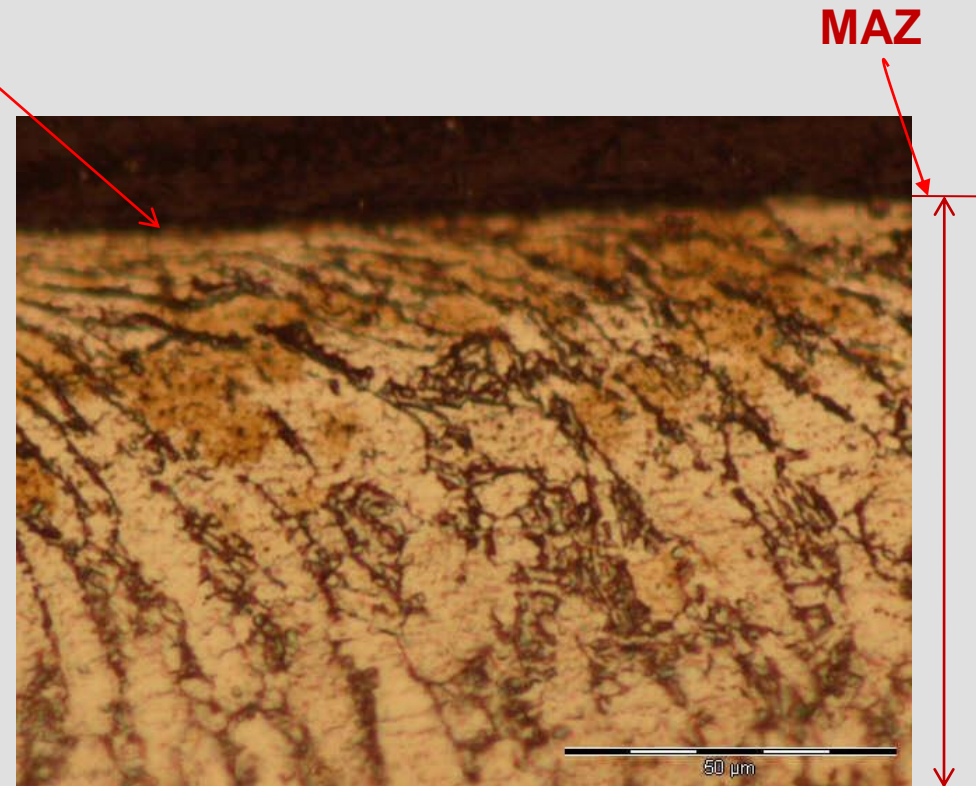
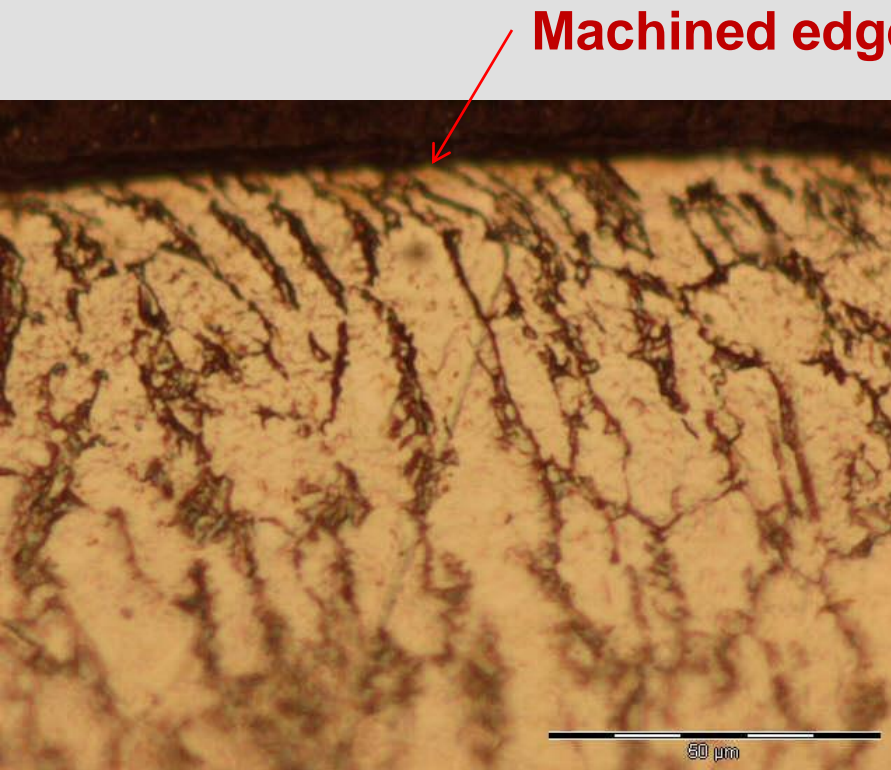
Temperature measurement



# Chip microstructure at dry, LN2, elevated temperature machining condition



Increased machining affected zone(MAZ) and material is subjected higher strain rate with increased temperature

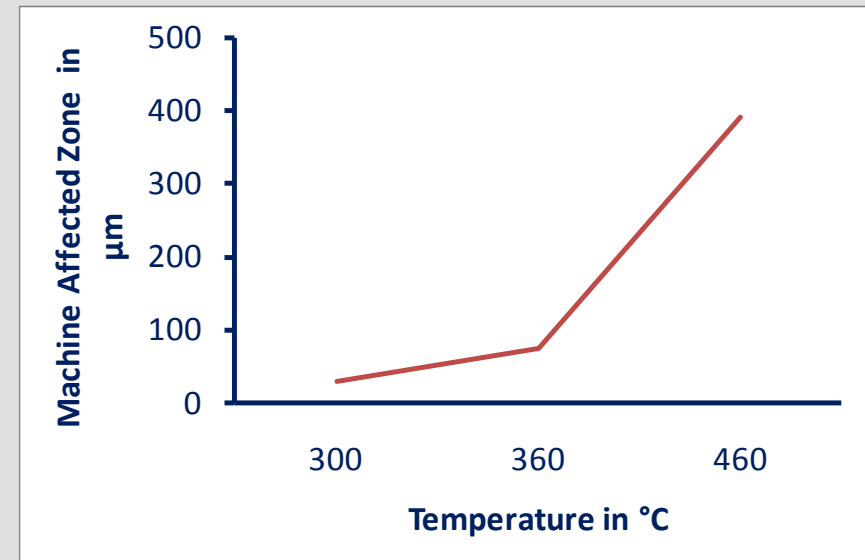
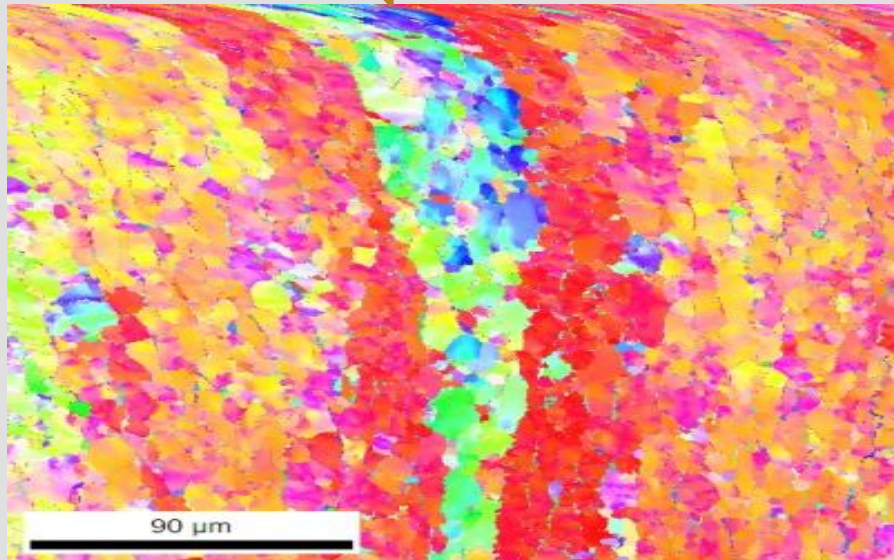


Optical image of chip obtained at 315 rpm  
feed rate of 0.11 mm/rev at **350°C**  
heating

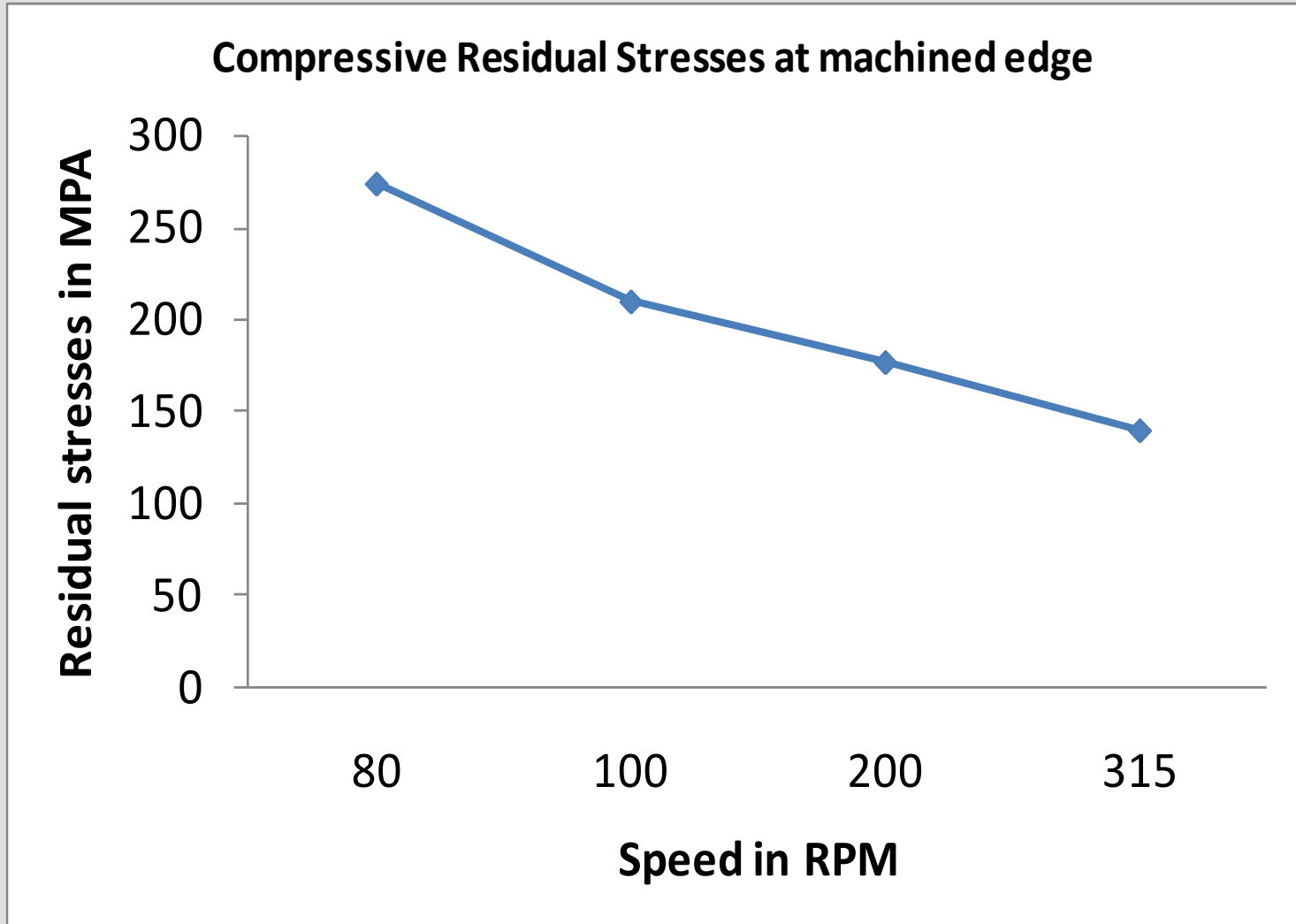
Optical image of chip obtained at 315 rpm  
feed rate of 0.11 mm/rev at **500°C** heating

# Electron Back Scatter Diffraction of Machining affected zone

Machined edge

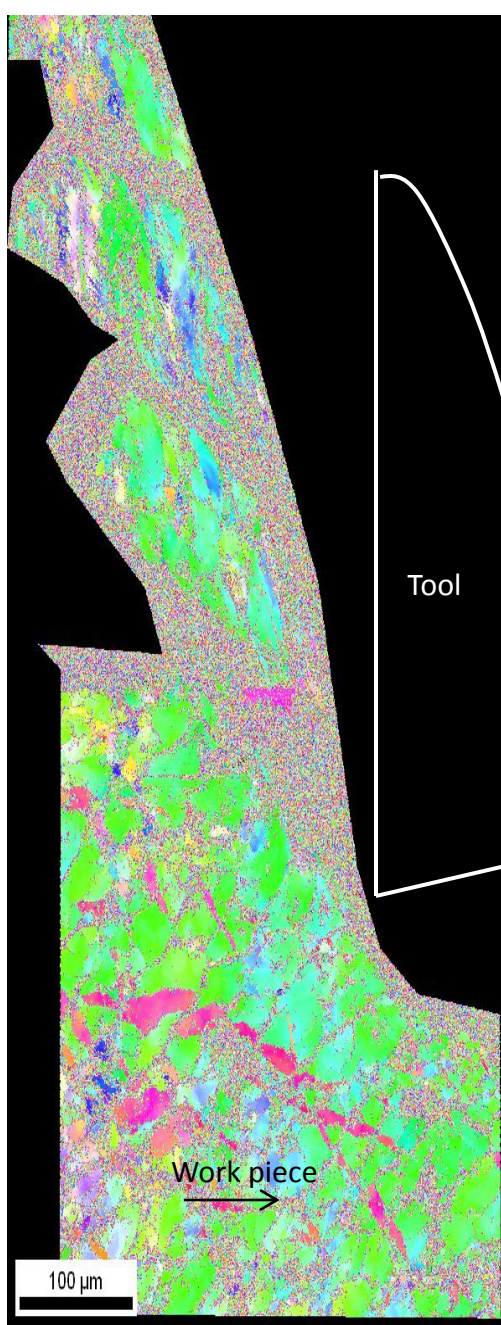


# Influence of speed on residual stress at Machined edge

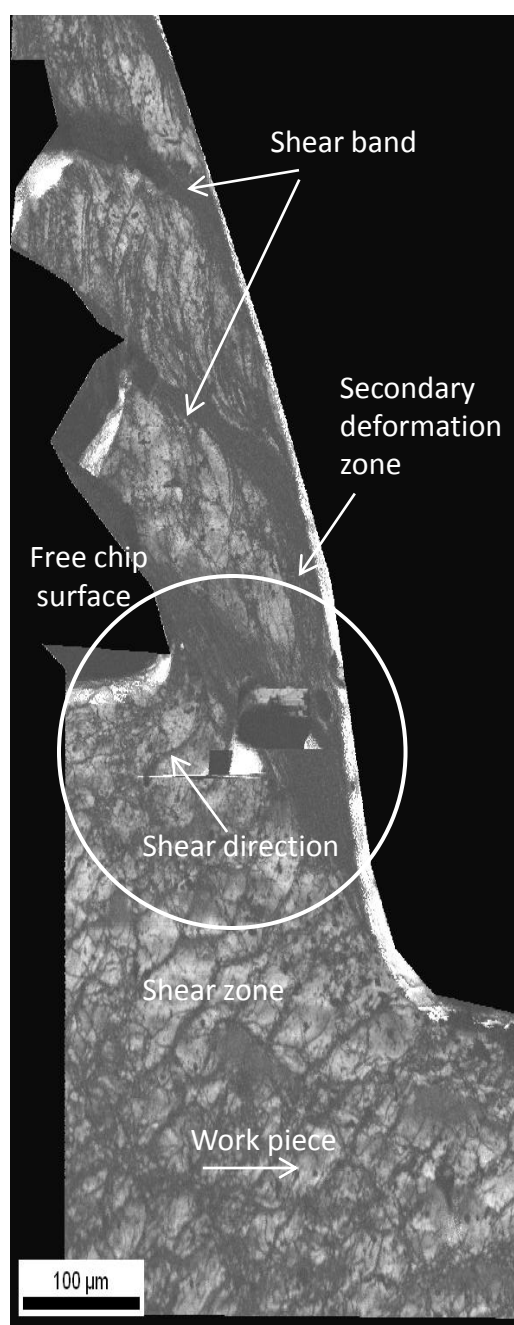


Influence of speed (feed constant 0.097 mm/rev.) on residual stress at Machined edge

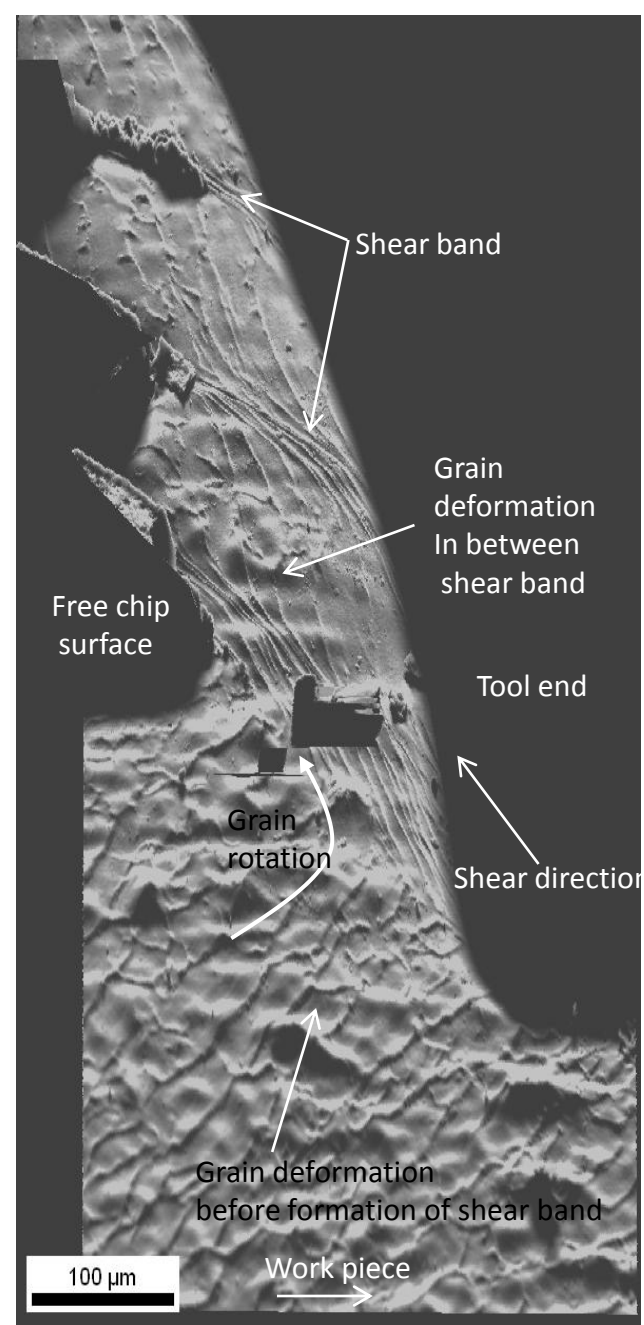




a. Phase quality map



b. Image quality map



c. SEM image

# Fracture criteria

- Segmented chips even at low cutting speeds (saw tooth profile)
- Chip segmentation criteria
- ✓ Thermoplastic instability
- ✓ Initiation and propagation of cracks inside the primary shear zone of the workpiece material

Cockroft and Latham damage criterion:  $C_i = \int_0^{\varepsilon_f} \sigma \left( \frac{\sigma^*}{\sigma} \right) d\varepsilon.$  [4,5,6]

Johnson Cook (JC) fracture model:  $D = \sum \frac{\Delta\varepsilon}{\varepsilon_f}$  [7,8,9]

where,  $\varepsilon_f = \left( D_1 + D_2 \exp(D_3 \sigma^*) \right) \left( 1 + D_4 \ln \left( \frac{\dot{\varepsilon}}{\dot{\varepsilon}_0} \right) \right) \left( 1 + D_5 \left( \frac{T - T_{room}}{T_{melt} - T} \right)^m \right)$   $\sigma^* = \frac{\sigma_m}{\sigma_v}$

Ref [4]"Prediction of chip morphology and segmentation during the machining of titanium alloys", Jiang Hua, Rajiv Shivpuri, Journal of Materials Processing Technology 150 (2004) 124–133

Ref [5] "Finite element simulation of conventional and high speed machining of Ti6Al4V alloy", Domenico Umbrello, Journal of materials processing technology 196 ( 2008 ) 79–87

Ref [6]"FEM simulation of orthogonal cutting: serrated chip formation", E. Ceretti, M. Lucchi, T. Altan, Journal of Materials Processing Technology 95 (1999) 17-26

Ref[7]"Material flow stress and failure in multiscale machining titanium alloy Ti-6Al-4V", J. Sun & Y. B. Guo, Int J Adv Manuf Technol (2009) 41:651–659

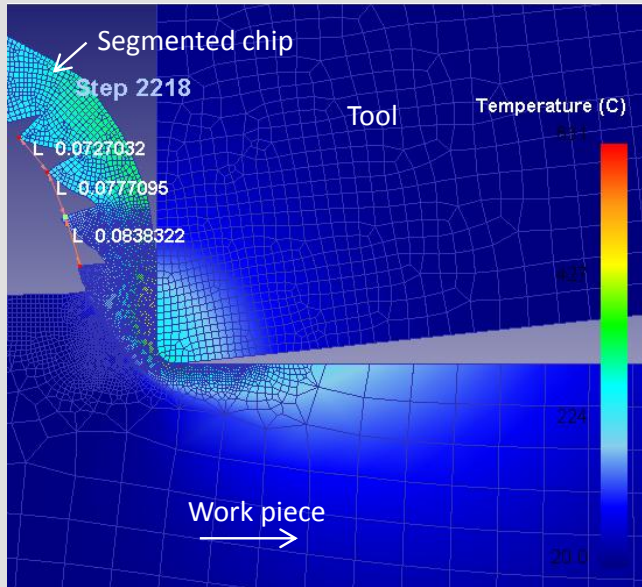
Ref[8]"A contribution to a qualitative understanding of thermo-mechanical effects during chip formation in hard turning", T. Mabrouki , J.-F. Rigal, Journal of Materials Processing Technology 176 (2006) 214–221

Ref [9]"Modelling of hard part machining", Eu-Gen Ng, David K. Aspinwall, Journal of Materials Processing Technology 127 (2002) 222–229

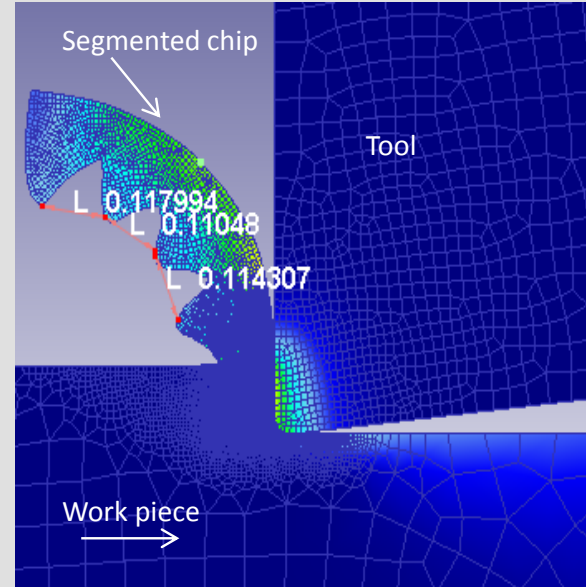
# Material Models

<p>JC Model</p> $\sigma = (A + B\varepsilon^n) \left( 1 + C \cdot \ln \left( \frac{\dot{\varepsilon}}{\varepsilon_o} \right) \right) \left( 1 - \left( \frac{T - T_{room}}{T_{melt} - T} \right)^m \right)$	<p>Takes in to account strain hardening effect, viscosity effect softening effect.</p>	<p>Coupling effects of strain rate and temperature absent The parameters fitted to the stress-strain curves (SPHB)</p>
<p>Modified JC model</p> $\sigma = \left( A + B\varepsilon^n \left( \frac{1}{\exp(\varepsilon^a)} \right) \right) \left( 1 + C \cdot \ln \left( \frac{\dot{\varepsilon}}{\varepsilon_o} \right) \right) \left( 1 - \left( \frac{T - T_{room}}{T_{melt} - T} \right)^m \right) \left( D + (1 - D) \tanh \left( \frac{1}{(\varepsilon + s)^c} \right) \right)$	<p>Incorporates the strain softening effect Was able to account for segmented chips formation at low cutting speed</p>	<p>The above mentioned models do not consider the effect of microstructure during machining.</p>
<p>Micromechanical Physic based model</p> $\sigma = (1215 \cdot \varepsilon^{0.06}) + 601.2 \left( \left( 1 - \left( -9.58 \times 10^{-5} T \cdot \ln \left( \frac{\dot{\varepsilon}}{4.2 \times 10^8} \right) \right)^{\frac{4}{5}} \right)^{\frac{3}{4}} \right)$	<p>Flow stress has two parts: Athermal part (<math>\sigma_a</math>) Thermal part (<math>\sigma^*</math>)</p>	<p>Above critical temperature, gave a constant value of stress for all temperature hence not for machining</p>
<p>Modified Micromechanical physics based model</p> $\sigma = (a\varepsilon^n + b)(cT^{*2} + dT^* + e)h(\varepsilon, \dot{\varepsilon})$	<p>Temperature dependent flow softening</p>	<p>Phase change not incorporated.</p>

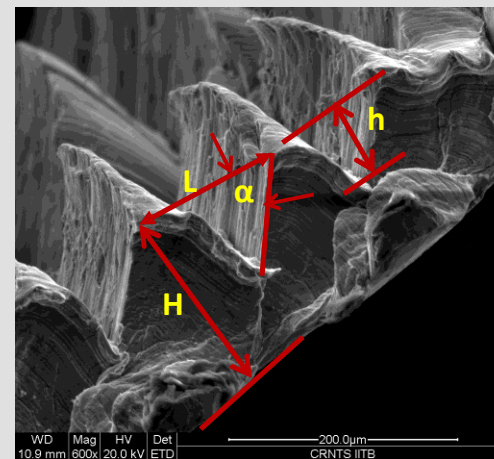
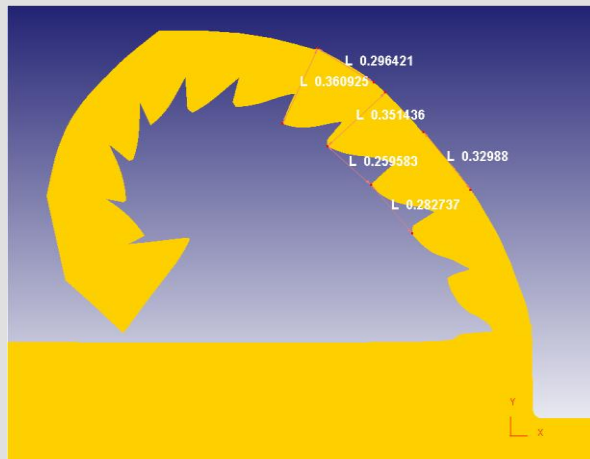
# FEM Simulation



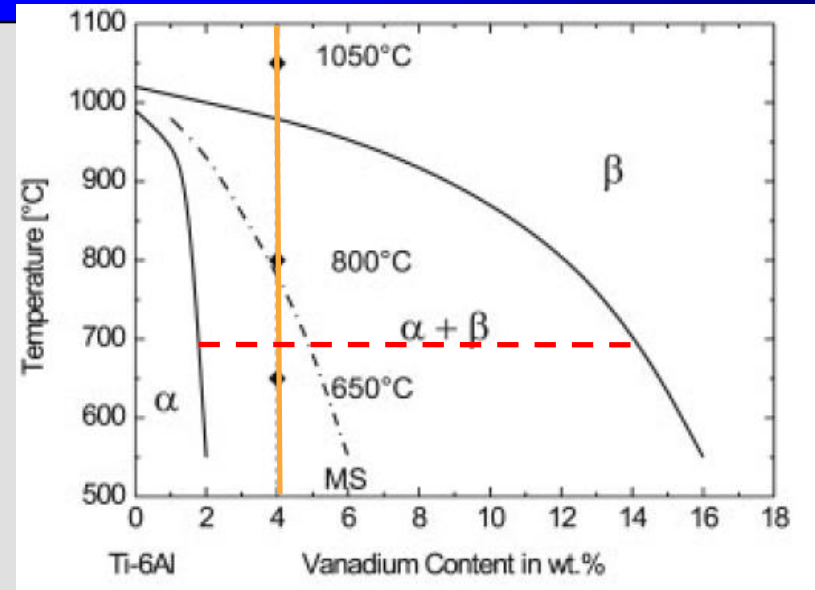
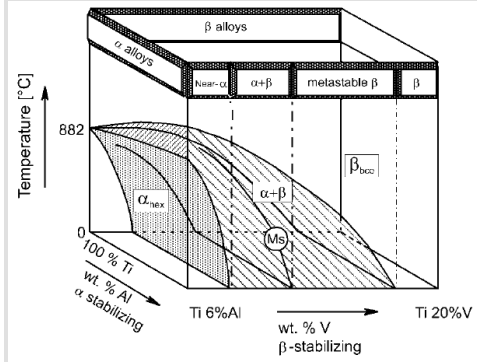
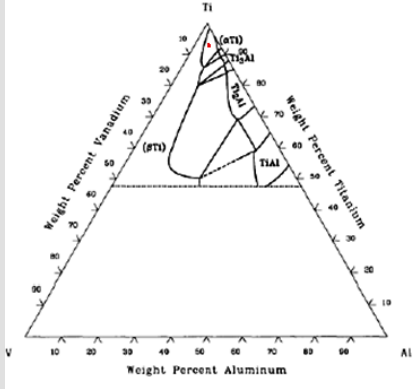
*a.* at 23.4 m/min , room temp.



*b.* at 91.8 m/min, room temp.

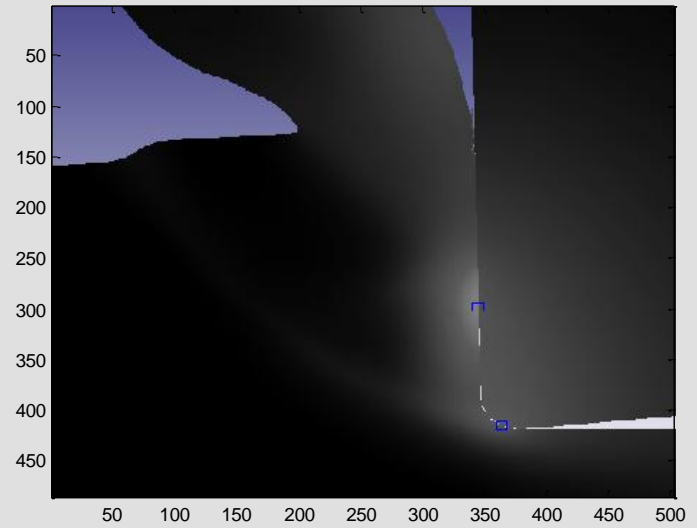
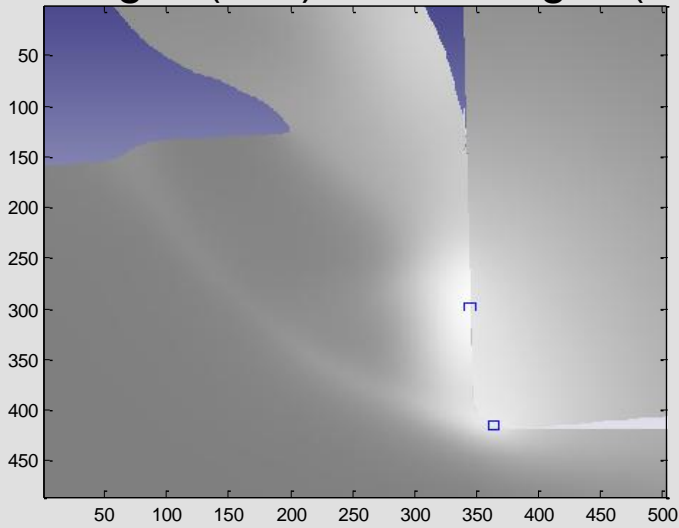


# Phase transformation calculation



Temperature distribution  
20 deg C (130) To 700 deg C (254)

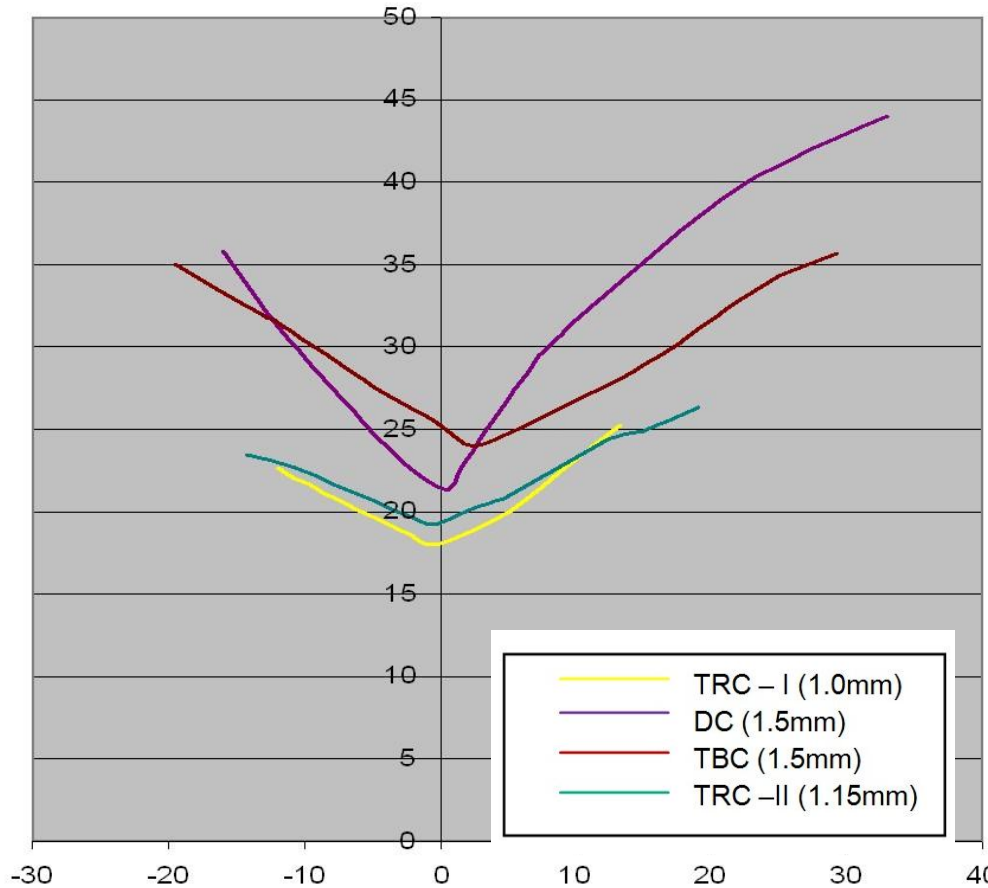
Beta Phase distribution  
8% (0) To 20% (255)



# Case Study 2

## Aluminum sheet metal forming

# Motivation



Large formability variation of same 5754 Al alloy processed through different processes

# Alloy composition and processing

5754 Alloy	Mg wt%	Mn wt%	Cr wt%	Fe wt%	Si wt%
DC	3.0	0.25	0.01	0.18	<0.10
TBC	3.1	0.25	<0.01	0.24	<0.10
TRC-I	2.8	0.01	<0.01	0.25	0.10
TRC-II	2.9	0.01	<0.01	0.24	0.08



Di

Co

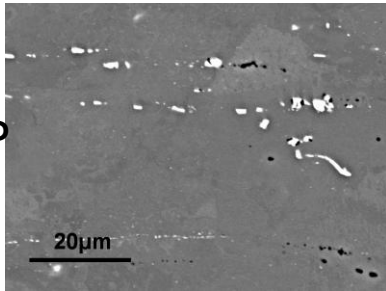
Co

Batch #

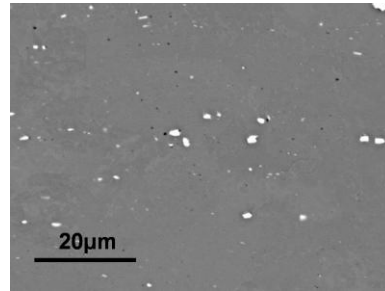


# Typical microstructure of various 5754 alloys

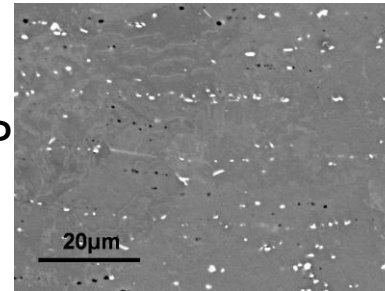
TBC



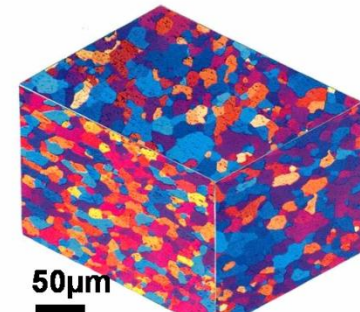
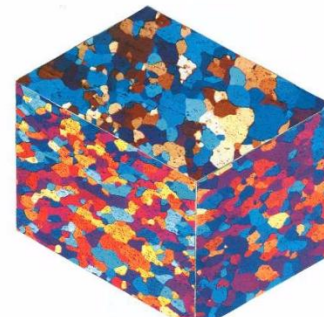
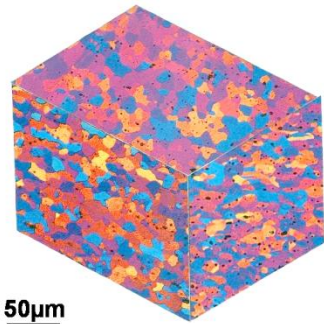
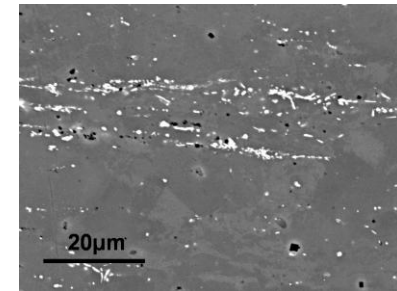
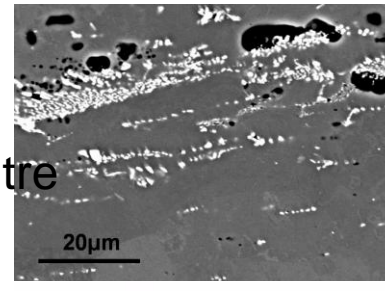
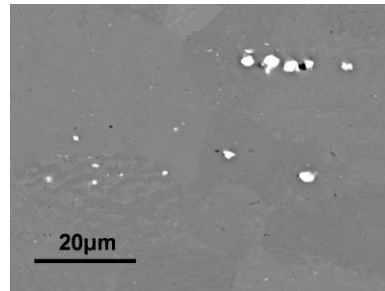
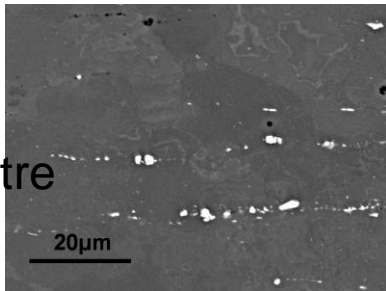
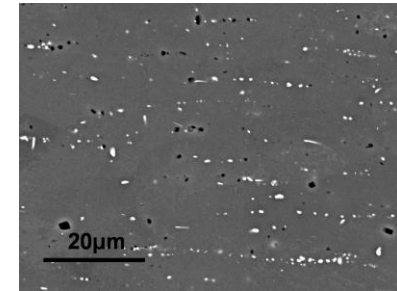
DC



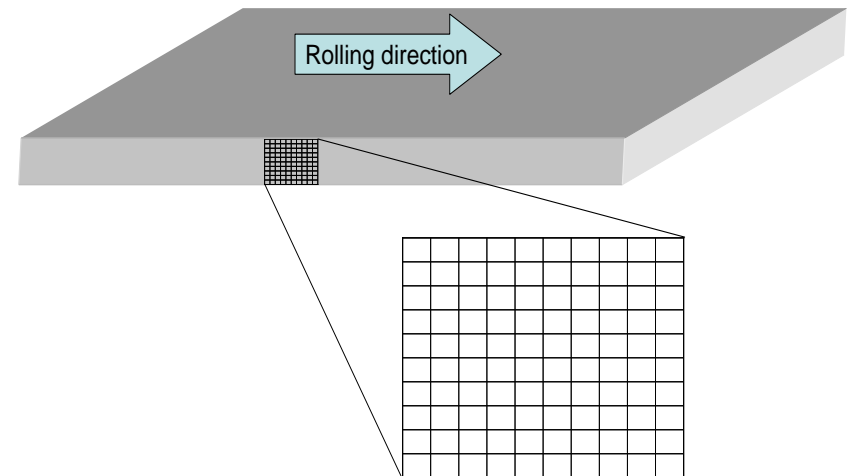
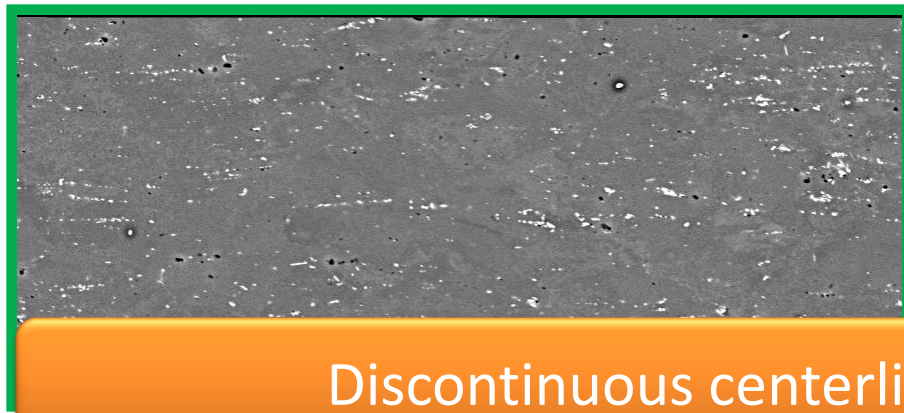
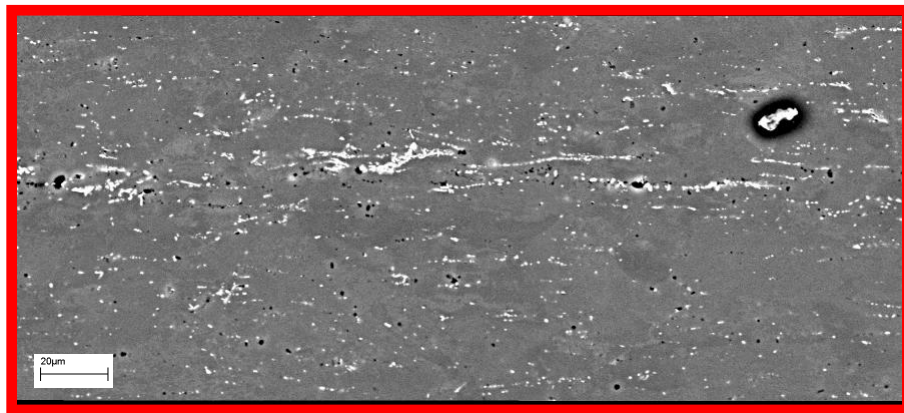
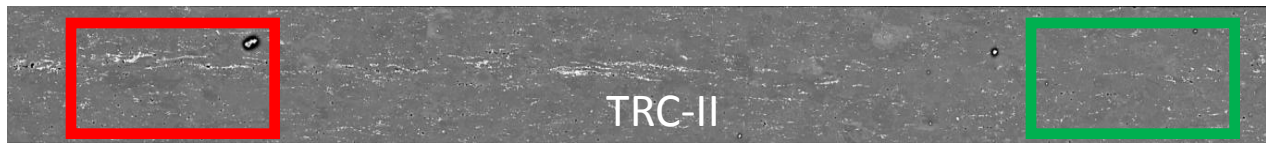
TRC-I



TRC-II

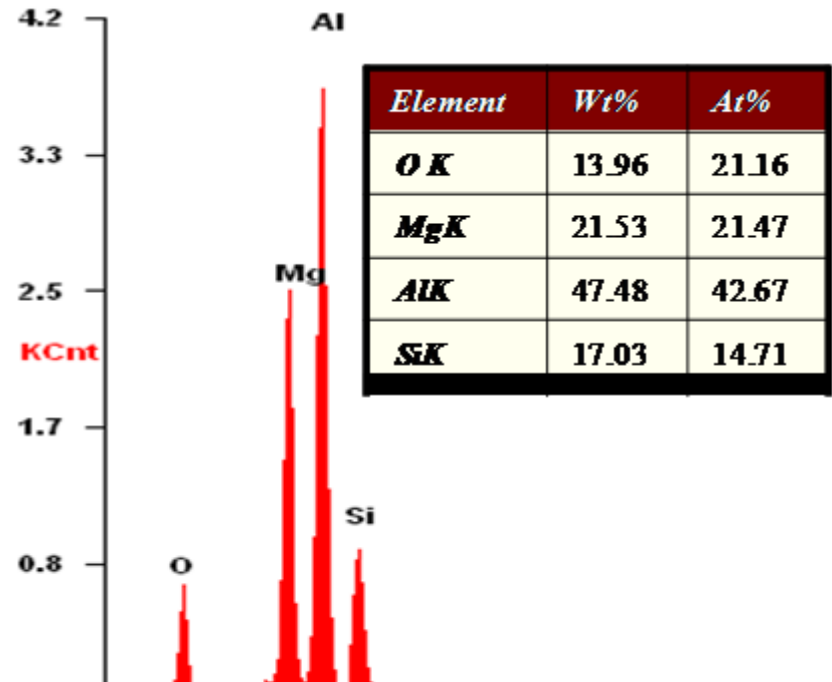
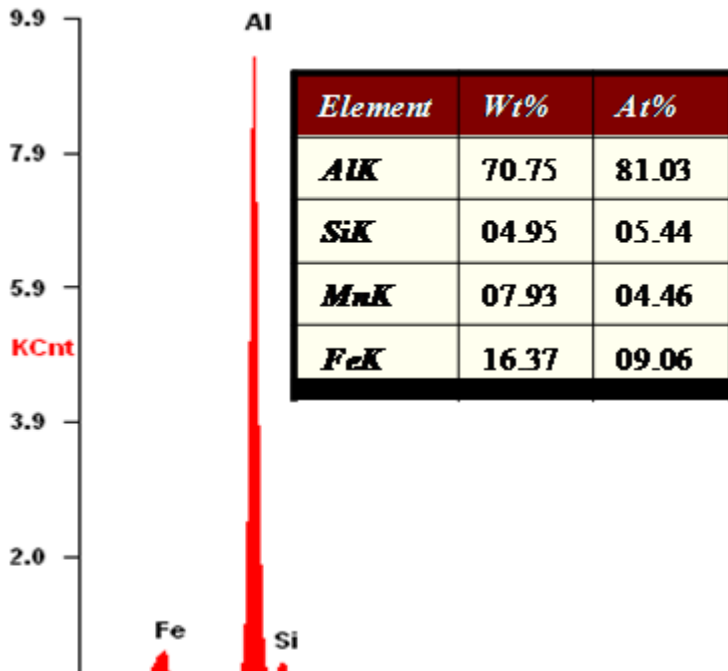
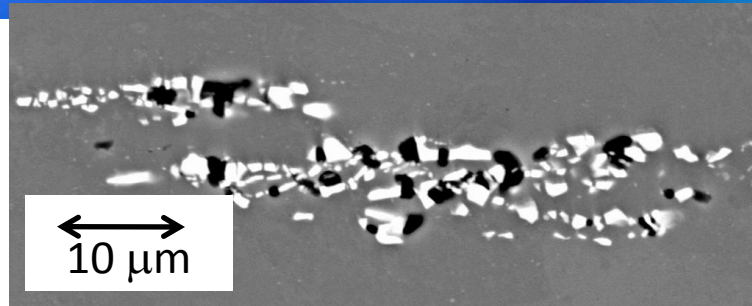


# Center-line Segregation



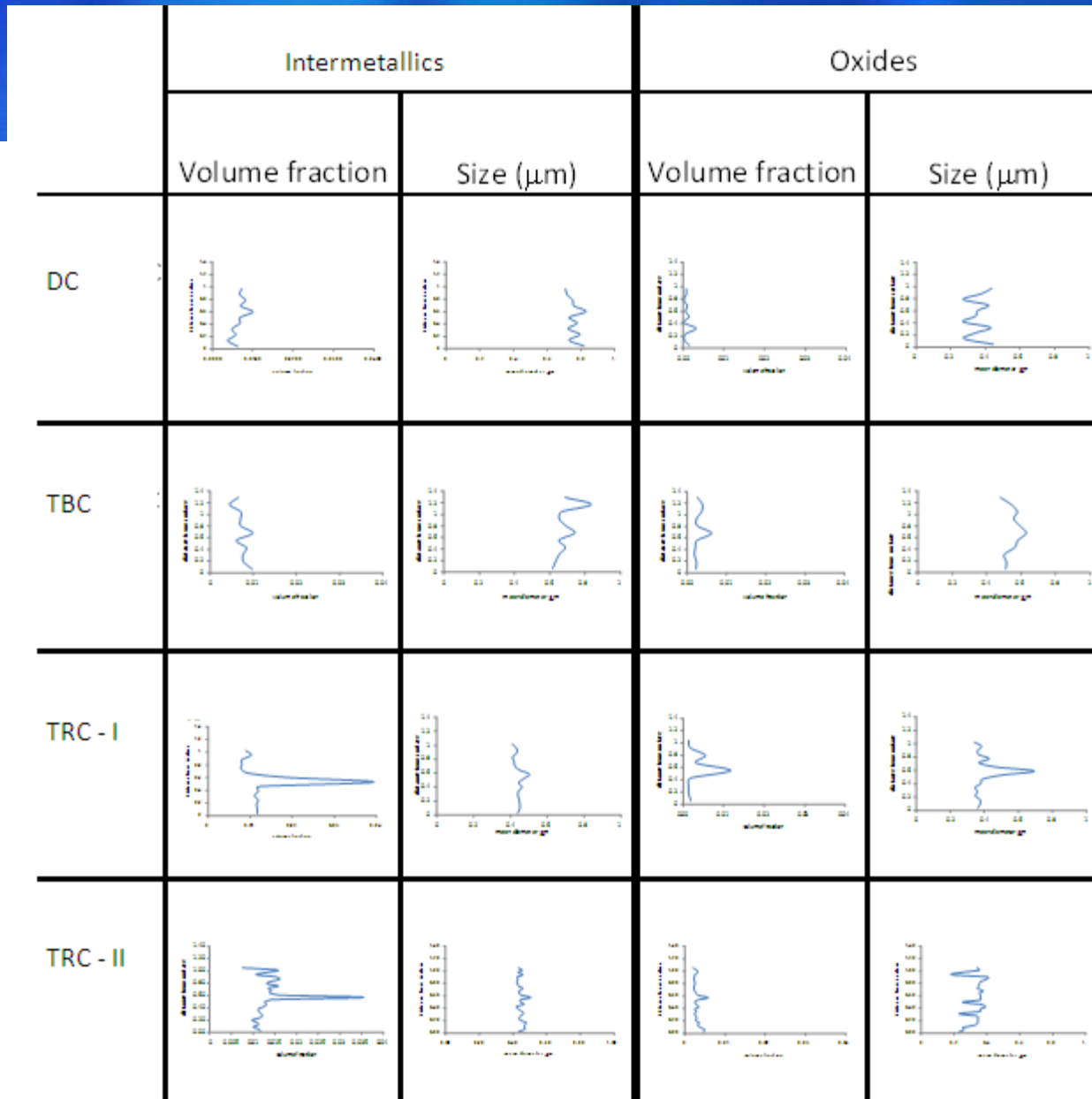
Discontinuous centerline segregation in TRC-II

# Second phase particles

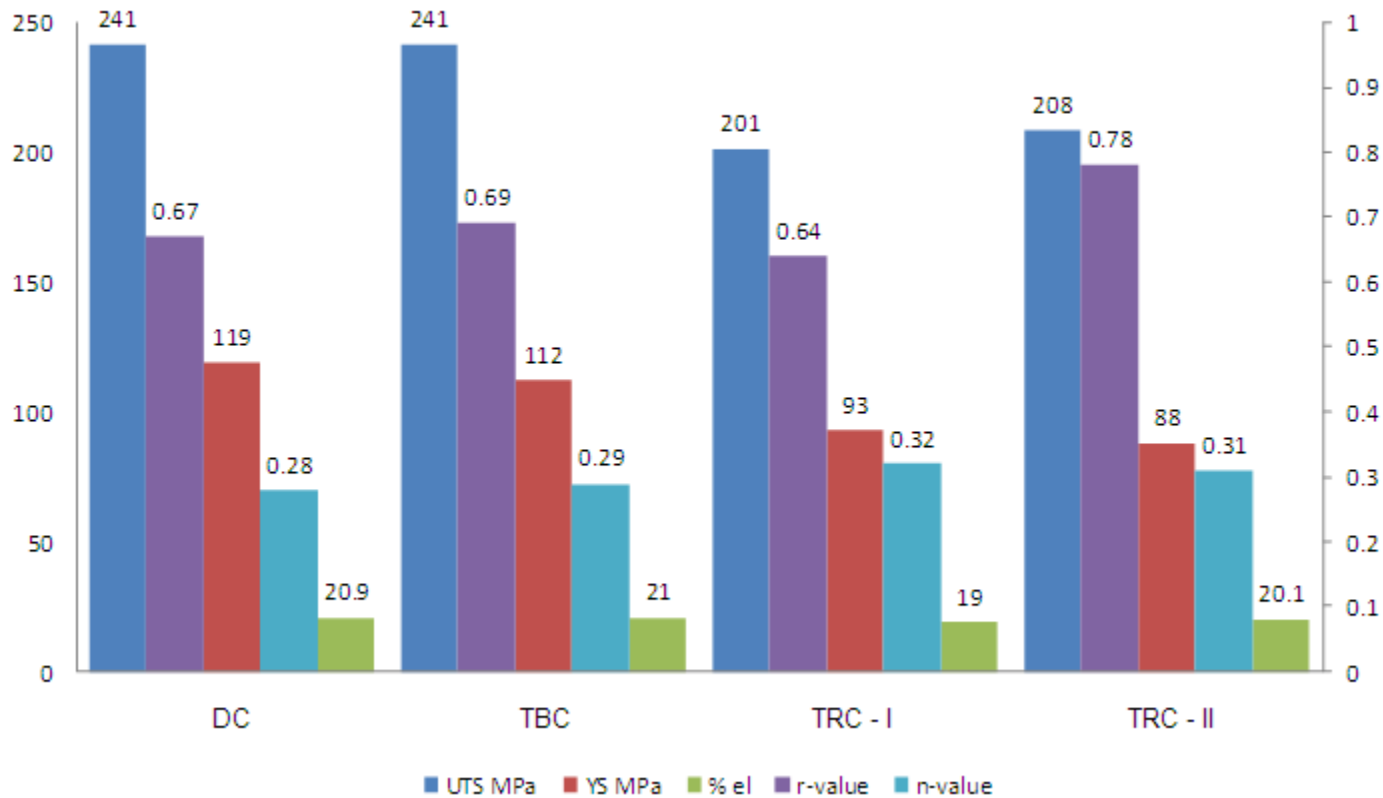


Two type of second phase particles are present

# Through thickness microstructure variation

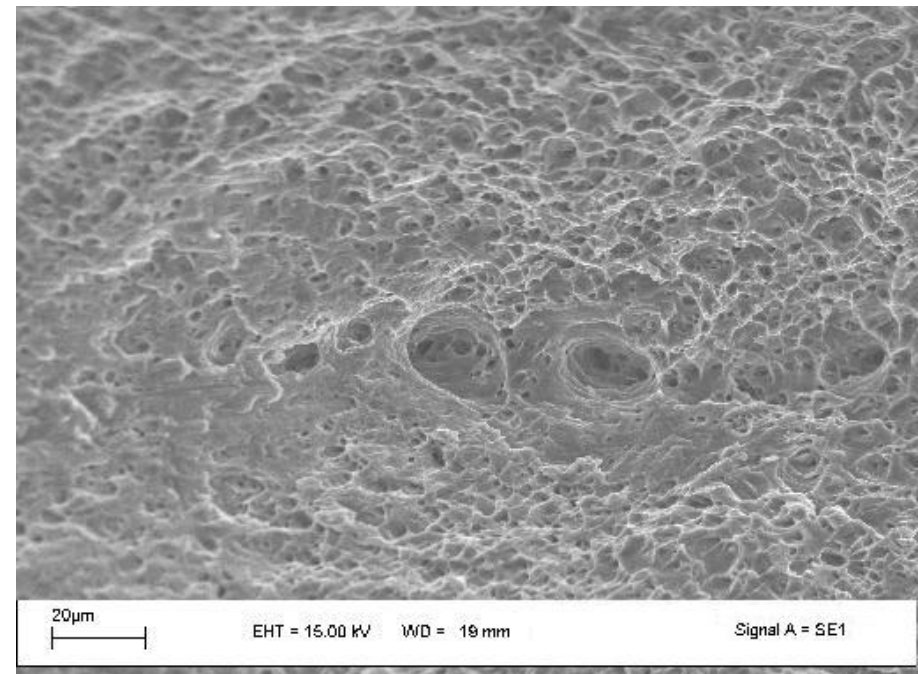
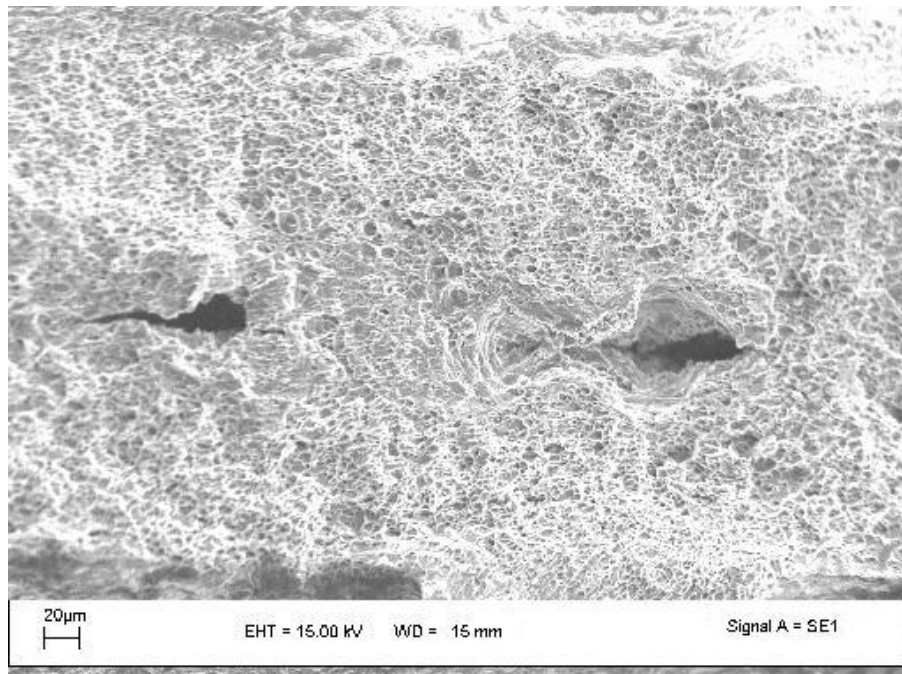


# Mechanical properties along the rolling direction



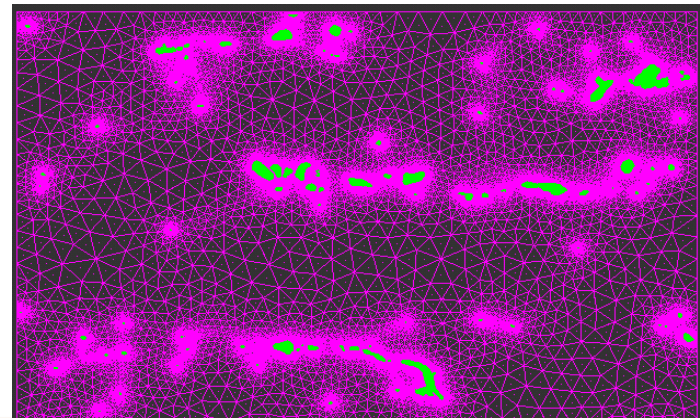
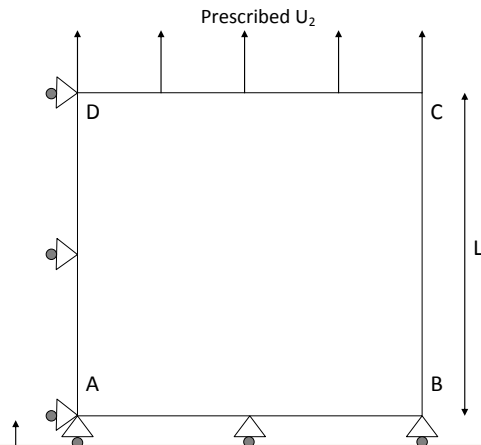
TRC has lower YS and UTS than TBC or DC

# Fractographic investigation (TRC-I)



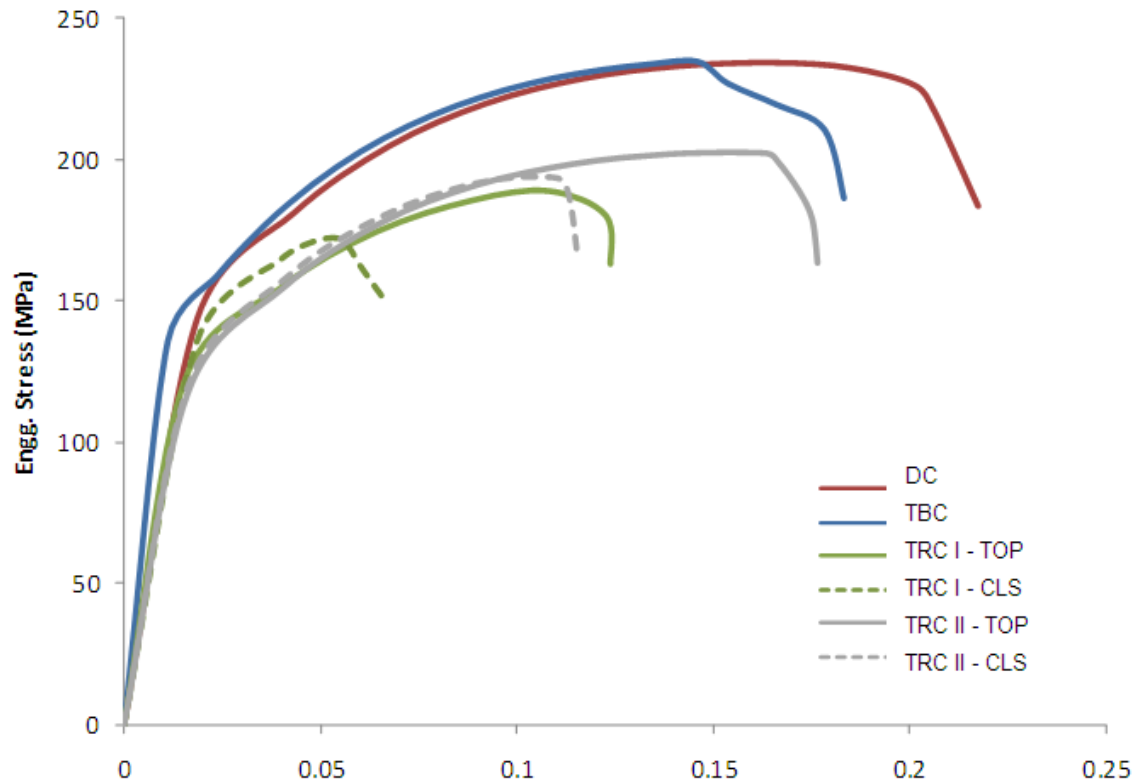
Microvoid formation at particle clusters

# Microstructure based FEA



Modeling particles as intersecting ellipses is a good approximation

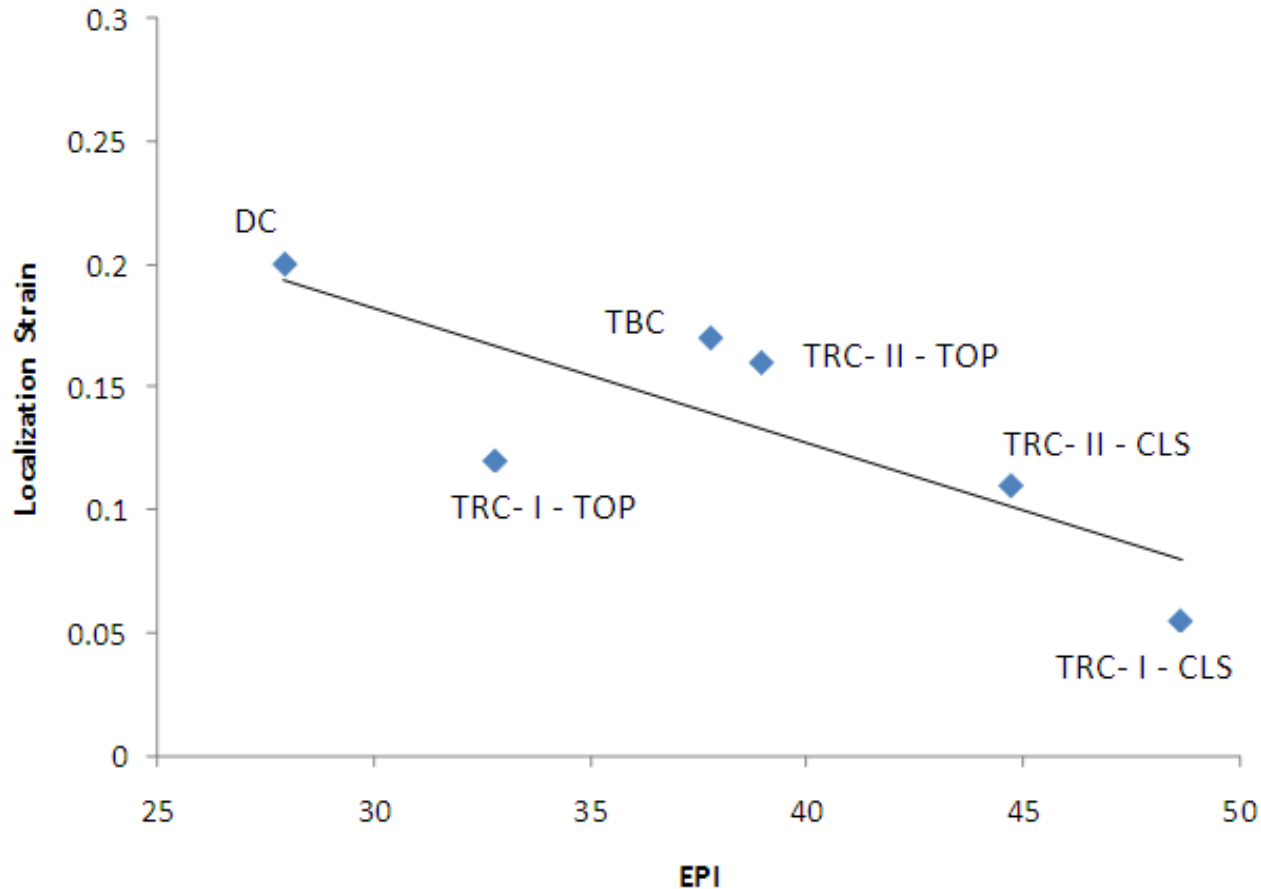
# FE predictions of uniaxial stress-strain behavior



Novelis has higher localization strain than Assan  
With in Assan, center region has lower localization strain than top

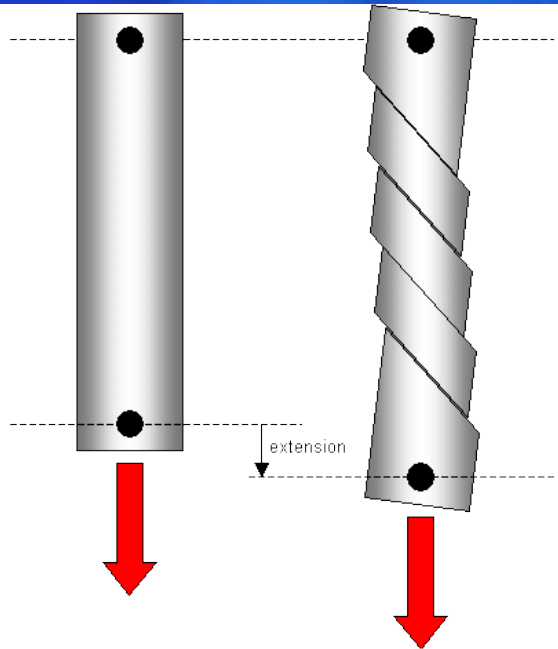


# Correlation of localization strain and Extreme Property Index (EPI)



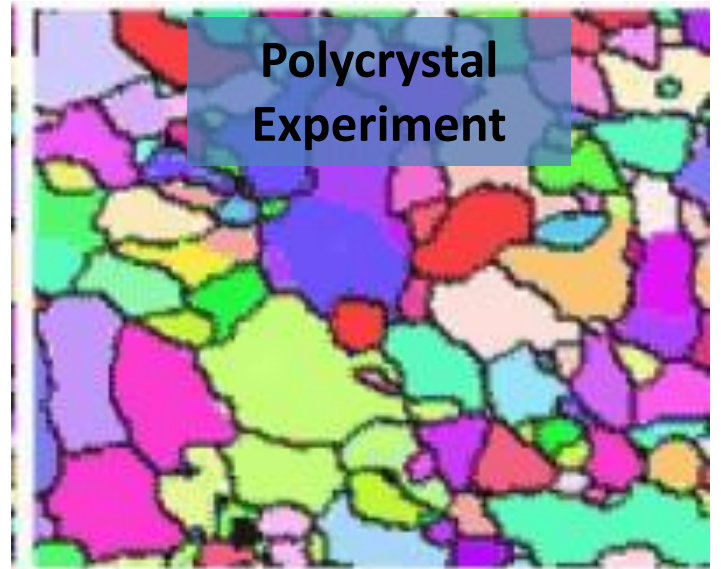
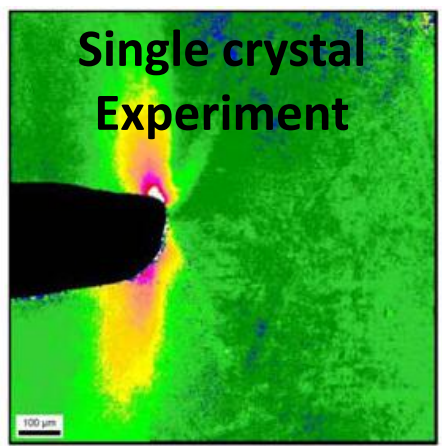
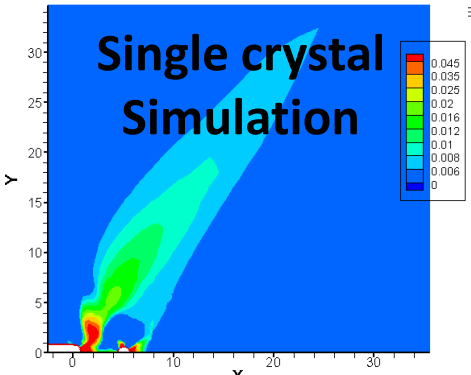
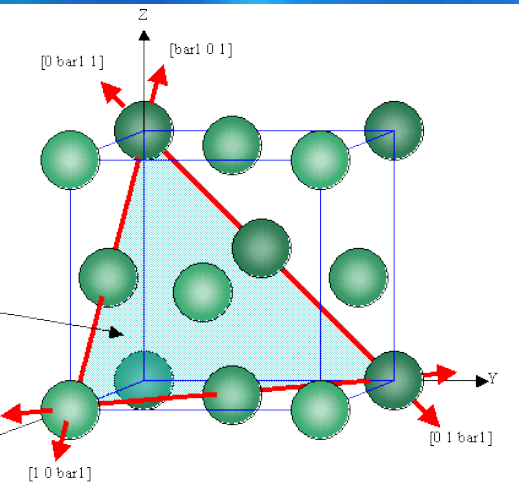
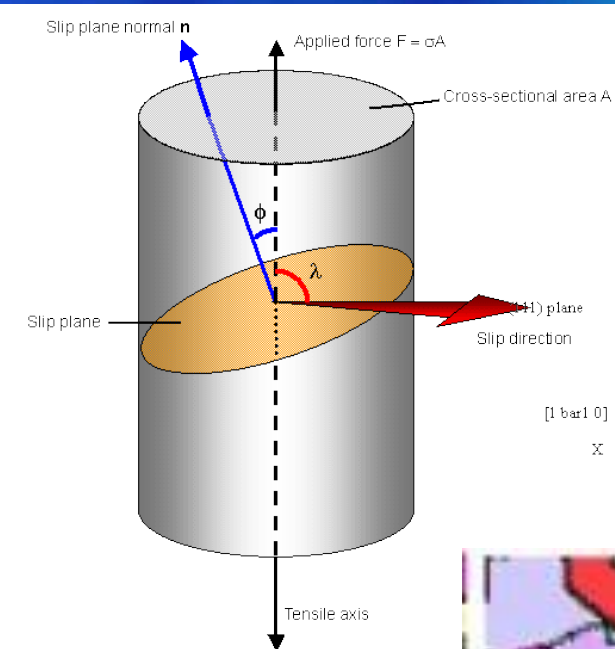
EPI is identified as a key microstructural attribute

# Plastic deformation by slip

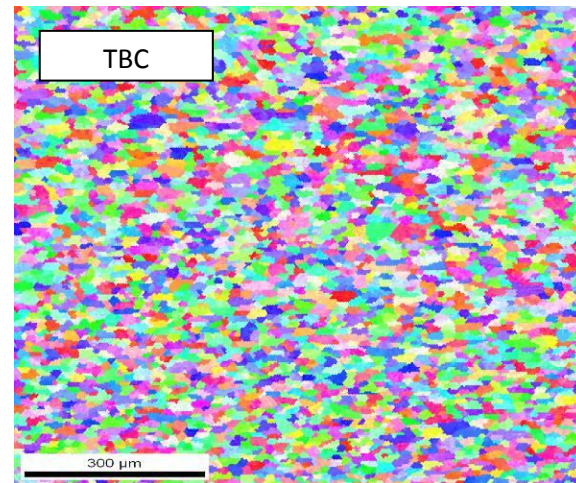
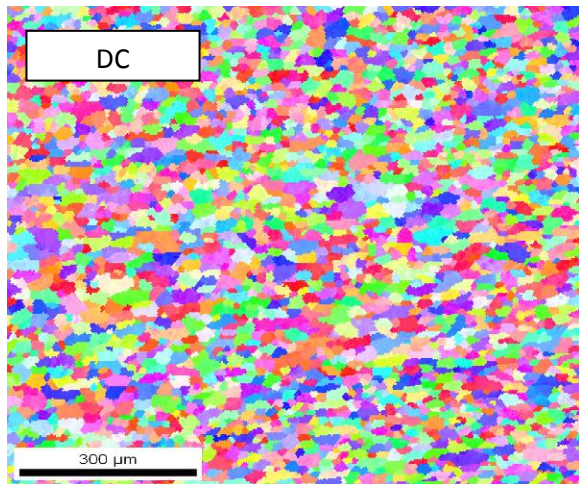


Unslipped single crystal fixed at top end.

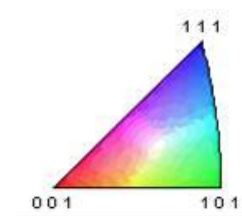
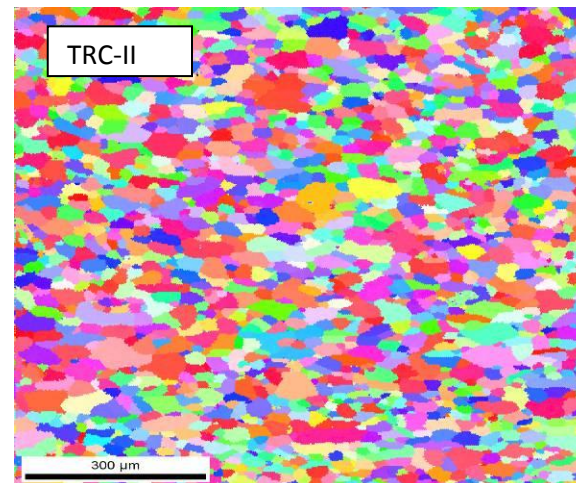
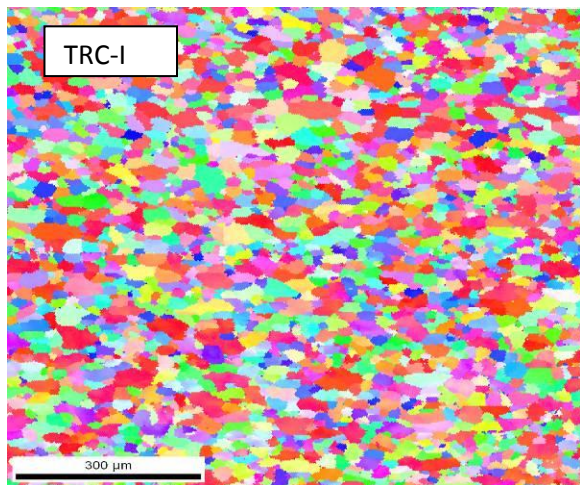
Single crystal after plastic deformation by tensile stress in the direction of the arrow. Slip occurs on distinct parallel



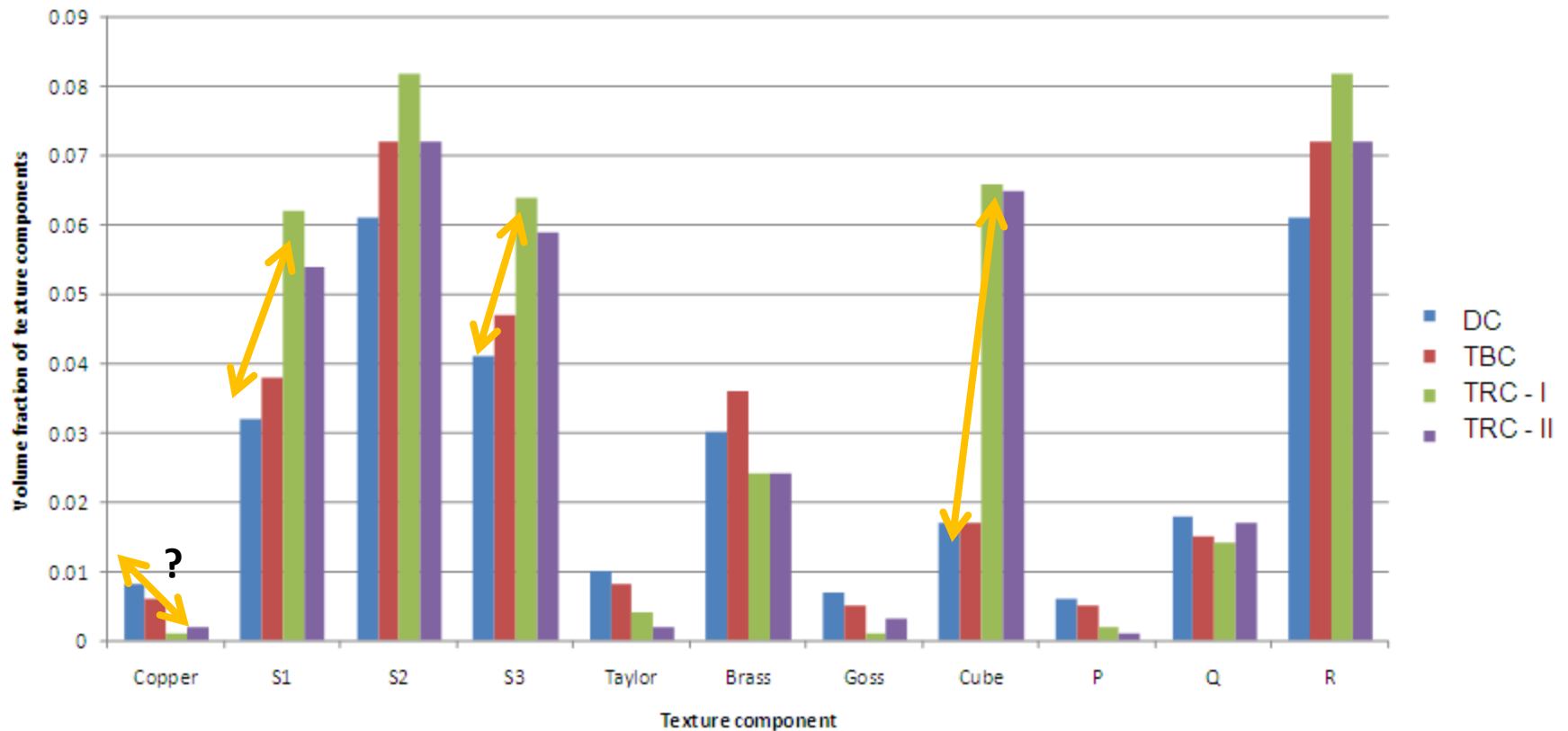
# Inverse pole figure maps



Rolling Direction  $\rightarrow$

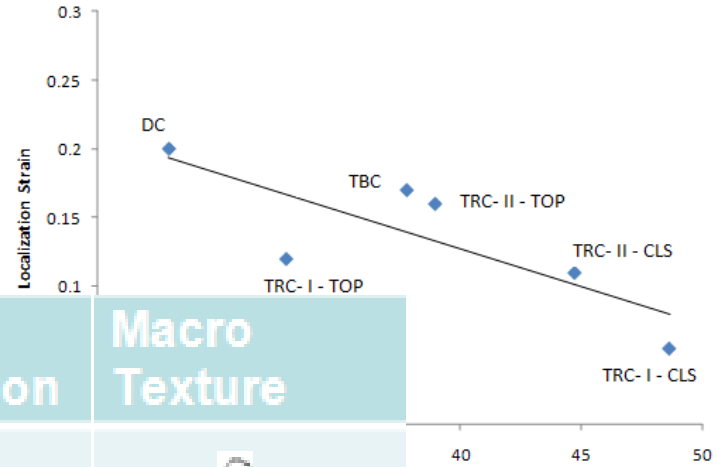
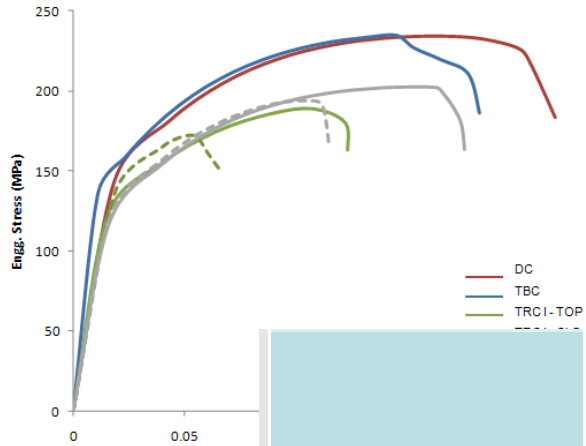


# Fraction of various texture components

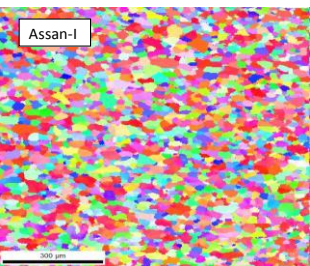
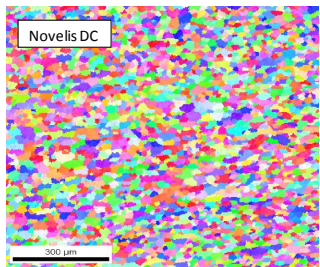


TBC has more rolling texture while TRC has more re-crystallization texture

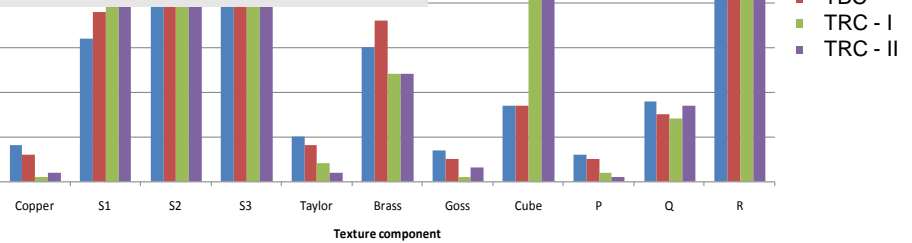
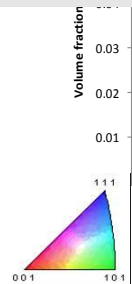
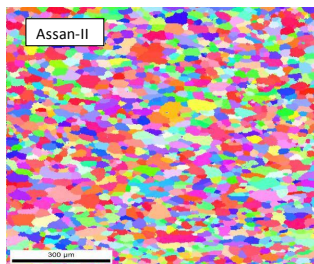
# Summary



	Particle distribution	Macro Texture
DC		
TBCC		
TRCC-I		
TRCC-II		



Rolling Direction



# Conclusion

Multi-scale Multimodality Microstructure plays a central role in manufacturing processes.

- 1.) Machined surface quality and performance is a stronger function of microstructure.
- 2.) In forming particle distribution and texture can work in cross purpose.